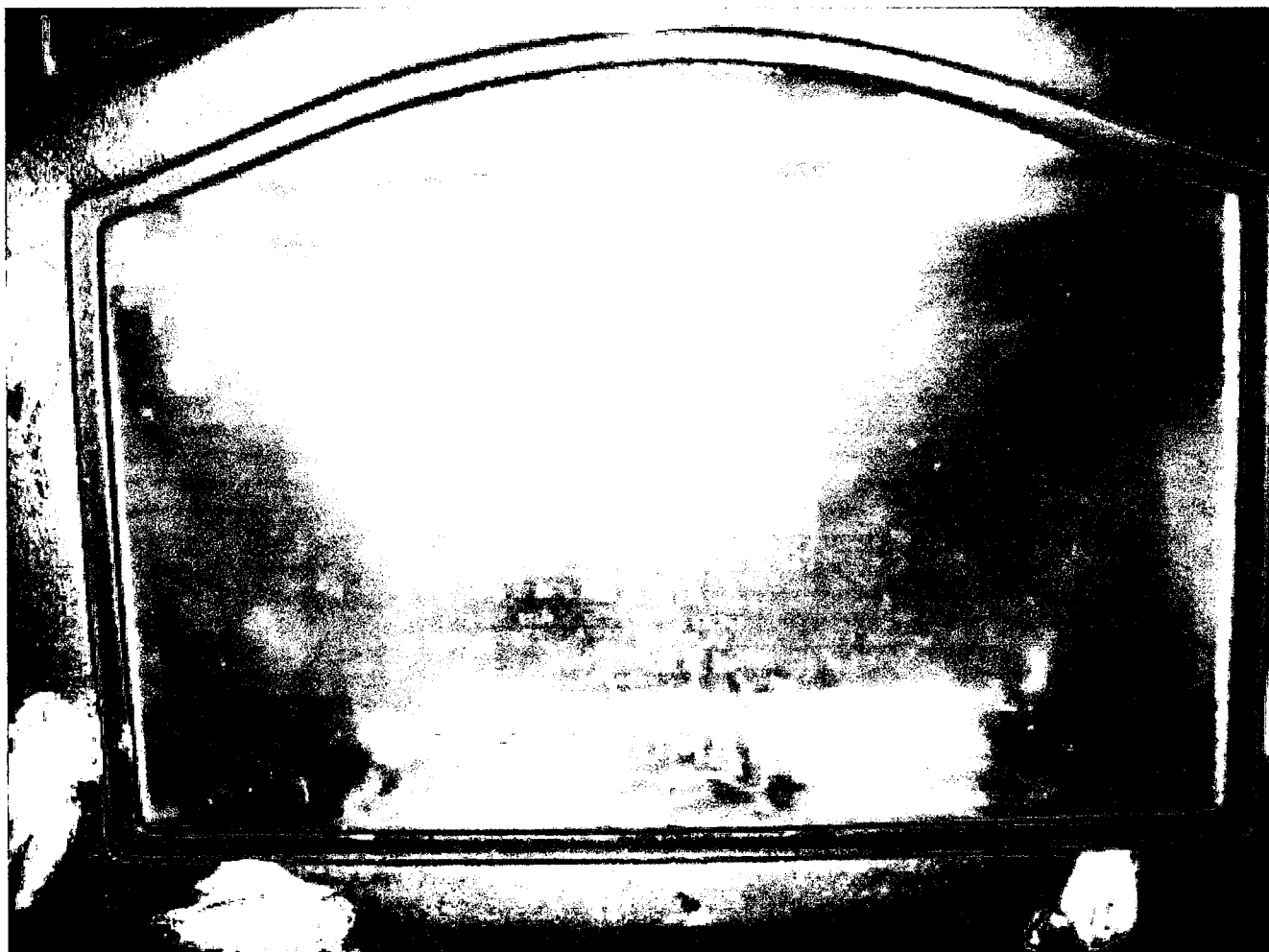


**US EPA WOOD HEATER  
CERTIFICATION TEST REPORT**

**KUMA STOVES, INC.  
KUMA ASHWOOD  
NONCATALYTIC WOOD HEATER**

**MARCH 28, 2009**



**MYREN CONSULTING, INC.**

**OFFICE**

512 WILLIAMS LAKE ROAD  
COLVILLE, WA 99114  
PHONE 509-684-1154  
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**LABORATORY**

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\* \* \* \* \*

CONFIDENTIAL

\* \* \* \* \*

The data and information in this test report is confidential, proprietary information and is not to be released to and/or discussed with any party who is not authorized by the manufacturer or the testing laboratory to receive such data.

\* \* \* \* \*

CONFIDENTIAL

\* \* \* \* \*

Photos:

This section contains two photographs of the fuel load for each test run and two color photographs (side and front view) of the wood heater tested and any other photographs pertinent to testing the unit.

Photos

vari

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FIELD OBSERVATION CHECKLIST

Unit Name: KUMA ASHWOOD

Manufacturer Name: KUMA STOVES, INC.

Manufacturer Address: 2150 W. HAYDEN AVE.  
HAYDEN, ID 83835

Manufacturer Phone: 208 762 8002

Fax: 208 762 ~~5882~~ 5862

Observers & Affiliation: NONE

SUPERVISOR: BEN MYREN

MYREN CONSULTING'S LAB TEAM: JOHN PALM, ILSE MYREN, PAT  
GARVEY, BEN MYREN

LAB LOCATION: 501-C WILLIAMS LAKE ROAD, COLVILLE, WA  
99114

LAB ELEVATION: 1645 FEET

MYREN CONSULTING, INC.

LABORATORY

501-C WILLIAMS LAKE ROAD  
COLVILLE, WA 99114  
509 685 9458

OFFICE

512 WILLIAMS LAKE ROAD  
COLVILLE, WA 99114  
509 684 1154  
509 684 3987

# REPORT CERTIFICATION

The sampling and analysis for the appliance described in this test report was carried out under my direction and supervision.

Date: 3/29/09 Signature: Alben V. Myren Jr  
Title: President

I have reviewed all of the test data and test results found in this test report and hereby certify that the test report is authentic and accurate.

Date: 3/29/09 Signature: Alben V. Myren Jr  
Title: President

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4. Manufacturer's Testing Instructions	Operator's Manual	P.1 of Section
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6. Wood Heater/Catalyst Aging Documentation	Stove/Cat Aging	
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      - 3. Net Data Sheet #6
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M5G-1 INDIVIDUAL TEST RUN PAGE INDEX  
The Data Sheets in the individual test runs  
Are organized in the following sequence.

A. Computer Printout(s)

- Table 1 Field Data - Sampling Interval Data
- Table 1 Field Data
- Table 1 Field Data Averages
- Table 1 Calculations
- Table 1 Proportional Rate Variation

B. Raw Data Sheets

	# of Pages
Data sheet # 2 Meterbox Data Sheets	Variable
Data Sheet # 4 Analytical Balance Data Sheets	
# 4-1 Filter Tare Weights	Variable
# 4-2 Beaker Tare weights	Variable
# 4-3 Constant Final Weights	Variable
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Data Sheet # 14 Burn Rate, Flue Gas & Temperature Data	Variable
Data Sheet # 15 Pre & Post Test Zero/Span Audits	
# 15-1 CO <sub>2</sub>	1
# 15-2 O <sub>2</sub>	1
# 15-3 CO	1
Data Sheet # 16 Quality Checks	1

## TEST SERIES INFORMATION AND DISCUSSION

Unit: Kuma Ashwood Noncatalytic Wood Heater

Model: Ashwood

Manufacturer: Kuma Stoves, Inc.

Date Received: 2/12/09 Date(s) Aged: 2/12 & 13/09

Test Dates: 2/16, 17, 18, 19, 20, 27 & 3/2 2009

Sampling Method(s): EPA M5G-1

Fueling Protocol: EPA M28

Number of Test Runs: 7

The Kuma Ashwood Noncatalytic wood heater manufactured by Kuma Stoves, Inc. located in Hayden, ID was tested by Myren Consulting, Inc. using the Environmental Protection Agency's (EPA) Method 28, "Certification and Auditing of Wood Heaters", Method 5G-1, "Determination of Particulate Emissions from Wood Heaters from A Dilution Tunnel Location" and, if applicable, Method 28A, "Measurement of Air to Fuel Ratio and Minimum Achievable Burn Rates for Wood Fired Appliances". (See the Federal Register/ Vol.53, No.38/ Friday, February 26, 1988/ pp.5860-54926.) The particulate matter (PM) emission data, if reported, was calculated as specified in the Wood Heater New Source Performance Standard (NSPS).

All events and information pertinent to the test data are recorded on the data sheets for each test run, particularly on pp. 9, 9-1, 9-2, 9-3, 9-4 and 9-5 if present.

Any deviations made or noted from the promulgated methods other than those that were accepted and certified by EPA during the laboratory accreditation process are listed and discussed below.

A brief note about how the EPA M5G-1 particulate samples were processed is necessary to help the reviewer understand the net catch values. Experience has shown that the small portions of the filters that are left on the frits in the M5G-1 filter housing apparatus after the

filters are removed are full of static electricity. When these small portions are removed to a plastic petri dish, they quickly adhere to the dish. Trying to recapture this material during weighing causes it to disintegrate into smaller and smaller pieces, which makes obtaining accurate catch weights difficult. Thus, it was decided to place this filter material in with the particulate captured with the acetone wash, where it shows up as catch. Some of the filter material was already following this pathway. Thus, there may be negative filter catch weights, particularly for the back half filter, that are used during the particulate emission rate calculation process. However, the filter material lost off the filters is accounted for in the acetone catch.

The following pages contain (1.) a diagram showing the height of the appliance and black pipe and Class A chimney and the location of the sampling ports in the chimney and (2.) a diagram of the EPA 6" diameter dilution tunnel used by Myren Consulting during testing, (3.) a copy of the letter requesting a waiver from the 30 day certification test notification requirement, (4.) a copy of the fax machine's output indicating that the fax had been received by EPA and (5.) a discussion of results.

#### DISCUSSION:

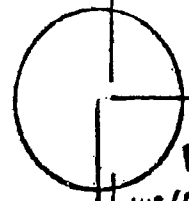
- (1.) The first Medium Low (1.0-1.25 kg/hr) test (Run 5) had emissions that were higher than expected. There was a break between Run 5 and Runs 6 & 7 because we waited for a final constant weight for the filters and beaker for Run 5 so that we knew for certain that the extra runs were really necessary. The manufacturer wanted the weighted average emission rate for the Ashwood to be below 4.0 g/hr if at all possible.
- (2.) The way the test results are calculated has changed slightly. The average tunnel gas velocity was calculated using the square root of the average of the  $\Delta p$  readings. Now the tunnel gas velocity is calculated using the average of the square roots of the  $\Delta p$  readings and the average static pressure ( $P_g$ ) reading. This change is based upon comments made by Mr. Mike Toney of OAQPS, EPA, RTP, NC.

STACK - HT. 14.396'

15.0 ± 1 ft. (MAB, 4.1.1)

172.75"

Top View  
Detail



Particulate Sampling Probe

Flow Rate Measurement System Probe

Wet/Dry Probe

Stack Temperature Probe

STEEL Flue Pipe HT 8.458'

8.5 ± 0.5 ft (MAB, 4.1.1)

106.5"

WET BULB/Dry Bulb Probe HT N/A  
(No specifications given)

Stack Temperature Probe HT 8.5'

8.5 ± 0.5 ft (DEQ, 3.2.1)

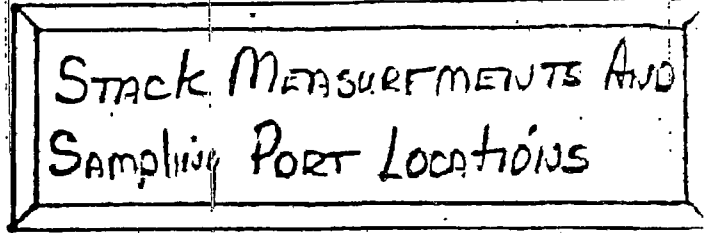
102"

Cutaway Detail on  
Barometric Oil Seal

Stack HT at the flue collar 28.5"

SO<sub>2</sub> Sampling Probe HT N/A

13.5 ft. ± 0.5 ft (MSH, S.1.5.2)



SO<sub>2</sub> Injection Probe HT. N/A

9.5 ft ± 0.5 ft (MSH, S.1.5.1)

Particulate Sampling Probe

HT. N/A 80 ± 0.5 ft (MSH, S.1.2)

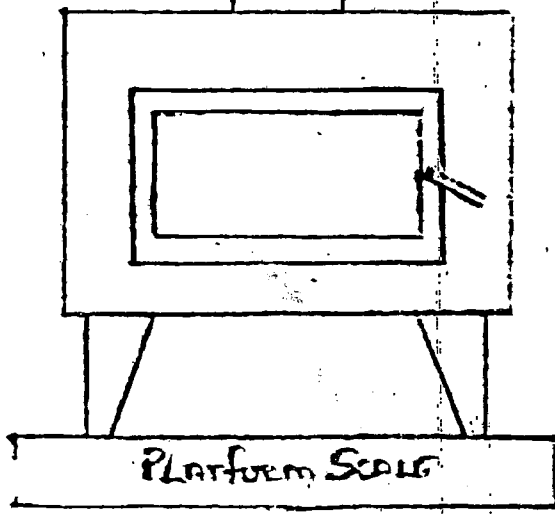
Flow Rate Measurement System Probe

HT. 7.906 7.5 ± 1.0 ft (MSH, S.1.6)

94.875"

Static Pressure Probe HT

< 1.0 ft above flue connector (MAB, 6.2)



Platform Scale

Unit Kama Ashwood

DATE 2/16/09

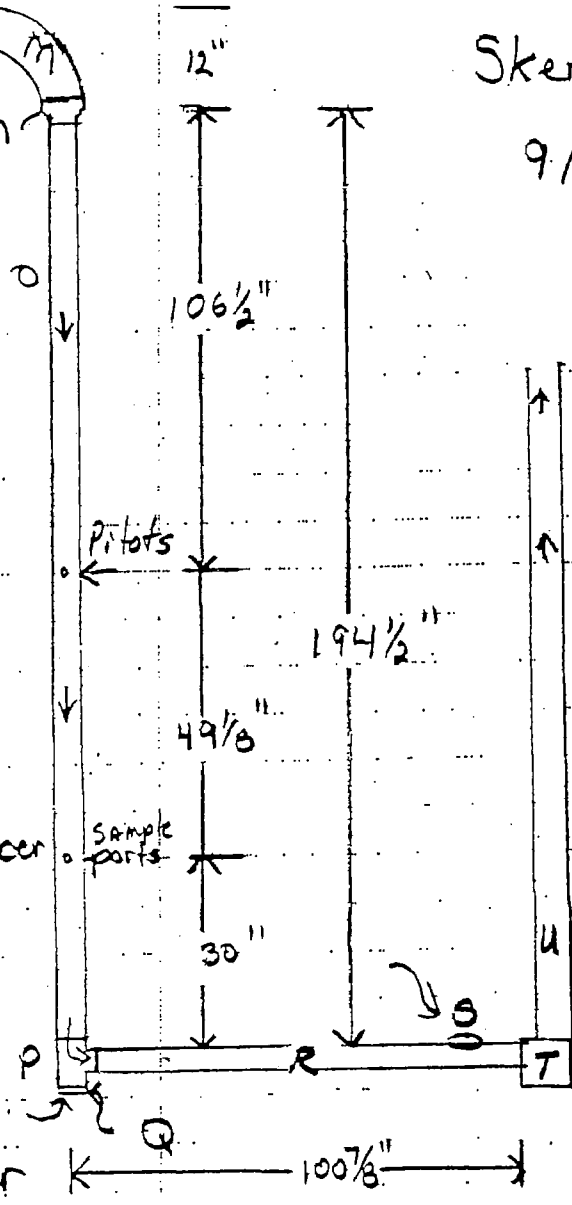
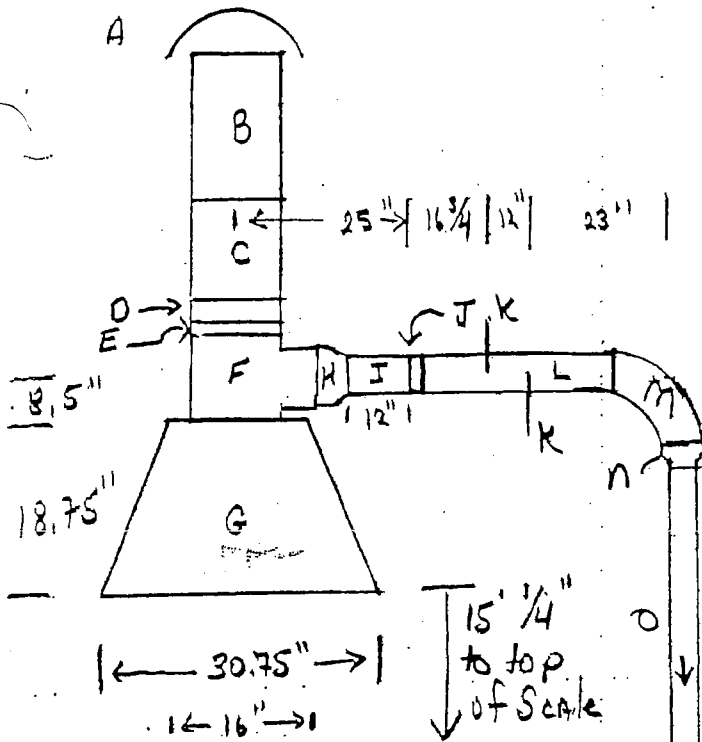
Technician ATM JRP

MYREN  
CONSULTING  
INC

Dilution TUNNEL

Schematic

9/9/97



- A: Class A Rain Cap
- B: 36" of 10" ID Class A Chimney
- C: 18" of 10" ID " " "
- D: Class A
- E: 10" Self-Cleaning Full Closure Blast Gate
- F: 10' 22ga Black Steel Pipe " "
- G: Dilution Tunnel Hood
- H: 10" to 8" Black Steel Pipe Reducer
- I: 12" of 8" Black Steel Pipe
- J: 8" Self-Cleaning Full Closure Blast Gate
- K: Mixing Baffles
- L: 51 3/4" of 8" Black Steel Pipe
- M: 8" 90° Black Steel Pipe Elbow
- N: 8" to 6" Black Steel Pipe Reducer
- O: 194 1/2" of Black Steel Pipe
- P: 6" Black Steel Pipe T Section
- Q: 6" Self-Cleaning Full Closure Blast Gate (for adjusting flows)
- R: 100 7/8" 6" Black Steel Pipe
- S: 2 1/4" diameter Bleed Hole
- T: Dayton Blower
- U: 6" Black Steel Pipe (Exhaust)

NOT TO SCALE

Dimensions shown are actual

TOTAL TUNNEL Length = 22.635'

# Myren Consulting, Inc.

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Colville, WA 99114

Office: (509) 684-1154      Lab: (509) 685-9458  
Fax: (509) 685-2262      email: <bmyren@plix.com>

---

Date: 14 February 2009

To: John Dupree

From: Ben Myren

RE: Request for a Thirty Day Certification Test Notification  
Waiver for the Kuma Ashwood Noncatalytic Woodheater

Friday Myren Consulting was asked by Mr. Mark Freeman of Kuma Stoves, Inc. if we would be able to conduct a certification test series on the Kuma Ashwood noncatalytic stove that Kuma has been developing and they believe is now ready for certification testing. R&D test results at our lab confirm this. So we are ready to start the certification series. Myren Consulting has the time available to conduct the test series, so granting the waiver would be beneficial to all parties, especially since the HPBA Expo is just a little over a month away. We would like to start the EPA test series on the Kuma unit starting on Monday, February 16, 2009 and then finish the series as quickly as possible. I intend to call to confirm the arrival of this fax and that the waiver has been granted. I am also emailing you this waiver request.

Regards and Thank You, Ben Myren

\* \* \* COMMUNICATION RESULT REPORT ( FEB.16.2009 10:57AM ) \* \* \*

FILE MODE	OPTION	ADDRESS (GROUP)	TTI RESULT	PAGE
675 MEMORY TX		101081112025640050	OK	P. 1/1

## REASON FOR ERROR

E-1) HANG UP OR LINE FAIL  
E-3) NO ANSWER

E-2) BUSY  
E-4) NO FACSIMILE CONNECTION

**Myren Consulting, Inc.**

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EPA WEIGHTED AVERAGES CALCULATIONS  
EPA WEIGHTED AVERAGE PARTICULATE EMISSION RATE

The weighted average particulate emission rate ( $\overline{PM}$ ) for the  
KUMA ASHWOOD NONCATALYTIC WOOD HEATER  
manufactured by KUMA STOVES, INC.  
of Hayden, ID is 3.50 g/hr.

EPA WEIGHTED AVERAGE OVERALL EFFICIENCY

The weighted average overall efficiency ( $\overline{OE}$ ) for the  
KUMA ASHWOOD is (default) 63 %.

II. EPA TEST RESULTS

\* Denotes runs used in weighted average calculations

Run #	Dry Burn Rate/kg/hr	Grams/Hour	Overall Efficiency
4	0.947	4.5244	
7	1.059	2.8534	
6	1.199	2.9311	
2	1.433	2.3332	
1	2.332	4.7518	
3 <sup>1</sup>	1.233	1.7596	
5 <sup>2</sup>	1.102	4.6078	

III. EPA CUMULATIVE PROBABILITY CALCULATIONS

$$P_n = \frac{[\text{Hi Prob.} - \text{Low Prob.}][\text{Act. Dry Burn Rate} - \text{Low Dry Burn Rate}]}{.05} + \text{Low Prob.} = P_n$$

$$P_1 = \frac{[.328 - .300][.947 - .900]}{.05} + .300 = .32632$$

$$P_2 = \frac{[.460 - .407][1.059 - 1.050]}{.05} + .407 = .41654$$

$$P_3 = \frac{[.550 - .490][1.199 - 1.150]}{.05} + .490 = .54880$$

$$P_4 = \frac{[.722 - .695][1.433 - 1.400]}{.05} + .695 = .71282$$

$$P_5 = \frac{[.951 - .945][2.332 - 2.300]}{.05} + .945 = .94884$$

$$P_6 = \frac{[ - ] [ - ]}{.05} + =$$

$$P_7 = \frac{[ - ] [ - ]}{.05} + =$$

$$P_8 = \frac{[ - ] [ - ]}{.05} + =$$

$$P_9 = \frac{[ - ] [ - ]}{.05} + =$$

$$P_{10} = \frac{[ - ] [ - ]}{.05} + =$$

$$P_{11} = \frac{[ - ] [ - ]}{.05} + =$$

$$P_{12} = \frac{[ - ] [ - ]}{.05} + =$$

$$P_{13} = \frac{[ - ] [ - ]}{.05} + =$$

$$P_{14} = \frac{[ - ] [ - ]}{.05} + =$$

$$P_{15} = \frac{[ - ] [ - ]}{.05} + =$$

$K_1 = P_2 - P_0 =$	<u>.41654</u>	-	<u>.000</u>	=	<u>.41654</u>
$K_2 = P_3 - P_1 =$	<u>.54880</u>	-	<u>.32632</u>	=	<u>.22248</u>
$K_3 = P_4 - P_2 =$	<u>.71282</u>	-	<u>.41654</u>	=	<u>.29628</u>
$K_4 = P_5 - P_3 =$	<u>.94884</u>	-	<u>.54880</u>	=	<u>.40004</u>
$K_5 = P_6 - P_4 =$	<u>1.0000</u>	-	<u>.71282</u>	=	<u>.28718</u>
$K_6 = P_7 - P_5 =$	_____	-	_____	=	_____
$K_7 = P_8 - P_6 =$	_____	-	_____	=	_____
$K_8 = P_9 - P_7 =$	_____	-	_____	=	_____
$K_9 = P_{10} - P_8 =$	_____	-	_____	=	_____
$K_{10} = P_{11} - P_9 =$	_____	-	_____	=	_____
$K_{11} = P_{12} - P_{10} =$	_____	-	_____	=	_____
$K_{12} = P_{13} - P_{11} =$	_____	-	_____	=	_____
$K_{13} = P_{14} - P_{12} =$	_____	-	_____	=	_____
$K_{14} = P_{15} - P_{13} =$	_____	-	_____	=	_____
$K_{15} = P_{16} - P_{14} =$	_____	-	_____	=	_____

#### IV. EPA WEIGHTED AVERAGES CALCULATIONS

The following formula is the one set out in Equation 28-1, Section 8.1, Method 28 and is to be used to calculate both the weighted average particulate emission rate (PM) and the weighted average overall efficiency (OE) as shown below. The formula uses interpolated probabilities for a given heat output demand calculated from the values listed in Table 28-1(2) in Method 28.

$$\overline{PM} = \frac{K_1 PM_1 + K_2 PM_2 + K_3 PM_3 + \dots + K_n PM_n}{K_1 + K_2 + K_3 \dots + K_n}$$



Unit: Kuma Ashwood

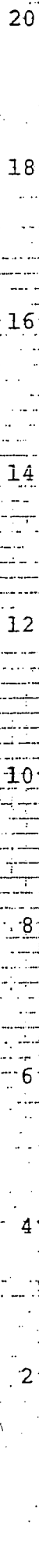
Non Catalyst Cap

Catalyst Cap

KEY:  $\odot$  = CERTIFICATION TEST

$\triangle$  = EAP CONFIRMATION TEST

Particulate Emissions (grams/hr.)



Woodstove Data Summary

Run #	4	7	6	2	1	3	5 <sup>2</sup>
<u>Particulate Emissions:</u>							
Concentration: grains/dscf:							
grams/m <sup>3</sup> :							
Emission Rate: grams/hr:							
Emission Factor: gms/kg:							
(dry fuel weight basis)							
Front Half Catch: % of total							
Total Mass Captured:							
Frt & Bck Halves:							
<u>Efficiency Values:</u>							
Overall Appliance Efficiency							
Combustion Efficiency							
Heat Transfer Efficiency							
<u>Heat Output:</u>							
Avg. BTU/hr for test cycle (EPA)	11,420	12,765	14,460	17,275	28,120	14,866	13,223
<u>Fuel Burn Rates:</u>							
Avg Kg/hr for test cycle (Wet basis)	1.132	1.273	1.449	1.724	2.809	1.478	1.319
Avg Kg/hr for test cycle (Dry basis)	0.947	1.059	1.199	1.433	2.332	1.233	1.102

Notes: 1 = Run 3 = Fan Confirmation Test  
 2 = Run 5 was replaced by 6 & 7

	4	7	6	2	1	3	5
<u>Fuel Moisture Content:</u>							
Kindling (Wet basis)	8.606	7.345	7.593	7.749	8.369	8.523	7.905 %
Pretest Fuel (Wet basis)	17.487	17.168	17.501	17.301	17.022	17.781	17.305 %
Test Fuel (Wet basis)	16.309	16.838	17.262	16.921	16.976	16.602	16.449 %

<u>Air/Fuel Ratio:</u>							
lbs air/lbs fuel							
<u>Average Stack Gas Composition:</u>							
Avg. % CO <sub>2</sub>							%
Avg. % O <sub>2</sub>							%
Avg. % CO							%
Avg. % Excess Air							%
Avg. % Moisture							%

<u>Average Stack Gas Flow Rate:</u>							
Stack flow rate - EPA CMB							dscfm
CHO balance							dscfm
Tracer Gas							dscfm
Draft (Static)	-0.32	-0.38	-0.41	-0.43	-0.61	-0.41	-0.37 in. H <sub>2</sub> O
Proportionality - Average	96.592	97.453	100.111	95.756	95.983	96.974	98.033

<u>Average Stack Gas Emission Factors:</u>							
CO - g/Kg							
g/hr							

	4	7	6	2	1	3	5
<b>Average Temperatures:</b>							
Stack Gas	228	264	289	298	480	271	238 OF
Primary Combustion Chamber Gas	691	741	776	851	990	809	731 OF
Secondary Combustion Chamber Gas	959	1013	1035	1102	1219	1062	971 OF
Catalytic Combustor Exit Gas	N/A	N/A	N/A	N/A	N/A	N/A	N/A OF
Stove Top	469	493	520	587	627	576	488 OF
Stove Left Sidewall	428	460	478	522	541	505	480 OF
Stove Back	310	347	353	414	329	379	344 OF
Stove Right Sidewall	420	444	457	508	513	487	435 OF
Stove Bottom	290	301	310	340	302	326	306 OF
Stove Temperature Change	-11.2	-100.6	-91.4	-63.8	-97.0	-86.8	-89.0 OF
<b>Test Chamber Environment:</b>							
Avg. Barometric Pressure	28.521	28.138	28.728	28.224	28.153	28.511	28.551 in Hg
Avg. Temperature	80	77	75	82	81	77	79 OF
Avg. % Ambient Moisture	1.175	1.20	1.00	1.05	1.175	.875	1.10 % H <sub>2</sub> O
Avg. % Relative Humidity	42.0	43.5	33.5	33.0	37.5	52.0	34.5 %RH
Avg. Air Velocity	00.0	00.0	00.0	00.0	00.0	00.0	00.0 m/sec
Avg. Dilution Tunnel Draft (If Applicable)	.000	.000	.000	.000	.000	.000	.000 in/H <sub>2</sub> O
<b>Test Fuel Weight and Burn Time:</b>							
Density (Dry basis)	0.3685	0.4546	0.4704	0.4265	0.4329	0.3748	0.4213 gm/cm <sup>3</sup>
Coal Bed Weight	3.3	2.9	2.7	3.1	2.8	2.9	3.0 lbs.
Pre Test Fuel Wt (Inc Kindling)	40.658	40.726	41.478	40.252	43.048	38.510	40.716 lbs.
Test Fuel Load Weight	13.808	13.330	13.214	13.306	13.210	13.308	13.332 lbs.
Total Test Cycle Burn Time	320	285	250	210	128	245	275 min.





MYREN CONSULTING CERTIFICATION TEST DATA

DILUTION TUNNEL CALCULATIONS

1/25/09, Md=28.56, Bws=4%

6" Tunnel

EPA 4

File Name:

KUMA

Manufacturer:

ASHWOOD

Model Number:

MYREN

Lab Name:

2/19/09

Test Date:

EPA 4

Run Number:

1.0177

Meter Box Y Factor:

28.521

Barometric pressure (in):

90

Gas meter temp (ave):

0.900

delta H(ave):

288.4130

Gas meter initial reading:

457.0270

Gas meter final reading:

5

Front catch (acetone) mg:

51.8

first filter catch (mg):

-0.3

second filter catch (mg):

139.094

Tunnel Flow (Qsd) (dscfm):

2.996

Emission Rate(g/hr):

4.524

Emission Rate(M5H) :

0.1994

Avg. of Delta P Sq. Roots:

814.153

Vs (Avg.)(ft/min):

94.939

Tunnel Avg. Temperature (F):

320

Test time(min):

13.308

Fuel Load(lb. wet):

16.309

Wood moisture(%wet):

0.947

Burn rate(dry kg/hr):

157.403

Sample Volume (dscf)

0.1603

Avg. Tunnel Static (-inch H2O):

0

Room Blank Catch (mg/dscf):

3.1625

Emission Factor (g/kg):

0.97411

Pitot Correction Factor:

712

front filter number

711

back filter number

24

Beaker Number:

PRELIMINARY RESULTS

FINAL RESULTS:

AUDITED

ASHWOOD

EPA 4

2/19/09

0.947

4.5244

3.1625

96.592

EMISSION RATE (g/hr)(M5H)

EMISSION FACTOR (g/kg):

AVG. % PROPORTIONALITY:

Run Time (min)	PITOT DELTAP (- INCH H2O)	TNL TEMP (°F)	GAS METER RDG (ft3)	GAS METER TEMP (°F)	GAS METER DELTA H (in.H2O)	TUNNEL VELOCITY (ft/min)	PROP RATE (%)	dDGM vol std (ft3)	Tunnel Static (- Inch H2O)	SQUARE ROOT DELTA P	DRY GAS METER RDG (m3)
0	0.041	97	288.4130	72	0.900	850.45			0.161	0.2025	
10	0.039	106	293.7030	75	0.900	836.12	105.3	5.074	0.157	0.1975	
20	0.040	98	298.9510	78	0.900	840.76	101.3	5.006	0.153	0.2000	
30	0.040	96	304.1800	81	0.900	839.25	99.6	4.960	0.154	0.2000	
40	0.039	98	309.3890	84	0.900	830.19	99.6	4.914	0.153	0.1975	
50	0.039	99	314.6090	86	0.900	830.93	99.1	4.907	0.154	0.1975	
60	0.039	99	319.8170	88	0.900	830.93	98.2	4.877	0.153	0.1975	
70	0.039	99	325.0480	89	0.900	830.93	98.3	4.890	0.154	0.1975	
80	0.040	99	330.2800	90	0.900	841.52	96.7	4.882	0.154	0.2000	
90	0.039	98	335.5320	90	0.900	830.18	98.2	4.901	0.151	0.1975	
100	0.041	98	340.7890	91	0.900	851.22	95.5	4.896	0.161	0.2025	
110	0.041	96	346.0520	92	0.900	849.69	95.1	4.893	0.162	0.2025	
120	0.041	96	351.3220	92	0.900	849.69	95.2	4.900	0.163	0.2025	
130	0.041	94	356.6010	92	0.900	848.16	95.2	4.908	0.163	0.2025	
140	0.042	93	361.8750	92	0.900	857.67	93.9	4.903	0.163	0.2049	
150	0.041	93	367.1600	92	0.900	847.39	95.3	4.914	0.162	0.2025	
160	0.041	93	372.4420	92	0.900	847.40	95.2	4.911	0.163	0.2025	
170	0.040	94	377.7300	92	0.900	837.75	96.6	4.916	0.163	0.2000	
180	0.040	94	383.0100	92	0.900	837.75	96.4	4.909	0.164	0.2000	
190	0.040	94	388.3000	93	0.900	837.75	96.3	4.909	0.163	0.2000	
200	0.040	94	393.5780	93	0.900	837.00	96.0	4.898	0.162	0.2000	
210	0.040	93	398.8690	93	0.900	837.00	96.2	4.910	0.163	0.2000	
220	0.040	93	404.1520	93	0.900	837.00	96.0	4.903	0.163	0.2000	
230	0.040	93	409.4480	93	0.900	836.24	96.2	4.915	0.163	0.2000	
240	0.040	92	414.7340	93	0.900	836.24	96.0	4.906	0.164	0.2000	
250	0.040	92	420.0260	93	0.900	836.24	96.1	4.911	0.163	0.2000	
260	0.040	92	425.3050	93	0.900	836.24	95.9	4.899	0.162	0.2000	
270	0.040	92	430.5960	93	0.900	836.24	96.1	4.910	0.163	0.2000	
280	0.040	92	435.8770	93	0.900	836.24	95.9	4.901	0.163	0.2000	
290	0.040	92	441.1670	93	0.900	836.24	96.1	4.909	0.163	0.2000	
300	0.040	92	446.4600	93	0.900	835.48	96.1	4.912	0.164	0.2000	
310	0.040	91	451.7380	93	0.900	835.48	95.8	4.898	0.163	0.2000	
320	0.040	91	457.0270	93	0.900	763.38	87.7	4.900	0.164	0.2000	
330			-0.0000			0.00	0.0	0.000		0.0000	
340			0.0000			0.00	0.0	0.000		0.0000	
350			0.0000			0.00	0.0	0.000		0.0000	
360			0.0000			0.00	0.0	0.000		0.0000	
370			0.0000			0.00	0.0	0.000		0.0000	
380			0.0000			0.00	0.0	0.000		0.0000	

METHOD 5G

PARTICULATE SAMPLING DATA

Rev. 2/09

DATE: 2/19/09 PAGE 1 OF 2 UNIT: Kuma Ashwood RUN: EPA 4

METER BOX: 45G-P METER Y: 1.0177 FILTER #'S: (F) 712 (R) 711

.208/.2085  
PRE TEST LEAK CHECK: .0005 CFM @ -15.5 IN HG FILTER SIZE: 110 mm

1079/1080  
POST TEST LEAK CHECK: 1001 CFM @ -15.0 IN HG PROBE LENGTH 21.0 IN

CLOCK	TIME ELAPSED	METER READING (FT <sup>3</sup> )	PITOT		TUNNEL TEMP (°F)	METER TEMP (°F)	GAS METER Δh	VAC (in Hg)
			ΔP	Pg				
1240	00	288.413	.041	-161	97	72	0.90	00
	50	293.703	.039	-157	106	75	1.90	0
1300	20	298.951	.040	-153	98	78	1.90	0
	10	304.180	.040	-154	98	81	1.90	0
	20	309.389	.039	-153	96	84	1.90	0
	30	314.609	.039	-154	99	86	1.90	0
	40	319.817	.039	-153	99	88	1.90	0
	50	325.048	.039	-154	99	89	1.90	0
1400	80	330.280	.040	-154	99	90	1.90	0
	10	335.532	.039	-157	98	90	1.90	0
	20	340.789	.041	-161	98	91	1.90	0
	30	346.052	.041	-162	96	92	1.90	0
	40	351.322	.041	-163	96	92	1.90	0
<del>1500</del>	30	356.601	.041	-163	94	92	1.90	0
1500	40	361.875	.042	-163	93	92	1.90	0
	10	367.160	.041	-162	93	92	1.90	0
	20	372.442	.041	-163	93	92	1.90	0
	30	377.730	.040	-163	94	92	1.90	0
	40	383.010	.040	-164	94	92	1.90	0
	50	388.300	.040	-163	94	93	1.90	0

BP

00	28.55	300	28.50
60	28.54	320	28.495
120	28.53		
180	28.52		
240	28.51		
AVG. = 28.521			

Pre Test Filter  
Check Weighing  
F .6892  
R .6658

End of Test Weight  
F .7420 R .6658  
.6892 .6656  
532 .0002

METHOD 5G

PARTICULATE SAMPLING DATA

Rev. 2/09

DATE: 2/19/09 PAGE 2 OF 2 UNIT: Kuma Ashwood RUN: EPA 4

METER BOX: 45G-P METER Y: 1.0177 FILTER #'S: (F) 712 (R) 711

209/12045  
PRE TEST LEAK CHECK: .0005 CFM @ -15.5 IN HG FILTER SIZE: 110 mm

POST TEST LEAK CHECK: .001 CFM @ -15.0 IN HG PROBE LENGTH 21.0 IN

TIME		METER READING (FT <sup>3</sup> )	PITOT		TUNNEL TEMP (°F)	METER TEMP (°F)	GAS METER Δh	VAC (in Hg)
CLOCK	ELAPSED		ΔP	Pg				
1600	200	393.578	1040	-1162	94	93	190	0
10	10	398.869	1040	-1163	93	93	190	0
20	20	404.152	1040	-1163	93	93	190	0
30	30	409.448	1040	-1163	93	93	190	0
40	240	414.734	1040	-1164	92	93	190	0
50	50	420.026	1040	-1163	92	93	190	0
1700	60	425.305	1040	-1162	92	93	190	0
10	70	430.596	1040	-1163	92	93	190	0
20	80	435.877	1040	-1163	92	93	190	0
30	90	441.167	1040	-1163	92	93	190	0
40	300	446.460	1040	-1164	92	93	190	0
50	10	451.738	1040	-1163	91	93	190	0
1800	20	457.027	1040	-1164	91	93	190	0
	30							
	40							
	50							
	60							
	70							
	80							
	90							

BP

00	28.55	300	28.50
60	28.54	320	28.495
120	28.53		
180	28.52		
240	28.51		
AVG. = 28.521			

Pre Test Filter  
Check Weighing  
F 1.6892  
R 1.6658

End of Test Weight  
F 1.6892 R 1.6656

MYREN CONSULTING, INC.

Dilution Tunnel Traverse Data with 8 Traverse Points

Unit: KUMMA Ashwood

Run #: EPA 4

Date: 2/19/09

Technicians:

Rev 4/2/08

Point	Location	Ap	$\sqrt{\Delta p_{trav}}$	$\Delta p$	$\sqrt{\Delta p_{cent}}$	T <sub>trav</sub>	T <sub>cent</sub>	Pg
W-1	0.5'	<u>1034</u>	<u>.1844</u>	<u>1040</u>	<u>.2000</u>	<u>106</u>		
2	1.5	<u>1039</u>	<u>.1975</u>	<u>1040</u>	<u>.2000</u>	<u>105</u>	<u>104</u>	<u>-157</u>
Center	Center							
3	4.5	<u>1040</u>	<u>.2000</u>	<u>1040</u>	<u>.2000</u>	<u>102</u>		
4	5.5	<u>1036</u>	<u>.1949</u>	<u>1040</u>	<u>.2000</u>	<u>102</u>		
S-1	0.5	<u>1036</u>	<u>.1897</u>	<u>1040</u>	<u>.2000</u>	<u>101</u>		
2	1.5	<u>1040</u>	<u>.2000</u>	<u>1040</u>	<u>.2000</u>	<u>100</u>	<u>100</u>	<u>-160</u>
Center	Center							
3	4.5	<u>1040</u>	<u>.2000</u>	<u>1040</u>	<u>.2000</u>	<u>99</u>		
4	5.5	<u>1037</u>	<u>.1924</u>	<u>1040</u>	<u>.2000</u>	<u>99</u>		
Totals			<u>1.5589</u>		<u>.4000</u>	<u>914</u>	<u>204</u>	<u>-1317</u>
Average			<u>.19406</u>		<u>.2000</u>	<u>101.75</u>	<u>102</u>	<u>-1585</u>
						<u>501.75</u>	<u>5625</u>	

$^{\circ}R = (^{\circ}F + 460)$

$Ps = BP + (-Pg/13.6) = 28.55 + (-1585/13.6) = 28.538$

LEAK CHECKS:

Pre Test: Pg Leg:  ARP Velocity Head Leg:  ARP

Post Test: Pg Leg:  ARP Velocity Head Leg:  ARP

Rev 4/19/08

DILUTION TUNNEL GAS VELOCITY & VOLUMETRIC FLOW RATE CALCULATIONS

UNIT: Kumar Ashwood DATE: 2/19/09 RUN #: EPA 4 TECHNICIAN(S): ATM JRP  
PDF

Average Gas Velocity in the Dilution Tunnel  $V_{strav}$  (EPA M2 EQN 2-9, ASTM E 2515-07 EQN 7)

$$(9) V_{strav} = (85.49) (0.99 \text{ cp}) (19406) \times \sqrt{\Delta P \text{ "H}_2\text{O}} = \frac{561.75}{(0)} \text{ Ts } ^\circ\text{A} = 13,691.59 \text{ fps}$$

$$(9A) V_s = (13,691.95 \text{ fps}) (60) = \frac{821,495}{(2)} \text{ fpm}$$

Gas Velocity in the Center of the Dilution Tunnel -  $V_{scent}$  (EPA M2 EQN 2-9, ASTM E 2515-07 EQN 7)

$$(9) V_{scent} = (85.49) (0.99 \text{ cp}) (2000) \times \sqrt{\Delta P \text{ "H}_2\text{O}} = \frac{562}{(0)} \text{ Ts } ^\circ\text{A} = 14,055.87 \text{ fps}$$
  
$$(2) (28.56 \text{ lb./ lb. mole}) (2) = 14,055.87 \text{ (2)}$$

$$(9A) V_s = (14,055.87 \text{ fps}) (60) = \frac{843,352}{(2)} \text{ fpm}$$

EPA M5G1 Section 4.2.2, ASTM E 2515-07 EQN 1 Adjustment Factor for Center of Tunnel Pitot Tube Location

$$F_p = V_{strav} / V_{scent} = \frac{13,691.95}{14,055.87} = 0.97411$$

Average Stack Gas Dry Volumetric Flow Rate -  $Q_{sd}$  (EPA M2 EQN 2-10, ASTM E 2515-07 EQN 3)

$$(10) Q_{sd} = 3600 (1 - 0.04 \text{ Bws}) (13,691.59 \text{ fps}) (1963 \text{ ft}^2) [(528 \text{ } ^\circ\text{A}) (28.538 \text{ Ps "Hg}) / (561.75 \text{ Ts } ^\circ\text{A}) (29.92 \text{ "Hg}) = \frac{8327.233}{(2)} \text{ dscfh (or dscfm)}$$

$$(10A) \frac{8327.233}{(1)} \text{ dscfh} \div 60 = \frac{138.787}{(1)} \text{ dscfm (or dscfm)}$$

Note: Number in { } under blank lines denotes number of decimals to be used. If a blank calls for an answer already calculated, use the number of decimals previously specified for that answer.

WOODSTOVE DATA SHEET #4-1: INITIAL FILTER WEIGHTS. (TARE WEIGHTS)

Into Dessicator: Date 1-20-09 Time 1149 By PDG Front Half X Back Half X

Manufacturer: Pall P/N. 60115 Size: 110 Lot.No.: 70726 Grade: A/E Glass

Filter #	First Wt	2009 Date	Time	By	Second Wt	Date	Time	By	Third Wt	2009 Date	Time	By
700	.6873	1-22	1331	GRP	.6877	1-23	1417	PDG				
701	.6871		1330	GRP	.6878		1419	PDG	.6877	1-26	1421	GRP
702	.6816		1329	GRP	.6825		1420	PDG	.6824	1-26	1420	GRP
703	.6761		1328	GRP	.6762		1421	PDG				
704	.6727		1327	GRP	.6732		1422	PDG				
705	.6833		1326	GRP	.6837		1423	PDG				
706	.6946		1325	GRP	.6948		1424	PDG				
707	.6773		1324	GRP	.6777		1425	PDG				
708	.6701		1323	GRP	.6702		1426	PDG				
709	.6799		1322	GRP	.6809		1427	PDG	.6806	1-26	1419	GRP
710	.6587		1321	GRP	.6590		1428	PDG				
711	.6654		1320	GRP	.6656		1429	PDG				
712	.6678		1319	GRP	.6692		1430	PDG				
713	.6864		1318	GRP	.6866		1431	PDG				
714	.6651		1318	GRP	.6655		1432	PDG				
715	.6741		1317	GRP	.6744		1433	PDG				
716	.6592		1316	GRP	.6590		1434	PDG				
717	.6531		1315	GRP	.6536		1435	PDG				
718	.6621		1314	GRP	.6623		1436	PDG				
719	.6769		1313	GRP	.6769		1437	PDG				
720	.6627		1312	GRP	.6628		1438	PDG				
721	.6567		1311	GRP	.6569		1439	PDG				
722	.6539		1310	GRP	.65340		1440	PDG				
723	.6552		1309	GRP	.6552		1441	PDG				
724	.6655		1308	GRP	.6656		1442	PDG				

Checked by ATM Date: 1/27/09 Time 1632

QA REWEIGH

Filter #	WT	Date	Time	By
703	.6761	1/27/09	1639	ATM
708	.6705		1640	ATM
715	.6744	V	1642	ATM

BALANCE ROOM ENVIRONMENTAL CONDITIONS

WB	DB	%RH	Date	Time	By
57	72	38	1-22-09	1138	ATM
58	25	33	1-23-09	1150	PDG
56	76	25	1-26-09	1559	GRP
58	72	31	1/27/09	1530	PDG

Post P-22 1.26 0.0000 99.9994  
 0.0000 0.0000 0.0000 0.0000  
 100.0000 99.9994 99.9993 99.9993

WOODSTOVE DATA SHEET #4-2:  
INITIAL BEAKER WEIGHTS (TARE WEIGHTS)

Blank done 12/9/07

Into Dessicator: Date: 10/12/07 Time: 0801 By: GRP

Beaker #	First Wt	Date	Time	By	Second Wt	Date	Time	By	Third Wt	Date	Time	By
22	71.8343	10/22/07	1358	GRP	71.8332	11/10/07	1938		71.8330	11-11-07	1746	Jm
24	73.2192		1400	GRP	73.2190	11/10/07	1940		73.2193	11-11-07	1746	Jm
25	72.6516		1401	GRP	72.6512	11/10/07	1944		← Blank			
26	71.7895		1403	GRP	71.7888	11/10/07	1939		71.7886	11-11-07	1747	Jm
27	72.3316		1402	GRP	72.3314	11/10/07	1945					
28	70.5979		1404	GRP	70.5975	11/10/07	1941		70.5977	11-11-07	1745	Jm
39	53.1508		1405	GRP	53.1500	11/10/07	1942					
37	53.7237	11/10/07	1945	ATM	53.7238	11/11/07	1743					Jm

Checked By: \_\_\_\_\_ Date: \_\_\_\_\_ Time: \_\_\_\_\_

QA REWEIGH

Beaker #	WT	Date	Time	By
27	72.3315	11-11	1740	Jm
25	72.6515	11-11	1741	Jm
39	53.1509	11-11	1744	Jm

Post weighing  
0.0000g

1st  
0.0000  
2nd

BALANCE ROOM ENVIRONMENTAL CONDITIONS

WB	DB	%RH	Date	Time	By
57	68	50	10/22/07	1344	GRP
			11/10		







WOODSTOVE DATA SHEET 4-4 SCALE QC RECORD SHEET

SCALE: SARTORIUS  
 MODEL: CP224S  
 SN: 17050374

FROM: 9/27/2007  
 THROUGH: 12/7/2007

Level	Recali	130 g	100 g	10 g	1.0 g	100 mg	20 mg	Date	Time	Tech	Wet Bulb	Dry Bulb	% RH
✓	N	129.9998	99.9998	10.0000	1.0000	0.1000	0.0199	9/27/07	1402	9RP	55	67	45
✓	Y	129.9995	99.9996	10.0001	1.0000	0.1000	0.0200	9/28/07	1335	9RP	57	69	46
✓	Y	129.9996	99.9996	9.9999	1.0000	0.1000	0.0200	10/1/07	1505	ATM	56	70	48
✓	N	129.9995	99.9996	10.0000	1.0000	0.1000	0.0199	10/2/07	1611	9RP	56	68	46
✓	N	129.9997	99.9997	9.9999	1.0000	0.1000	0.0199	10/3/07	122	9RP	56	68	46
✓	N	129.9996	99.9996	10.0000	1.0000	0.1000	0.0199	10/4/07	1225	9RP	55	67	45
✓	Y	129.9996	99.9996	10.0000	1.0000	0.1000	0.0199	10/5/07	0750	9RP	51	62	45
✓	N	129.9997	99.9997	9.9999	1.0000	0.1000	0.0199	10/5/07	1513	9RP	56	69	43
✓	Y	129.9996	99.9996	10.0000	1.0000	0.1000	0.0200	10/9/07	305	ATM	50	71	44
✓	N	129.9996	99.9997	10.0000	1.0000	0.1000	0.0200	10/12/07	1259	ATM	50	70	48
✓	Y	129.9995	99.9996	9.9999	1.0000	0.1000	0.0199	10/22/07	1344	9RP	57	68	50
✓	Y	129.9996	99.9997	9.9999	1.0000	0.1000	0.0199	10/29/07	1338	9RP	53	63	50
✓	N	129.9995	99.9995	10.0000	1.0000	0.1000	0.0200	10/30/07	0933	ATM	56	70	40
✓	Y	129.9996	99.9997	10.0000	1.0000	0.1000	0.0199	10/30/07	1457	9RP	55	70	36
✓	Y	129.9996	99.9996	9.9999	1.0000	0.1000	0.0199	10/31/07	1528	9RP	57	75	30
✓	Y	129.9996	99.9996	9.9999	1.0000	0.1000	0.0199	11/2/07	1238	9RP	50	67	33
✓	Y	129.9996	99.9996	10.0000	1.0000	0.1000	0.0199	11/5/07	0730	9RP	57	73	35
✓	Y	129.9996	99.9997	10.0000	1.0000	0.1000	0.0200	11/9/07	1550	ATM	58	70	48
✓	N	129.9996	99.9997	10.0000	1.0000	0.1000	0.0200	11/10/07	1885	ATM	55	71	44
✓	Y	129.9997	99.9997	9.9999	1.0000	0.1000	0.0199	11/11/07	1810	ATM	55	69	39
✓	N	129.9997	99.9996	9.9999	1.0000	0.1000	0.0199	11/21/07	0822	9RP	54	67	41
✓	N	129.9996	99.9996	10.0000	1.0000	0.1000	0.0199	11/27/07	1224	ATM	58	72	41
✓	N	129.9998	99.9997	9.9999	0.9999	0.1000	0.0200	11/14/07	1710	9RP	58	73	39
✓													
✓	Y	129.9997	99.9997	10.0000	1.0000	0.1000	0.0200	11/15/07	1350	ATM	59	72	45
✓	N	129.9996	99.9996	9.9999	0.9999	0.1000	0.0200	11/16/07	1800	9RP	58	71	44
✓	N	129.9996	99.9996	10.0000	1.0000	0.1000	0.0199	11/19/07	1758	ATM	740	74	43
✓	Y	129.9997	99.9997	10.0000	1.0000	0.1000	0.0200	11/19/07	1143	ATM	56	70	40
✓	Y	129.9995	99.9996	10.0000	1.0000	0.1000	0.0199	11/20/07	1416	9RP	54	69	35
✓	N	129.9996	99.9996	10.0000	1.0000	0.1000	0.0200	11/21/07	1110	ATM	57	70	44
✓	N	129.9995	99.9996	10.0000	1.0000	0.1000	0.0199	12/3/07	0730	9RP	55	69	40
✓	N	129.9996	99.9996	10.0000	1.0000	0.1000	0.0200	12/6/07	1125	ATM	54	67	44
✓	Y	129.9996	99.9996	10.0000	1.0000	0.1000	0.0200	12/17/07	1348	9RP	55	69	40

QC Services Audit 11/17/07

WOODSTOVE DATA SHEET 4-4 SCALE QC RECORD SHEET

SCALE: SARTORIUS  
 MODEL: CP224S  
 SN: 17050374

FROM: 12/2/07  
 THROUGH: 2/3/08

Level	Recall	130 g	100 g	10 g	1.0 g	100 mg	20 mg	Weight	Date	Time	Tech	Wet Bulb	Dry Bulb	% RH
✓	N	129.9996	99.9996	10.0000	1.0000	0.1000	0.0200	0.0200	12/8	12:15	ATM	57	73	35
✓	N	129.9996	99.9996	10.0000	1.0000	0.1001	0.0200	0.0200	12/8	19:10	ATM	57	72	38
✓	N	129.9997	99.9996	10.0000	1.0000	0.1000	0.0199	0.0199	12/9	19:35	ATM	55	72	31
✓	Y	129.9996	99.9996	10.0000	1.0000	0.1000	0.0200	0.0200	12/10	19:53	ATM	56	72	34
✓	N	129.9997	99.9997	10.0000	1.0000	0.1000	0.0199	0.0199	12/11	16:18	GRP	57	76	28
✓	N	129.9997	99.9996	10.0000	1.0000	0.0999	0.0199	0.0199	12/12	15:05	GRP	56	74	30
✓	N	129.9996	99.9996	9.9999	0.9999	0.1000	0.0199	0.0199	12/13	13:07	GRP	55	73	29
✓	N	129.9996	99.9996	9.9999	0.9999	0.1000	0.0199	0.0199	12/14	13:21	GRP	57	75	31
✓	N	129.9998	99.9998	9.9999	1.0001	0.1000	0.0199	0.0199	12/15	16:02	GRP	57	75	31
✓	Y	129.9996	99.9997	9.9999	1.0000	0.1000	0.0199	0.0199	12/17	08:17	GRP	55	73	29
✓	N	129.9997	99.9997	10.0000	1.0000	0.1000	0.0199	0.0199	12/18	08:53	GRP	58	75	34
✓	N	129.9997	99.9997	10.0000	1.0000	0.1000	0.0199	0.0199	12/19	08:12	GRP	55	72	31
✓	Y	129.9995	99.9996	10.0000	1.0001	0.0999	0.0199	0.0199	12/20	09:16	GRP	57	71	41
✓	Y	129.9998	99.9997	10.0000	1.0000	0.1000	0.0199	0.0199	12/21	10:85	ATM	55	70	36
✓	N	129.9997	99.9996	10.0000	1.0000	0.1000	0.0200	0.0200	12/22	14:34	ATM	54	66	44
✓	N	129.9996	99.9996	10.0000	1.0000	0.1000	0.0200	0.0200	12/23	09:15	ATM	57	70	44
✓	N	129.9996	99.9996	9.9999	1.0000	0.1000	0.0199	0.0199	12/26	10:30	ATM	57	70	44
✓	N	129.9996	99.9997	10.0000	1.0000	0.1000	0.0200	0.0200	12/27	10:30	ATM	56	72	34
✓	N	129.9997	99.9997	9.9999	1.0000	0.1000	0.0200	0.0200	1/8/08	13:42	GRP	54	68	38
✓	N	129.9997	99.9997	10.0000	1.0001	0.1000	0.0200	0.0200	1/9/08	07:42	GRP	55	70	36
✓	N	129.9997	99.9997	10.0000	1.0000	0.1000	0.0199	0.0199	1/11/08	10:40	ATM	59	73	42
✓	Y	129.9996	99.9997	10.0000	1.0000	0.1000	0.0199	0.0199	1/16/08	12:21	GRP	51	72	18
✓	N	129.9999	99.9998	10.0000	1.0000	0.1000	0.0199	0.0199	1/17/08	12:37	GRP	56	71	37
✓	N	129.9998	99.9998	10.0000	1.0000	0.0999	0.0200	0.0200	1/18/08	11:16	GRP	56	71	37
✓	Y	129.9995	99.9996	9.9999	1.0001	0.1000	0.0199	0.0199	1/21/08	14:26	GRP	56	72	34
✓	N	129.9995	99.9996	10.0000	1.0001	0.1000	0.0199	0.0199	1/22/08	15:13	GRP	56	71	37
✓	Y	129.9996	99.9996	9.9999	1.0000	0.1000	0.0199	0.0199	1/23/08	08:05	GRP	54	69	36
✓	Y	129.9996	99.9996	10.0000	1.0000	0.1000	0.0200	0.0200	1/24/08	07:58	GRP	54	70	33
✓	N	129.9998	99.9997	10.0000	1.0000	0.1000	0.0199	0.0199	1/24/08	14:50	GRP	56	71	37
✓	N	129.9997	99.9996	10.0000	1.0000	0.1000	0.0200	0.0200	1/31/08	15:05	GRP	55	69	38
✓	N	129.9996	99.9996	10.0000	1.0000	0.1000	0.0199	0.0199	2/11/08	10:29	GRP	54	69	36
✓	N	129.9996	99.9996	9.9999	1.0000	0.1000	0.0199	0.0199	2/20/08	16:20	ATM	56	72	41
✓	N	129.9996	99.9997	10.0000	1.0000	0.1000	0.0200	0.0200	2/3/08	17:10	ATM	57	70	44

WOODSTOVE DATA SHEET 4-4 ANALYTICAL BALANCE QC RECORD SHEET  
 SCALE: SARTORIUS  
 MODEL: CP224S  
 SN: 170550374

FROM: 12/30/08  
 THROUGH: 2/17/09

Level	Recall	140 g	100 g	10 g	1.0 g	100 mg	20 mg	Weight	Weight	Date	Time	Tech	Wet Bulb	Dry Bulb	% RH
✓	N	139.9995	99.9995	9.9999	1.0000	0.1000	0.0199	0.0199	12/30/08	1430	ARM	58	72	42	
✓	N	139.9995	99.9995	9.9999	1.0000	0.1000	0.0199	0.0199	12/23/08	1057	GRP	60	76	38	
✓	N	139.9994	99.9994	9.9999	1.0000	0.1000	0.0200	0.0200	12/21/08	1019	ATM	59	72	43	
✓	N	139.9994	99.9994	9.9999	1.0000	0.1000	0.0200	0.0200	12/20/08	1112	ATM	59	72	45	
✓	N	139.9994	99.9994	9.9999	1.0000	0.1000	0.0200	0.0200	01/08/09	1050	ATM	60	75	37	
✓	N	139.9994	99.9994	9.9999	1.0000	0.1000	0.0199	0.0199	10/25/08	1157	PDG	58	75	34	
✓	N	139.9994	99.9994	9.9999	1.0000	0.1000	0.0199	0.0199	1/16/09	1845	ATM	60	75	37	
✓	N	139.9995	99.9995	9.9999	1.0000	0.1000	0.0199	0.0199	1/7/09	1530	GRP	58	70	48	
✓	N	139.9994	99.9994	9.9999	1.0000	0.1000	0.0199	0.0199	1/8/09	1356	PDG	60	72	49	
✓	Yes	139.9993	99.9993	9.9999	1.0000	0.1000	0.0200	0.0200	1/09/09	1023	PDG	58	72	42	
✓	Yes	139.9993	99.9993	9.9999	1.0000	0.1000	0.0199	0.0199	1/11/09	1128	SRP	55	72	31	
✓	Yes	139.9994	99.9994	9.9999	1.0000	0.1000	0.0199	0.0199	1/12/09	0845	PDG	59	75	38	
✓	NO	139.9993	99.9993	9.9999	1.0000	0.1000	0.0200	0.0200	1/13/09	0825	JRP	58	74	37	
✓	Yes	139.9993	99.9993	9.9999	1.0000	0.1000	0.0199	0.0199	1-14-09	1212	PDG	57	72	36	
✓	NO	139.9993	99.9993	9.9999	1.0000	0.1000	0.0199	0.0199	1/14/09	1420	GRP	59	75	37	
✓	Yes	139.9994	99.9994	9.9999	1.0000	0.1000	0.0199	0.0199	1-15-09	1128	GRP	58	74	37	
✓	Yes	139.9993	99.9993	9.9999	1.0000	0.1000	0.0199	0.0199	1-20-09	0950	PDG	58	74	37	
✓	Yes	139.9993	99.9993	9.9999	1.0000	0.1000	0.0199	0.0199	1-20-09	1230	PDG	56	71	37	
✓	NO	139.9994	99.9994	9.9999	1.0000	0.1000	0.0199	0.0199	1-20-09	1613	SRP	57	73	35	
✓	NO	139.9994	99.9994	9.9999	1.0000	0.1000	0.0200	0.0200	1/22/09	1130	ATM	57	72	38	
✓	NO	139.9993	99.9993	9.9999	1.0000	0.1000	0.0199	0.0199	1-23-09	1150	PDG	58	75	35	
✓	YES	139.9992	99.9992	9.9999	1.0000	0.1000	0.0200	0.0200	1-26-09	1359	SRP	56	72	35	
✓	NO	139.9994	99.9994	9.9999	1.0000	0.1000	0.0199	0.0199	1/27/09	1530	PDG	58	72	31	
✓	NO	139.9993	99.9993	9.9999	1.0000	0.1000	0.0200	0.0200	1/28/09	1452	ATM	61	75	41	
✓	YES	139.9993	99.9993	9.9999	1.0000	0.1000	0.0199	0.0199	1-29-09	1436	GRP	58	77	29	
✓	NO	139.9995	99.9995	9.9999	1.0000	0.1000	0.0199	0.0199	1/30/09	1256	PDG	60	72	49	
✓	Yes	139.9993	99.9993	9.9999	1.0000	0.1000	0.0199	0.0199	2/1/09	1200	ATM	59	74	37	
✓	NO	139.9993	99.9993	9.9999	1.0000	0.1000	0.0199	0.0199	2/2/09	1350	GRP	58	77	29	
✓	Yes	139.9995	99.9995	9.9999	1.0000	0.1000	0.0199	0.0199	2/5/09	1118	PDG	59	72	45	
✓	NO	139.9995	99.9995	9.9999	1.0000	0.1000	0.0199	0.0199	2/6/09	1150	GRP	57	74	33	
✓	NO	139.9994	99.9994	9.9999	1.0000	0.1000	0.0200	0.0200	2/9/09	1015	ATM	49	70	19	
✓	NO	139.9994	99.9994	9.9999	1.0000	0.1000	0.0199	0.0199	2/10/09	1501	PDG	61	78	36	
✓	NO	139.9993	99.9993	9.9999	1.0000	0.1000	0.0200	0.0200	2/17/09	1139	JRP	56	72	35	

WOODSTOVE DATA SHEET 4-4 ANALYTICAL BALANCE QC RECORD SHEET

SCALE: SARTORIUS

FROM: 2/10/09  
THROUGH:

MODEL: CP2245  
SN: 17650374

Level	Recali	140 g			100 g			10 g			1.0 g			100 mg			20 mg			Date		Tech	Wet		Dry	
		Weights	Weight	Weight	Weight	Weight	Weight	Weight	Weight	Weight	Weight	Weight	Weight	Weight	Weight	Weight	Weight	Weight	Weight	Bulb	Bulb		% RH	Bulb	Bulb	% RH
Y	Y	139.9993	99.9994	99.9995	9.9999	9.9999	1.0000	0.1000	0.0199	2/10/09	1802	ATM	55	70	26											
Y	Y	139.9993	99.9994	99.9995	9.9999	9.9999	1.0000	0.1000	0.0199	2/10/09	1248	JRP	56	73	32											
Y	Y	139.9993	99.9994	99.9995	9.9999	9.9999	1.0000	0.1000	0.0199	2/20/09	1018	PDB	57	74	33											
Y	Y	139.9993	99.9994	99.9995	9.9999	9.9999	1.0000	0.1000	0.0200	2/21/09	1519	ATM	60	77	35											
Y	Y	139.9993	99.9994	99.9995	9.9999	9.9999	1.0000	0.1000	0.0199	2/23/09	1223	ATM	47	59	37											
Y	Y	139.9994	99.9994	99.9995	9.9999	9.9999	0.9999	0.1000	0.0199	2/23/09	1406	PDB	58	70	48											
Y	No	139.9994	99.9994	99.9995	9.9999	9.9999	1.0000	0.1000	0.0200	2/24/09	0953	ATM	59	76	35											
Y	Yes	139.9995	99.9995	99.9995	9.9999	9.9999	1.0000	0.1000	0.0199	2/25/09	1223	PDB	60	76	38											
Y	Yes	139.9994	99.9994	99.9995	9.9999	9.9999	1.0000	0.1000	0.0199	2/26/09	1258	JRP	55	70	36											
Y	Yes	139.9993	99.9993	99.9993	9.9999	9.9999	1.0001	0.1001	0.0200	2/29/09	1320	ATM	57	74	33											
Y	Yes	139.9995	99.9995	99.9995	9.9999	9.9999	0.9999	0.1000	0.0199	3/3/09	1431	PDB	59	76	35											
Y	Yes	139.9993	99.9993	99.9995	9.9999	9.9999	1.0000	0.1000	0.0199	3/4/09	1556	JRP	56	70	40											
Y	No	139.9994	99.9994	99.9994	9.9999	9.9999	1.0001	0.1001	0.0200	3/5/09	1350	ATM	60	75	40											
Y	No	139.9993	99.9993	99.9993	9.9999	9.9999	1.0000	0.1000	0.0200	3/7/09	0850	ATM	57	71	41											
Y	Yes	139.9993	99.9993	99.9993	10.0000	10.0000	1.0001	0.1000	0.0200	3/8/09	1323	ATM	55	70	36											
Y	Yes	139.9993	99.9993	99.9993	9.9999	9.9999	1.0000	0.1000	0.0199	3/10/09	1222	PDB	50	75	10											

Woodstove Particulate  
 Catch Processing Sheet  
 Woodstove Data Sheet #5  
 EPA M5G-1

Unit: Kumar Ashwood  
 Run: EPA 4  
 Date: 2/19/09  
 Technicians: ATM  
 Revised 1/16/98-Data Sheet #5

Filters

Filter # (Front) 712 Beaker # 24  
 Final Wt. .7410 g MI 45  
 Tare Wt. .6892 g Desc. Acetone  
 Net Wt. .0518 g

Final Wt. 73.2238 g  
 Tare Wt. 73.2188 g  
 Net Wt. .0050 g

Filter # (Rear) 711 Beaker # \_\_\_\_\_  
 Final Wt. .6653 g MI \_\_\_\_\_  
 Tare Wt. .6656 g Desc. \_\_\_\_\_  
 Net Wt. -.0003 g

Final Wt. \_\_\_\_\_ g  
 Tare Wt. \_\_\_\_\_ g  
 Net Wt. \_\_\_\_\_ g

Acetone Blank Calculation:

Blank Date: 12/8/07

Blank Beaker # 25 Final Wt. 72.6511 g  
 MI 50 Tare Wt. 72.6512 g  
 Desc. Acetone Net Wt. -0.0001 g = 0.0000  
0.0000 g ÷ 50 ml = 0.00000 g/ml

Blank Residue Value Calculation:

0.00000 g/ml acetone X 45 ml acetone = 0.0000 g  
 Blank Residue Value

Total Particulate Catch Calculation

Filter: .0518 g ✓  
 Filter: -.0003 g ✓  
 Beakers: .0050 g - 0.0000 g = .0050 g ✓  
 Total Catch Blank Residue Value  
 Total Catch = .0565 g ✓

Unit Kuma Ashwood  
 Run # EPA 4  
 Date 2/19/09  
 Technician ATM JRP PDL  
 WST6-Form1, Rev8/96

MISCELLANEOUS TEST DATA  
 WOODSTOVE DATA SHEET #8

Useable Firebox Dimensions: See QC Section Useable Volume: 2.094 ft<sup>3</sup>

Dilution Tunnel Draft (If applicable): Start .000 Stop .000 "H<sub>2</sub>O

Test Chamber Air Velocity: Start: 00.0 Stop: 00.0 Avg: 00.0 ft/min

Wet Bulb/ Start: WB: 57 °F DB: 73 °F 1.0 % Amb Moisture 35 %RH

Dry Bulb Stop: WB: 60 °F DB: 72 °F 1.35 % Amb Moisture 49 %RH

$\bar{X} = 1.175$  % Ambient Moisture  $\bar{X} = 42.0$  % Relative Humidity (RH)

Empty Stove Wt: 440.2 lbs.

Empty Stove Wt with Stack (Inc. Oil Seal) Wet: 763.8 lbs. Dry: 763.8 lbs.

Empty Stove Wt with Stack and Ash Ash: — lbs. Total: — lbs.

Kindling Wt. Total 4.8 lbs. Paper: 0.4 lbs. Wood: 4.4 lbs.

Pre Burn Fuel Wt. 11,434 + 13,786 + 10,638 Total: 35,858 lbs.

Total Kindling and Pre Burn Fuel Wt 40.658 lbs.

Coal Bed Wt-lbs: Range (33 - 2.7) 767.1 - 764.5 lbs. Actual: 33 lbs.

Allowable Amount of Charcoal that can be removed:

Coal Bed Wt. Range  $\left( \frac{33}{\text{Upper Wt.}} + \frac{2.7}{\text{Lower Wt.}} \right) / 2 \times .25 = 0.7$  lbs.

Test Fuel Wt-lbs: Ideal 14.7 lbs. Range: 16.1 - 13.2 lbs. Actual: 13,308 lbs.

Test Fuel Size (pcs.) (.75 x 1.5 x 5" Flanges) 16 Pcs.

2 x 4's x 16.375 " 3 Pcs 7.088 lbs. 53.27 %

4 x 4's x 16.375 " 2 Pcs 6.218 lbs. 46.73 %

510512 kg

Est. Dry Burn Rate (Kg/Hr.)  $\frac{13308 - (13308 \times .16309)}{2.2046} \times \frac{60}{320} = 0.9471$  Est. Dry Burn Rate (Kg/Hr)

Est EPA Heat Output (HO<sub>E</sub>) (19,140) x  $\frac{63}{100} \times .9471 = 11,420$  Est Heat Output (HO<sub>E</sub>) BTU's/Hr

Comments: 305 mins = 0.9937 kg/hr



Stove Operating Data  
Woodstove Test Data Sheet #9  
Cold Start

Unit: Kuma Ashwood  
Run: EPD 4  
Date: 2/19/09  
Technician(s): AT Myren  
Data Sheet #9-Rev 1/98-Pg.2

Fire Started: 0:8:46

Warm up and Preburn: Primary Air: Wide open from ignition until the start of preburn when the primary air control(s) was (were) adjusted to the run setting of 0.3655" PAC. At the run setting until the start of the test. 2.3735" Threaded rod

Secondary Air: No Controls, Naturally drafted

Secondary Burn Bypass: N/A

Charcoal Bed Preparation: Broke up, raked and leveled the coal bed prior to the addition of each warm up/pre burn fuel charge. Starting 1:30 before the start of the test, broke up, raked and leveled the coal bed. In stove for 32 seconds.

Test: Door wide open during loading 1 min 15 sec, then closed.

Primary Air: Wide open from the start of the test (0:00) until 4:45. Adjusted to the run setting of 0.3655" between 4:45 and 5:00. At the run setting of 0.3655" open at 5:00 into the run.

Secondary Air: No Controls, Naturally drafted.

Secondary Burn Bypass: N/A

Fan: ON/OFF during the warm up, ON/OFF Low during the preburn, ON/OFF at the start of test, ON/OFF for the first 30 minutes of test, ON/OFF Low at 30 minutes into test, ON/OFF for the rest of test.

Test Run Anomalies:

WOODSTOVE OPERATING DATA  
WOODSTOVE DATA SHEET #9A-1

Wood Data: Kindling: A mix of the below grades

	Size	Mill	Grade	Species
Pre Burn	2X4	Forest Grove	# 2, Std # BTR	D. Fir, Sfc. Oak
Test Fuel	2X4	Forest Grove	# 2, Std # BTR	D. Fir, Sfc. Oak
	4X4	Forest Grove	No. 1	D. Fir, Sfc. Oak

All grades WCLB Rules unless otherwise noted.

Warm up Information:

- 1st Warm up/Pre Burn Fuel charge (11.434 lbs) added at 0906.
- 2nd Warm up/Pre Burn Fuel charge (13.786 lbs) added at 1006.
- 3rd Warm up/Pre Burn Fuel charge (10.638 lbs) added at 1117.
- 4th Warm up/Pre Burn Fuel charge (\_\_\_\_\_ lbs) added at \_\_\_\_\_.
- 5th Warm up/Pre Burn Fuel charge (\_\_\_\_\_ lbs) added at \_\_\_\_\_.
- 6th Warm up/Pre Burn Fuel charge (\_\_\_\_\_ lbs) added at \_\_\_\_\_.
- 7th Warm up/Pre Burn Fuel charge (\_\_\_\_\_ lbs) added at \_\_\_\_\_.
- 8th Warm up/Pre Burn Fuel charge (\_\_\_\_\_ lbs) added at \_\_\_\_\_.

1<sup>st</sup> Rick 4-12" 4-16" 2X4's      3<sup>rd</sup> Rick 4-12", 3-16" 2X4's  
 2<sup>nd</sup> Rick 8-16" 2X4's

The coals were scooped out of the stove immediately prior to adding the 3<sup>rd</sup> pre burn/warm up fuel charge. The stove lost 0 lbs. 20 lbs. of coals were put back in the stove after the scoop.

All pre burn/warm up fuel pieces were either 12 or 16 inches long. All preburn pieces/fuel charges were "ricked" in the stove. The pieces in the bottom layer in each rick contained 2 pcs that were 12 or 16 inches long and were loaded flat and perpendicular to the door. The pieces in the second layer in each rick were loaded on their side (edge) approximately parallel to the door and contained 3 or 4 pcs 16 inches long. The third layer (and fourth layer if present) was loaded flat, perpendicular to the door and contained 2 pcs 12 or 16 inches long. The majority of the pieces in each rick were in the second layer which had an approximate 0.5-1.0" space between pieces. (The loading directions indicate the direction of the longest dimension on each piece relative to the loading door opening.) Each pre burn/warm up fuel charge normally weighs within the weight range allowed for the actual test fuel charge

WOODSTOVE OPERATING DATA  
WOODSTOVE DATA SHEET #9A-2

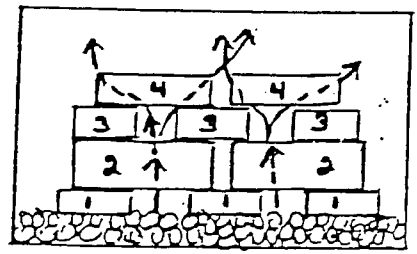
Unit: Kuma Ashwood  
Run # EPA 4  
Date 2/19/09  
Technician ATM  
Page 2 of 5  
WST7-Form2-A, Rev 6/90

Warm up Information (cont.):

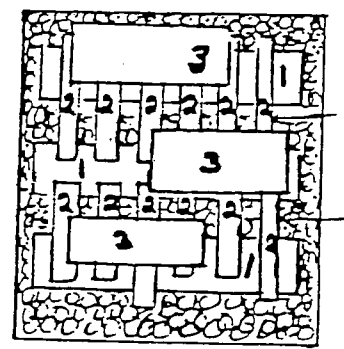
Each warm up/preburn fuel charge was ricked in exactly (as much as possible) the same manner and the weight of each rick was usually within the allowable weight range for the test fuel charge. The physical arrangement and alignment of each rick was designed to accomplish three (3) things: (1) The bottom layer was nestled firmly into the coal bed and was as close to being level with the bottom of the stove as possible, thus providing a stable loading platform for the rest of the rick, keeping it in a ricked state (as opposed to a collapsed or fallen down state) until the rick reached the charcoal stage and sags or collapses of its own accord. (2) It enhances the flow of primary air through the ricked preburn fuel charge, for the primary air would flow through the spaces between the pieces in the first layer and then up through the spaces between the pieces in the second, third and, if present, fourth layers. (3) It maximized, as much as possible, the surface to volume ratio of each preburn fuel charge, thereby allowing the fire immediate access to as much wood surface as possible and, thereby, insuring uniform charcoalization. All three of these enhance combustion and so get the stove as hot as possible during the warm up period, thereby maximizing the amount of heat (BTU's) stored in the stove. The actual preburn was not started until the stove surface temperatures had maximized and stabilized, thus indicating that the amount of heat stored in the stove had peaked. For this stove, the thermal storage was monitored using the Stove Top T/C

758  
948  
1044

surface temperature(s) and the peak value(s) obtained were 1044 OF.



Front View



Top View

The arrows indicate the direction of the air flow through the rick.

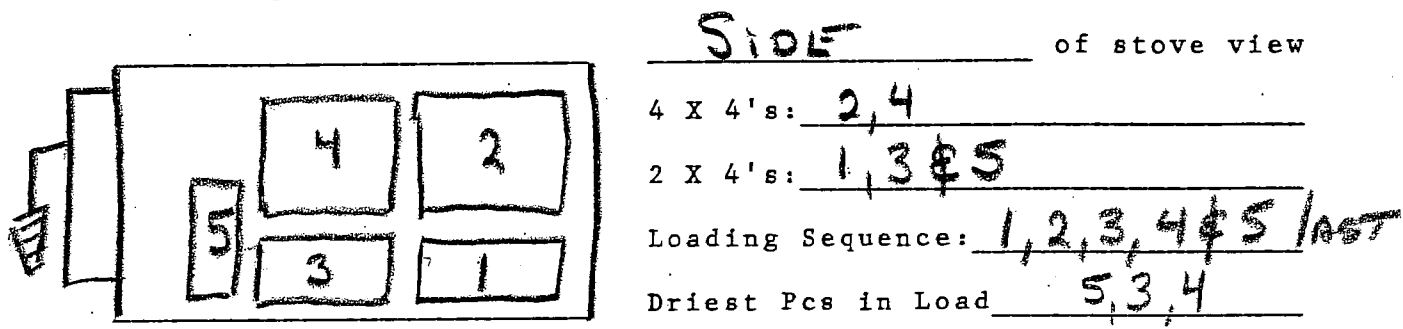
The primary air was adjusted to the run setting of 0.3655" open 3.5 lbs above the upper charcoal bed weight.

Additional Comments: Test Start Sequence: ① Turned Fan off  
② Adjusted PAC to wide Open ③ opened door ④ loaded fuel ⑤ cleared coals away from in front of the LPAO  
⑥ closed door

TOTAL ELAPSED Time: 1:15  
Photo @ 1:40

Test Fuel Charge Loading Information:

Test Fuel Charge and Loading Sequence Diagram



Loaded the test fuel charge on an essentially level, medium sized, average coal bed (in appearance, color and temperature for a Low (5.0 kg/hr) burn rate. Load: 1:15 Ignition: 1:16

- 1:17 VC to the baffle
- 1:30 Secondaries starting to ignite
- 1:40 Photo
- 3:30 Secondaries full width of pcs 4 & 5
- 4:45 - 5:00 Adjusted PAC to run setting
- 5:00 Flames decreased. Maintained a hot pocket of coals under pc 5 with a VC up to baffle with secondaries at the top of the VC. Both VC and secondaries decreasing fairly quickly.
- 5:30 11.9 / 1.49 (%CO<sub>2</sub> / %CO)
- 6:21 Secondaries on/off above pc 4
- 6:47 VC increasing in height and width

WOODSTOVE OPERATING DATA  
 WOODSTOVE DATA SHEET #9A-4

Additional Comments:

- 8:40 just secondary flashes at the top of the VC  
 10:07 Secondaries, VC decreasing  
 10:29 5.9/1.94 M smoke Lots of velocity in VC. Just V  
 flickers to the baffles. No Secondaries.  
 14:49 VC flickers to baffles.  
 15:28 5.5/1.11 MH  
 16:03 center part of VC out briefly 2 times  
 Dip in fire  
 16:20 Left side of VC increasing  
 17:07 Secondary flash above center/top of 4  
 18:00 VC decreasing again  
 18:25 Secondary flashes increasing  
 20:46 5.9/1.27 MH  
 21:50 Flames on bottom edge of PCS left of center  
 24:53 VC spreading to left of center, Secondary  
 flashes staying lit longer  
 25:26 6.4/1.33 MH/H  
 26:11 Left side of VC increased, then decreased  
 26:43 Secondaries burst on, then quickly off  
 27:40 " almost steady  
 30:00 Fan On Low. Steady Secondaries  
 30:43 8.10/1.53 M/MH  
 31:39 VC decreasing. Top down burn. Cold blue orange 2nd  
 32:19 Secondaries forward past front tube.  
 33:11 Secondaries barely full width of 4  
 33:48 yellow flames center front of PCS M smoke  
 straight into stackitis

WOODSTOVE OPERATING DATA  
WOODSTOVE DATA SHEET #9A-4

Additional Comments:

34149 12.85 / 1.55  
36108 14.52 / 1.63  
36149 15.10 / 1.50 Gas Balance m/MH still stuck in  
37147 out of balance - velocity in secondaries  
40120 15.6 / 1.34 back in balance  
45141 P5 has cracked thru.

Unit: Kuma Ashwood  
 Run: EPA 4  
 Date: 2/19/09  
 Technician: AM JRP PUG  
 WST1-Form7-Rev11/89

FUEL MOISTURE  
 WOODSTOVE TEST DATA SHEET #10

5kg. = 11.024 lbs      1kg. = 2.204 lbs

Room Temperature: 64.8 °F

Correction Factor: 10.5

NOTE: Record readings to the nearest 0.5% moisture  
 Uncor Values are corrected for temperature: Yes  No   
 Time Test Fuel Moisture Readings taken at: \_\_\_\_\_  
 Calibration Checks: X  Y  12.0 11.75 22.0 22.0

Pc #	Dimen	Use	Top		Bottom		Side		Piece Avg Corrected
			Uncor	Cor	Uncor	Cor	Uncor	Cor	
1	3 pcs	K	10.75	11.45	9.5	9.95	7.5	7.85	9.417
2									
3									
4	2x4-8'	P	19.5	20.9	18.0	19.2	18	19.2	19.767
5			21	22.6	22	23.7	18	19.2	21.833
6			18.5	19.8	18.5	19.8	19.5	20.9	20.167
7			19	20.3	19.5	20.9	22	23.7	21.633
8	∇	∇	19.5	20.9	21.5	23.1	22	23.7	22.567
9									105.967
10	"								
11	2x4-16 3/8	T	18	19.2	18	19.2	18	19.2	19.200
12		∇	18.5	19.8	18.5	19.8	19	20.3	19.967
13	∇	∇	18.5	19.8	18.5	19.8	18	19.2	19.600
14	"								
15	4x4-16 3/8	T	20	21.4	21.5	23.1	13	13.9	19.467
16	∇	∇	18	19.2	18	19.2	18	19.2	19.200
17									97.434
18									
19	SPACERS	T	19	20.3	19	20.3	18.5	19.8	20.133
20									OUT SPACERS

8  
 2.112  
 1.594  
 3.514  
 3.224  
 1.480

Kindling	Pretest Fuel	Test Load
9.417 %	21.1934 %	19.4868 %
8.606 %	17.487 %	16.309 %

% Moisture - Dry Basis:  
 % Moisture - Wet Basis:  
 13.306 4x4 7.088

To obtain Wet from Dry:  $\frac{100 \times \% \text{ Dry Rdg.}}{100 + \% \text{ Dry Rdg.}} = \% \text{ Moisture, Wet Basis}$   
 1, 11.434

Acceptable Ranges: 16-20% wet; 19-25% dry  
 (17.5 - 22.5 on Meter [Uncor reading] at 70°F)  
 2, 13.786  
 3, 10.638

Key for Use: K= Kindling P= Pretest Fuel T= Test Fuel

WOOD DENSITY DETERMINATION  
WOODSTOVE TEST DATA SHEET #11

Unit: Kuma Ash wood  
Run#: EPA 4  
Date: 2/19/09  
Technician: A. T. Myren  
WST2-form11-Rev 6/90

2X4

Wood Piece: Nominal Dimensions: 3.5 x 3.5 x 1.5  
Depth (D): 3.830 cm  
Width (W): 8.825 cm  
Length (L): 9.265 cm  
9.250 cm  
9.315 cm  
9.290 cm  
Length  $\bar{X}$  = 9.280 cm  
Volume: 313.662 cm<sup>3</sup>  
(D X W X L)

MOISTURE: Room Temperature: 67.8 OF Correction Factor: +0.5

Uncorrected Meter Readings Corrected for temperature: Yes  No

NOTE: Record moisture meter readings to the nearest 0.5%

	Uncor	Cor	%
Top:	18.5	19.8	%
Bottom:	18.5	19.8	%
Side:	17.5	18.6	%
$\bar{X}$ :		19.400	%

Avg % Moisture (Dry) 19.400 %  
Avg % Moisture (Wet) 16.248 %  
Scale: Levelled In  Out   
Zeroed: In  Out

Wet Weight: 137.9 g Dry Weight: 115.6 g

% Moisture Dried Basis: 16.171 %  
[1 - (Dry Wt ÷ Wet Wt)] X 100

Into Dryer Date 2/19/09 Time 1337 Temp 190 OF  
Out of Dryer Date 3/2/09 Time 0915 Temp 192 OF  
(Minimum Time in Dryer: 24 hrs.) Minimum Dryer Temp 100°C (212°F)

Density = 115.6 g (dry wt) ÷ 313.662 cm<sup>3</sup> (volume) = 0.3695 g/cm<sup>3</sup>

Pellet Fuel Moisture Content Determination

Tare Beaker Wt. \_\_\_\_\_ g  
Wet Wt: \_\_\_\_\_ g - \_\_\_\_\_ g = \_\_\_\_\_ g  
Gross Wet Wt. Tare Beaker Wt. Net Wet Wt.  
Dry Wt: \_\_\_\_\_ g - \_\_\_\_\_ g = \_\_\_\_\_ g  
Gross Dry Wt. Tare Beaker Wt. Net Dry Wt.  
% Moisture Dried Basis: \_\_\_\_\_ %  
[1 - (Net Dry Wt ÷ Net Wet Wt.)] X 100



PRE BURN DATA  
 RECORD SHEET #13  
 WST2-FORM16

Unit: KUMON  
 Run: EPA  
 Page: 1 of 1

Date: 2-19-09  
 Technician(s): A-TM G.R.P.  
 P.D.C.

Hot Box On ✓

Minute	Scale Weight	Burn Rate	Stove Top	Left Side	Back	Right Side	Bottom	Firebox	2nd Burn	Room Temp	Static	Comments
0	770.6	0	990	583	398	596	381	1003	1296	79	-1073	Primary Air Set at 3655
5	769.9	1.7	970	601	402	600	390	952	1251	81	-1064	Secondary Air Set at
10	769.3	1.6	910	602	404	601	396	938	1342	82	-1060	Fan: on hi @ 2004 - Low @ 30
15	768.7	1.6	889	599	412	594	398	934	1390	80	-1059	TUNNEL ON AT: 1205
20	768.2	1.5	826	595	414	585	396	926	1375	80	-1057	Buckets ICED ✓
25	767.9	1.3	833	592	411	581	393	927	1333	80	-1053	ANALYZERS SPANNED
30	767.7	1.2	730	582	416	565	387	902	1150	81	-1047	Pumps turned on at:
35	767.6	1.1	692	574	416	556	385	893	1153	80	-1043	52006 AT 1407
40	767.5	1.1	625	555	412	542	382	865	1025	80	-1042	503.2 - 2.14
45	767.4	1.1	587	536	402	527	378	829	933	80	-1040	Check WB/DB: 48.2.4 - 16.18
50	767.3	1.1	580	520	393	511	376	799	886	80	-1038	470.0 - 16.14
55	767.2	1.1	517	503	380	495	373	769	851	80	-1036	453.6 - 16.4
60	767.2	0	493	489	370	462	371	749	836	80	-1034	Probe IN TUNNEL
65	767.1	0	474	476	362	469	369	732	825	79	-1034	TUNNEL AP 441.0 - 12.14
70	-	-	-	-	-	-	-	-	-	-	-	430.0 - 11.1
75	-	-	-	-	-	-	-	-	-	-	-	-
80	-	-	-	-	-	-	-	-	-	-	-	-
85	-	-	-	-	-	-	-	-	-	-	-	-
90	-	-	-	-	-	-	-	-	-	-	-	-
95	-	-	-	-	-	-	-	-	-	-	-	-
100	-	-	-	-	-	-	-	-	-	-	-	-

Rake FWD @ Flameout or 30 mins. (36 min)

Start 430-435

Raked Fuel @ 36 min













PRE AND POST TEST ZERO/SPAN CHECK  
WOODSTOVE DATA SHEET #15-1

Colville

Site: Myren Consulting, ~~Myren Consulting~~, WA Date: 2/19/09 Analyte: CO<sub>2</sub>

Source: Kuma Ashwood Run #: EPA 4

Zero Cyl #: TC 30AM154 Conc. 00.0 % CO<sub>2</sub> Cyl Press: 1510 psi

Certified by: Oxarc Date: 11/12/07

Span Cyl #: AS 90457 Conc. 12.5 % CO<sub>2</sub> Cyl Press: 1470 psi

Certified by: Matheson Tri Gas Date: 2/2/09

Analyzer: Make: Horiba Model: PIR-2000 SN: 607024

Range: 0 - 25.0% CO<sub>2</sub> Analyzer Output: 0 - 1.0 v.

Flow: 1.5 SCFH Measured by: Rotameter: X Flowmeter:         

EPA Span Value = 25.0% CO<sub>2</sub>  
EPA Control Limits = + 2.5% of 25.0% CO<sub>2</sub> = + 0.625% CO<sub>2</sub>

Pre Run Audit: By: A.P. Myren Time: 1140 Temp: 78 °F

Audit Results

Point #	Expected Response			Actual Response			+ Conc. Difference	Δ %
	Meter	DVM	%	Meter	DVM	%		
Zero	00.0	.000	00.0	00.0	.000	0.050453	+0.050453	+0.22
Span	50.00	1.500	12.5	49.75	1.499	12.3858	-0.11425	-0.91

Comments:

Post Run Audit: By: A.P. Myren Time: 1855 Temp: 77 °F

Audit Results

Point #	Expected Response			Actual Response			+ Conc. Difference	Δ %
	Meter	DVM	%	Meter	DVM	%		
Zero	00.0	.000	00.0	00.0	.000	0.050453	+0.050453	+0.22
Span	50.00	1.500	12.5	49.5	1.498	12.36124	-0.13896	-1.11

Comments:

+ Conc. Difference = Act % - Exp (Std) %  
 Zero % Difference =  $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Full Scale Value}} \times 100$   
 Span % Difference =  $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Exp \% (ppm)}} \times 100$



PRE AND POST TEST ZERO/SPAN CHECK  
WOODSTOVE DATA SHEET #15-3

Colville

Site: Myren Consulting, ~~Woodville~~, WA Date: 2/19/09 Analyte: CO

Source: Kumar Ashwood Run #: EPA 4

Zero Cyl #: TC3AAM 154 Conc. 00.0 % CO Cyl Press: 1510 psi

Certified by: Oxarc Date: 11/12/07

Span Cyl #: A390457 Conc. 2.00 % CO Cyl Press: 1470 psi

Certified by: Matheson Tri Gas Date: 2/2/09

Analyzer: Make: MORIBA Model: MEXA 311GE SN: GE-30025

Range: 0 - 10.0% CO Analyzer Output: 0 - 100 mv.

Flow: 1.5 SCFH Measured by: Rotameter: X Flowmeter:     

EPA Span Value = 5.0% CO  
EPA Control Limits = +2.5% of 5.0% CO = + 0.125% CO

Pre Run Audit: By: A.T. Myren Time: 1140 Temp: 78 °F

Audit Results

Point #	Expected Response			Actual Response			+ Conc. Difference	Δ %
	Meter	DVM	%	Meter	DVM	%		
Zero	00.0	00.0	00.0	0.00	0.000	0.00443	-0.00443	-0.04
Span	2.00	2.00	2.00	1.97	1.97	1.9758	-0.0242	-1.210

Comments:

Post Run Audit: By: A.T. Myren Time: 1855 Temp.: 77 °F

Audit Results

Point #	Expected Response			Actual Response			+ Conc. Difference	Δ %
	Meter	DVM	%	Meter	DVM	%		
Zero	00.0	00.0	00.0	0.00	0.000	0.00443	-0.00443	-0.04
Span	2.00	2.00	2.00	1.96	1.96	1.9657	-0.03426	-1.71

Comments:

+ Conc. Difference = Act % - Exp (Std) %  
 Zero % Difference =  $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Full Scale Value}} \times 100$   
 Span % Difference =  $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Exp \% (ppm)}} \times 100$

Unit: Lucma Ashwood  
 Run: EPA 4  
 Date: 2/19/89  
 Technicians: ARM JRP PDG  
 WSTB-Form3-Rev11/89

QUALITY CHECKS  
 WOODSTOVE DATA SHEET #16

Ambient = Tr: \_\_\_\_\_ °F T/C#30: \_\_\_\_\_ °F  
 Thermocouple Check (at ambient): T/C#1: \_\_\_\_\_ °F; T/C#2: 68.6 °F;  
 T/C #3: 71.0 °F; T/C #4: 71.9 °F; T/C #5: 73.5 °F;  
 T/C #6: 71.9 °F; T/C #7: 72.3 °F; T/C #8: 72.8 °F;  
 T/C #9: 74.0 °F; T/C #10: 74.0 °F; T/C #11: 64.8 °F;  
 T/C #12: 71.1 °F; T/C #13: 68.0 °F; T/C #14: 63.4 °F;  
 T/C #15: 67.7 °F; T/C #16: 59.0 °F; T/C #17: 74.4 °F;  
 T/C #18: \_\_\_\_\_ °F; T/C #19: \_\_\_\_\_ °F; T/C #20: \_\_\_\_\_ °F;  
 T/C #21: \_\_\_\_\_ °F; T/C #22: \_\_\_\_\_ °F; T/C #23: \_\_\_\_\_ °F;  
 T/C #24: \_\_\_\_\_ °F; T/C #25: \_\_\_\_\_ °F; T/C #26: \_\_\_\_\_ °F;

Comments: \_\_\_\_\_

Thermocouple Readout: Pretest Zero/Span Check and Calibration:  
 Zero (0°F) : 0.2 °F Adj to: \_\_\_\_\_ °F Post Test Check Zero (0°F): 1.0 °F % Difference +0.22  
 Span (2000°F): 2000.7 °F Adj to: \_\_\_\_\_ °F Span (2000°F): 2002.4 °F % Difference +0.10

(Allowable % Difference = 1.5%. Use formulas on Woodstove Data Sheet #15 to calculate % Difference) In Degrees Absolute.

Thermocouple Readout Pretest Linearity Check  
 0°F = 0.2 °F; 200°F = 202.2 °F; 400°F = 399.5 °F;  
 600°F = 601.7 °F; 800°F = 802.0 °F; 1000°F = 1001.2 °F;  
 1200°F = 1199.0 °F; 1400°F = 1400.0 °F; 1600°F = 1600.6 °F;  
 1800°F = 1800.7 °F; 2000°F = 2000.8 °F

Combustion Gas (CO<sub>2</sub>, O<sub>2</sub>, CO) Train Leak Check: Pre ✓ PDG Post ✓ PDG  
 Draft (Static) Gauge Zero Check: Pre ✓ JRP Post ✓ ARM

Scale Check Pre (Wt. #'s): 768.8 - 763.8 = 5.0 lbs / 5.0 lbs = OK (ARM)  
 Post (Wt. #'s): 771.9 - 766.9 = 5.0 lbs / 5.0 lbs = OK (ARM)

Stack cleaned prior to the run: Yes \_\_\_\_\_ No ✓  
 Tunnel cleaned prior to the run: Yes \_\_\_\_\_ No ✓

MYREN CONSULTING CERTIFICATION TEST DATA

DILUTION TUNNEL CALCULATIONS

1/25/09, Md=28.56, Bws=4%  
6" Tunnel  
EPA 6

File Name:

Manufacturer:

Model Number:

Lab Name:

Test Date:

Run Number:

Meter Box Y Factor:

Barometric pressure (in):

Gas meter temp (ave):

delta H(ave):

Gas meter initial reading:

Gas meter final reading:

Front catch (acetone) mg:

first filter catch (mg):

second filter catch (mg):

Tunnel Flow (Qsd) (dscfm)

Emission Rate(g/hr):

Emission Rate(M5H) :

Avg. of Delta P Sq. Roots:

Vs (Avg.)(ft/min):

Tunnel Avg. Temperature (F):

Test time(min):

Fuel Load(lb. wet):

Wood moisture(%wet):

Burn rate(dry kg/hr):

Sample Volume (dscf)

Avg. Tunnel Static (-inch H2O):

Room Blank Catch (mg/dscf):

Emission Factor (g/kg):

Pitot Correction Factor:

front filter number

back filter number

Beaker Number:

PRELIMINARY RESULTS

FINAL RESULTS:

DATA SUMMARY

MODEL:

RUN:

DATE:

DBR:

EMISSION RATE (g/hr)(M5H)

EMISSION FACTOR (g/kg):

AVG. % PROPORTIONALITY:

RUN TIME (min)	PITOT DELTAP (-INCH H2O)	TNL TEMP (°F)	GAS METER RDG (ft3)	GAS METER TEMP (°F)	GAS METER DELTA H (ft. H2O)	TUNNEL VELOCITY (ft/min)	PROP RATE (%)	dGDM vol std (ft3)	Tunnel Static (-Inch H2O)	SQUARE ROOT DELTA P	DRY GAS METER RDG (m3)
0	0.041	94	603.1000	68	0.900	845.10	105.8	5.178	0.163	0.2025	
10	0.042	101	608.4090	70	0.900	860.73	103.0	5.088	0.167	0.2049	
20	0.042	97	613.6550	73	0.900	857.66	101.4	5.027	0.168	0.2049	
30	0.042	99	618.8680	76	0.900	859.20	101.1	4.982	0.166	0.2025	
40	0.041	101	624.0720	80	0.900	850.42	100.2	4.962	0.164	0.2025	
50	0.041	100	629.2750	82	0.900	849.66	100.8	4.944	0.165	0.2000	
60	0.040	99	634.4680	83	0.900	838.49	99.5	4.958	0.167	0.2025	
70	0.041	99	639.6950	85	0.900	848.91	99.4	4.971	0.165	0.2025	
80	0.041	97	644.9460	86	0.900	847.39	100.6	4.978	0.163	0.2000	
90	0.040	95	650.2040	86	0.900	835.48	100.2	4.971	0.162	0.2000	
100	0.040	94	655.4640	87	0.900	834.73	100.2	4.982	0.163	0.2000	
110	0.040	91	660.7360	87	0.900	832.47	100.3	4.990	0.163	0.2000	
120	0.040	91	666.0160	87	0.900	832.47	100.2	4.981	0.163	0.2000	
130	0.040	92	671.2870	87	0.900	833.22	98.8	4.988	0.163	0.2025	
140	0.041	90	676.5750	88	0.900	842.04	100.2	4.981	0.163	0.2000	
150	0.040	91	681.8560	88	0.900	832.47	98.8	4.992	0.163	0.2025	
160	0.041	90	687.1480	88	0.900	842.04	99.7	4.976	0.162	0.2000	
170	0.040	91	692.4330	89	0.900	832.46	99.0	4.997	0.163	0.2025	
180	0.041	91	697.7300	88	0.900	842.81	99.6	4.979	0.161	0.2000	
190	0.040	90	703.0180	89	0.900	831.71	99.8	4.992	0.163	0.2000	
200	0.040	89	708.3200	89	0.900	830.95	98.5	4.987	0.162	0.2025	
210	0.041	89	713.6160	89	0.900	841.28	98.3	4.985	0.163	0.2025	
220	0.041	88	718.9100	89	0.900	840.51	98.3	4.984	0.162	0.2025	
230	0.041	88	724.2030	89	0.900	840.51	99.7	4.994	0.164	0.2000	
240	0.040	87	729.5070	89	0.900	829.44	99.5	4.992	0.163	0.2000	
250	0.040	86	734.8090	89	0.900	828.68	0.0	0.000	0.000	0.0000	
260			0.0000			0.00	0.0	0.000	0.000	0.0000	
270			0.0000			0.00	0.0	0.000	0.000	0.0000	
280			0.0000			0.00	0.0	0.000	0.000	0.0000	
290			0.0000			0.00	0.0	0.000	0.000	0.0000	
300			0.0000			0.00	0.0	0.000	0.000	0.0000	
310			0.0000			0.00	0.0	0.000	0.000	0.0000	
320			0.0000			0.00	0.0	0.000	0.000	0.0000	
330			0.0000			0.00	0.0	0.000	0.000	0.0000	
340			0.0000			0.00	0.0	0.000	0.000	0.0000	
350			0.0000			0.00	0.0	0.000	0.000	0.0000	
360			0.0000			0.00	0.0	0.000	0.000	0.0000	
370			0.0000			0.00	0.0	0.000	0.000	0.0000	
380			0.0000			0.00	0.0	0.000	0.000	0.0000	

ASHWOOD

EPA 6

2/27/09

1.199

2.9311

1.4807

100.111

DATE: 2/27/09 PAGE 1 OF 2 UNIT: Kama Ashwood RUN: EPA 6

METER BOX: 456P METER Y: 1.0177 FILTER #'S: (F) 716 (R) 715

.941 / .9415  
PRE TEST LEAK CHECK: .0005 CFM @ -16.0 IN HG FILTER SIZE: 110 mm

.865 / .866  
POST TEST LEAK CHECK: 1001 CFM @ -15.8 IN HG PROBE LENGTH 21 IN

TIME		METER READING (FT <sup>3</sup> )	PITOT		TUNNEL TEMP (°F)	METER TEMP (°F)	GAS METER Δh	VAC (in Hg)
CLOCK	ELAPSED		AP	Pg				
1345	00	603.100	1041	-1163	94	66	.90	0
55	10	608.409	1042	-1167	101	70	.90	0
1405	20	613.655	1042	-1169	97	73	.90	0
15	30	618.868	1042	-1169	99	76	.90	0
25	40	624.072	1041	-1166	101	80	.90	0
35	50	629.275	1041	-1164	100	82	.90	0
45	60	634.468	1040	-1165	99	83	.90	0
55	70	639.695	1041	-1167	99	85	.90	0
1505	80	644.946	1041	-1165	97	86	.90	0
15	90	650.204	1040	-1163	95	86	.90	0
25	100	655.464	1040	-1162	94	87	.90	0
35	110	660.736	1040	-1163	91	87	.90	0
45	120	666.016	1040	-1163	91	87	.90	0
55	130	671.287	1040	-1163	92	87	.90	0
1605	140	676.575	1041	-1163	90	88	.90	0
15	150	681.856	1040	-1163	91	88	.90	0
25	160	687.148	1041	-1163	90	88	.90	0
35	170	692.433	1040	-1162	91	89	.90	0
45	180	697.730	1041	-1163	91	88	.90	0
55	190	703.018	1040	-1161	90	89	.90	0

BP

00	28.73	250	28.725
60	28.73		
120	28.73		
180	28.73		
240	28.725	AVG. =	28.720

Pre Test Filter  
Check Weighing  
F .6695  
R .6747

End of Test Weight  
F .6901 R .6752  
.6690 .6744  
.0211 .0008

17.20-1  
13.314 lbs.

**METHOD 5G -1 (EPA) PARTICULATE SAMPLING DATA**

Rev. 2/09

DATE: 2/22/09 PAGE 2 OF 2 UNIT: Kuma Asthwood RUN: EPA6

METER BOX: 456-P METER Y: 1.0177 FILTER #'S: (F) 716 (R) 715

1941/19415  
PRE TEST LEAK CHECK: 10005 CFM @ -16.0 IN HG FILTER SIZE: 110 mm

POST TEST LEAK CHECK: .001 CFM @ -15.8 IN HG PROBE LENGTH 21 IN

TIME		METER READING (FT <sup>3</sup> )	PITOT		TUNNEL TEMP (°F)	METER TEMP (°F)	GAS METER Δh	VAC (in Hg)
CLOCK	ELAPSED		ΔP	Pg				
1205	200	708.320	1040	-1163	89	89	190	0
15	10	713.616	1041	-1162	89	89	190	0
25	20	718.910	1041	-1163	88	89	190	0
35	30	724.203	1041	-1162	88	89	190	0
45	240	729.507	1040	-1164	87	89	190	0
55	250	734.809	1040	-1163	86	89	190	0
	60							
	70							
	80							
	90							
	00							
	10							
	20							
	30							
	40							
	50							
	60							
	70							
	80							
	90							

BP

00	<u>28.73</u>	<u>2SD</u>	<u>28.725</u>
60	<u>28.73</u>		
120	<u>28.73</u>		
180	<u>28.73</u>		
240	<u>28.725</u>	AVG. =	

Pre Test Filter  
Check Weighing  
F 16595  
R 16247

End of Test Weight  
F 16590 R 16244

MYREN CONSULTING, INC.

Dilution Tunnel Traverse Data with 8 Traverse Points

Unit: KUMA Ashwood  
 Run #: EPA C  
 Date: 2.27.09  
 Technicians: ATM ARP PPG  
 #12 Rev 2/16/09

Point	Location	$\Delta p$	$\sqrt{\Delta p_{trav}}$	$\Delta p$	$\sqrt{\Delta p_{cent}}$	$T_{trav}$	$T_{cent}$	Pg
W-1	0.5"	<u>.035</u>	<u>.1871</u>	✓	✓	<u>97</u>	✓	✓
2	1.5	<u>.041</u>	<u>.2025</u>	✓	✓	<u>97</u>	✓	✓
Center	Center	<u>.041</u>	<u>.2025</u>	✓	✓	<u>98</u>	<u>159</u>	✓
3	4.5	<u>.040</u>	<u>.2000</u>	✓	✓	<u>98</u>	✓	✓
4	5.5	<u>.038</u>	<u>.1949</u>	✓	✓	<u>96</u>	✓	✓
S-1	0.5	<u>.032</u>	<u>.1769</u>	✓	✓	<u>96</u>	✓	✓
2	1.5	<u>.037</u>	<u>.1924</u>	✓	✓	<u>96</u>	<u>156</u>	✓
Center	Center	<u>.040</u>	<u>.2000</u>	✓	✓	<u>96</u>	✓	✓
3	4.5	<u>.040</u>	<u>.2000</u>	✓	✓	<u>95</u>	✓	✓
4	5.5	<u>.038</u>	<u>.1949</u>	✓	✓	<u>95</u>	✓	✓
Totals			<u>1.5507</u>	✓	<u>.4025</u>	<u>773</u>	<u>194</u>	<u>1815</u>
Average			<u>.1930</u>	✓	<u>.2013</u>	<u>96.625</u>	<u>97</u>	<u>1845</u>
		$^{\circ}R = (^{\circ}F + 460)$			<u>556.6</u>	<u>557</u>	✓	✓

$P_s = BP + (-Pg/13.6) = 28.74 + (-1515/13.6) = 28.740$  "Hg

LEAK CHECKS:  
 Pre Test: Pg Leg: OK ARP Velocity Head Leg: OK PPG  
 Post Test: Pg Leg: OK PPG Velocity Head Leg: OK PPG

Rev 4/19/08

DILUTION TUNNEL GAS VELOCITY & VOLUMETRIC FLOW RATE CALCULATIONS

UNIT: Kuma Ashwood DATE: 2.27.09 RUN #: EPA6 TECHNICIAN(S): ATM JRP  
PDC

Average Gas Velocity in the Dilution Tunnel Vstrav (EPA M2 EQN 2-9, ASTM E 2515-07 EQN 7)

$$(9) V_{strav} = (85.49) (0.99 \text{ cp}) \left( \frac{1998}{\sqrt{\Delta P}} \times \sqrt{\Delta P} \right) \frac{Ts}{Ts - Ta} = 13,50965 \text{ fps}$$

$$(9A) V_s = (13,50965 \text{ fps}) (60) = 810.579 \text{ fpm}$$

Gas Velocity in the Center of the Dilution Tunnel - Vscnt (EPA M2 EQN 2-9, ASTM E 2515-07 EQN 7)

$$(9) V_{scnt} = (85.49) (0.99 \text{ cp}) \left( \frac{2010}{\sqrt{\Delta P}} \times \sqrt{\Delta P} \right) = 14,03751 \text{ fps}$$

$$(9A) V_s = (14,03751 \text{ fps}) (60) = 842.251 \text{ fpm}$$

EPA M5G1 Section 4.2.2, ASTM E 2515-07 EQN 1 Adjustment Factor for Center of Tunnel Pitot Tube Location

$$F_p = V_{strav} / V_{scnt} = 13,50965 / 14,03751 = 96240$$

Average Stack Gas Dry Volumetric Flow Rate - Qsd (EPA M2 EQN 2-10, ASTM E 2515-07 EQN 3)

$$(10) Q_{sd} = 3600 (1 - 0.04 Bws) (13,50965 \text{ fps}) (1963 \text{ ft}^2) (528 \text{ }^\circ\text{A}) (29.726 \text{ Ps } ^\circ\text{A}) (29.92 \text{ }^\circ\text{Hg}) / (550.6 \text{ }^\circ\text{A}) (29.92 \text{ }^\circ\text{Hg}) = 2847.812 \text{ dscfhr (or dscfh)}$$

$$(10A) \frac{2847.812 \text{ dscfhr}}{60} = 47.4637 \text{ dscfm (or dscfm)}$$

Note: Number in { } under blank lines denotes number of decimals to be used. If a blank calls for an answer already calculated, use the number of decimals previously specified for that answer.

WOODSTOVE DATA SHEET #4-1: INITIAL FILTER WEIGHTS (TARE WEIGHTS)

Into Dessicator: Date 1-27-09 Time 11:49 By PDG Front Half X Back Half X

Manufacturer: Pall P/N: 60115 Size: 110 Lot.No.: 70726 Grade: A/E GLASS

Filter #	First Wt	2009 Date	Time	By	Second Wt	Date	Time	By	Third Wt	2009 Date	Time	By
700	.6873	1-22	1331	GRP	.6877	1-23	1417	PDG				
701	.6871		1330	GRP	.6878		1419	PDG	.6877	1-26	1421	GRP
702	.6816		1329	GRP	.6825		1420	PDG	.6824	1-26	1420	GRP
703	.6761		1328	GRP	.6762		1421	PDG				
704	.6727		1327	GRP	.6732		1422	PDG				
705	.6833		1326	GRP	.6837		1423	PDG				
706	.6946		1325	GRP	.6948		1424	PDG				
707	.6773		1324	GRP	.6777		1425	PDG				
708	.6701		1323	GRP	.6702		1426	PDG				
709	.6799		1322	GRP	.6809		1427	PDG	.6806	1-26	1419	GRP
710	.6587		1321	GRP	.6590		1428	PDG				
711	.6654		1320	GRP	.6656		1429	PDG				
712	.6688		1319	GRP	.6692		1430	PDG				
713	.6864		1318	GRP	.6866		1431	PDG				
714	.6651		1318	GRP	.6655		1432	PDG				
715	.6741		1317	GRP	.6744		1433	PDG				
716	.6692		1316	GRP	.6690		1434	PDG				
717	.6531		1315	GRP	.6536		1435	PDG				
718	.6721		1314	GRP	.6723		1436	PDG				
719	.6769		1313	GRP	.6769		1437	PDG				
720	.6627		1312	GRP	.6628		1438	PDG				
721	.6567		1311	GRP	.6569		1439	PDG				
722	.6539		1310	GRP	.65340		1440	PDG				
723	.6552		1309	GRP	.6552		1441	PDG				
724	.6655		1308	GRP	.6656		1442	PDG				

Checked by A.T. Myer Date: 1/27/09 Time 1632

QA REWEIGH

Filter #	WT	Date	Time	By
703	.6761	1/27/09	1639	AMM
708	.6705		1640	AMM
715	.6749		1642	AMM

BALANCE ROOM ENVIRONMENTAL CONDITIONS

WB	DB	%RH	Date	Time	By
57	72	38	1-22-09	1138	ATM
58	25	33	1-23-09	1150	PDG
56	76	25	1-26-09	1359	GRP
58	72	31	1/27/09	1530	PDG

Post  
 0.0000 0.0000 0.0000 0.0000  
 100.0000 99.9994 99.9993 99.9993



WOODSTOVE DATA SHEET #4-2:  
INITIAL BEAKER WEIGHTS (TARE WEIGHTS)

Into Dessicator: Date: 9.04.08 Time: 13:33 By: GRP

Beaker #	First Wt	2008 Date	Time	By	Second Wt	2009 Date	Time	By	Third Wt	2009 Date	Time	By
24	73.2197	12/17	1628	GRP	73.2186	1/20	1000	PDG	73.2188	1/20	1635	GRP
25	72.6520		1625	GRP	72.6512		1002	PDG	72.6514		1635	GRP
26	71.7887		1631	GRP	71.7881		1007	PDG	71.7877		1626	GRP
28	70.5985		1627	GRP	70.5976		1003	PDG	70.5977		1632	GRP
29	71.5207		1635	GRP	71.5191		1008	PDG	71.5193		1637	GRP
30	70.7867		1629	GRP	70.7855		1005	PDG	70.7856		1627	GRP
33	53.1490		1632	GRP	53.1483		1012	PDG	53.1486		1633	GRP
34	53.2618		1636	GRP	53.2609		1014	PDG	53.2609		1628	GRP
35	53.2826		1637	GRP	53.2817		1016	PDG	53.2815		1629	GRP
36	53.5752		1638	GRP	53.5742		1010	PDG	53.5744		1634	GRP
42												
43	53.2325		1633	GRP	53.2315		1011	PDG	53.2319		1631	GRP

Checked By: A.T. Myam Date: 1/23/09 Time: 1145

QA REWEIGH

Beaker #	WT	Date	Time	By
35	53.2820	1/23/09	1146	AMM
26	71.7882	1/23/09	1147	AMM
43	53.2323	1/23/09	1149	AMM

BALANCE ROOM ENVIRONMENTAL CONDITIONS

WB	DB	%RH	Date	Time	By
52	70	25	12/17/08	1619	GRP
58	74	37	1/20/09	0930	PDG
57	73	38	1/20/09	1613	GRP
58	72	38	1/23/09	1138	AMM

WOODSTOVE DATA SHEET #4-2:  
 INITIAL BEAKER WEIGHTS (TARE WEIGHTS)

*Blank done 12/9/07*

Into Dessicator: Date: 10/12/07

Time: 0801

By: GRP

Beaker #	First Wt	Date	Time	By	Second Wt	Date	Time	By	Third Wt	Date	Time	By
22	71.8343	10/22/07	1358	GRP	71.8332	11/10/07	1938		71.8330	11-11-07	1748	Jm
24	73.2192	1	1400	GRP	73.2190	11/10/07	1940		73.2193	11-11-07	1746	Jm
25	72.6516		1401	GRP	72.6512	11/10/07	1944		<b>Blank</b>			
26	71.7895		1403	GRP	71.7888	11/10/07	1939		71.7886	11-11-07	1747	Jm
27	72.3316		1402	GRP	72.3314	11/10/07	1945					
28	70.5977		1404	GRP	70.5975	11/10/07	1941		70.5977	11-11-07	1745	Jm
39	53.1508		1405	GRP	53.1500	11/10/07	1942					
37	53.7237	11/10/07	1945	ATM	53.7238	11/11/07	1743	Jm				

Checked By: \_\_\_\_\_ Date: \_\_\_\_\_ Time: \_\_\_\_\_

QA REWEIGH

BALANCE ROOM ENVIRONMENTAL CONDITIONS

Beaker #	WT	Date	Time	By
27	72.3315	11-11	1740	Jm
25	72.6515	11-11	1741	Jm
39	53.1509	11-11	1744	Jm

WB	DB	%RH	Date	Time	By
57	68	50	10/22/07	1344	GRP
			11/10		

Post weighing  
 0.0002g  
 in room

LSD  
 0.0002  
 00000k

2nd

WOODSTOVE DATA SHEET #4-3: C ) TANT FINAL WEIGHTS

85 ml

FINAL BEAKER WEIGHTS

Beaker #	Into Dessic	Date	Time	By	First	Date	Time	By	Second	Date	Time	By	Third	Date	Time	By
26	71.792	3/2	1905	AM	71.792	3/3	1433	PDG	71.7927	2009		2009				

FINAL FILTER WEIGHTS

Filter #	Into Dessic	Date	Time	By	First	Date	Time	By	Second	Date	Time	By	Third	Date	Time	By
716	.6901	2/27	1915	AM	.6890	2/28	1340	AM	.6888	3/3	1437	PDG				
715	.6752	1915	1915	AM	.6750	2/28	1342	AM	.6750	3/3	1435	PDG				

QA REWEIGH: FINAL WEIGHTS

Date	Beaker #	Final Wt	By
Date	Filter #	Final WT	By

SCALE ROOM ENVIRONMENTAL CONDITIONS

Weighing Session	Date	Time	By	WB	DB	%RH
1	0/28	1330	ATM	87	74	33
2	3/3	1431	PDG	89	70	35
3	3/4	1556	SKP	56	70	40
4						
5						

SCALE ROOM ENVIRONMENTAL CONDITIONS

Date	Time	By	WB	DB	%RH
6					
7					
8					
9					
Comments					



WOODSTOVE DATA SHEET 4-4 SCALE QC RECORD SHEET

SCALE: SARTORIUS  
 MODEL: CP224S  
 SN: 17050374

FROM: 9/27/2007  
 THROUGH: 12/7/2007

Level	Recali	130 g	100 g	10 g	1.0 g	100 mg	20 mg	Date	Time	Tech	Wet Bulb	Dry Bulb	% RH
✓	N	129.9998	99.9998	10.0000	1.0000	0.1000	0.0199	9/27/07	1402	GRP	55	67	45
✓	Y	129.9995	99.9996	10.0001	1.0000	0.1000	0.0200	9/28/07	1335	GRP	57	69	46
✓	Y	129.9996	99.9996	9.9999	1.0000	0.1000	0.0200	10/1/07	1505	ATM	50	70	40
✓	N	129.9995	99.9996	10.0000	1.0001	0.1000	0.0199	10/2/07	1611	GRP	56	68	46
✓	N	129.9997	99.9997	9.9999	1.0001	0.1000	0.0199	10/3/07	1122	GRP	56	68	46
✓	N	129.9996	99.9996	10.0000	1.0000	0.0999	0.0199	10/4/07	0925	GRP	55	67	45
✓	Y	129.9996	99.9996	10.0000	1.0000	0.1000	0.0199	10/5/07	0750	GRP	51	62	45
✓	N	129.9997	99.9997	9.9999	1.0000	0.1000	0.0199	10/5/07	1513	GRP	56	69	43
✓	Y	129.9996	99.9996	10.0000	1.0001	0.1001	0.0200	10/9/07	1505	ATM	50	71	44
✓	N	129.9996	99.9997	10.0000	1.0001	0.1001	0.0200	10/12/07	1259	ATM	50	70	48
✓	Y	129.9995	99.9996	9.9999	1.0000	0.1000	0.0199	10/22/07	1344	GRP	57	68	50
✓	Y	129.9996	99.9997	9.9999	1.0000	0.1000	0.0199	10/29/07	1338	GRP	53	63	50
✓	N	129.9995	99.9995	10.0000	1.0000	0.1000	0.0200	10/31/07	0933	ATM	56	70	40
✓	Y	129.9996	99.9997	10.0000	1.0000	0.1000	0.0199	11/30/07	1457	GRP	55	70	36
✓	Y	129.9996	99.9996	9.9999	1.0000	0.1000	0.0199	10/31/07	1528	GRP	57	75	30
✓	Y	129.9996	99.9996	9.9999	1.0000	0.0999	0.0199	11/2/07	1038	GRP	50	67	33
✓	Y	129.9996	99.9996	10.0000	1.0001	0.1000	0.0199	11/5/07	0730	GRP	57	73	35
✓	Y	129.9996	99.9997	10.0000	1.0000	0.1001	0.0201	11/9/07	1550	ATM	58	70	48
✓	N	129.9996	99.9997	10.0000	1.0000	0.1000	0.0200	11/10/07	1885	ATM	58	71	44
✓	Y	129.9997	99.9997	9.9999	1.0000	0.1000	0.0199	11/11/07	1810	ATM	55	69	39
✓	N	129.9997	99.9996	9.9999	1.0000	0.1000	0.0199	11/12/07	0822	GRP	54	67	41
✓	N	129.9996	99.9996	10.0000	1.0000	0.1000	0.0199	11/12/07	1226	ATM	58	72	41
✓	N	129.9998	99.9997	9.9999	0.9999	0.1000	0.0200	11/14/07	1710	GRP	58	73	39
✓													
✓	Y	129.9997	99.9997	10.0000	1.0000	0.1000	0.0200	11/15/07	1350	ATM	59	72	45
✓	N	129.9996	99.9996	9.9999	0.9999	0.1000	0.0200	11/16/07	1600	GRP	58	71	44
✓	N	129.9996	99.9996	10.0000	1.0000	0.1000	0.0199	11/19/07	1758	ATM	760	74	43
✓	Y	129.9997	99.9997	10.0000	1.0001	0.1001	0.0200	11/19/07	1143	ATM	56	70	40
✓	Y	129.9995	99.9996	10.0000	1.0000	0.1000	0.0199	11/20/07	1416	GRP	54	69	35
✓	N	129.9996	99.9996	10.0000	1.0000	0.1000	0.0200	11/27/07	1110	ATM	57	70	44
✓	N	129.9995	99.9996	10.0000	1.0000	0.1000	0.0199	12/3/07	0730	GRP	55	69	40
✓	N	129.9996	99.9996	10.0000	1.0000	0.0999	0.0200	12/16/07	1125	ATM	54	67	44
✓	Y	129.9996	99.9996	10.0000	1.0000	0.1000	0.0200	12/17/07	1348	GRP	55	69	40

QC Services Audit 11/17/07

SCALE: SARTORIUS  
 MODEL: CP224S  
 SN: 17050374

WOODSTOVE DATA SHEET 4-4 SCALE QC RECORD SHEET

FROM: 12/2/04  
 THROUGH: 2/3/08

Level	brated,	Weights	100 g	10 g	1.0 g	100 mg	20 mg	Date	Time	Tech	Wet	Dry	% RH
✓	N	129.9996	99.9996	10.0000	1.0000	0.1000	0.0200	12/8	12:15	ATM	57	73	35
✓	N	129.9996	99.9996	10.0000	1.0000	0.1000	0.0200	12/8	19:10	ATM	57	72	38
✓	N	129.9997	99.9996	10.0000	1.0000	0.1000	0.0199	12/9	19:35	ATM	55	72	31
✓	Y	129.9996	99.9996	10.0000	1.0000	0.1000	0.0200	12/10	19:53	ATM	56	72	34
✓	N	129.9997	99.9997	10.0000	1.0000	0.1000	0.0199	12/11	16:18	GRP	57	76	28
✓	N	129.9997	99.9996	10.0000	1.0000	0.1000	0.0199	12/12	5:05	GRP	56	74	30
✓	N	129.9996	99.9996	9.9999	0.9999	0.1000	0.0199	12/13	3:07	GRP	55	73	29
✓	N	129.9996	99.9996	9.9999	0.9999	0.1000	0.0199	12/14	13:21	GRP	57	75	31
✓	N	129.9996	99.9996	9.9999	0.9999	0.1000	0.0199	12/15	16:02	GRP	57	75	31
✓	Y	129.9996	99.9997	9.9999	0.9999	0.1000	0.0199	12/17	08:17	GRP	55	73	29
✓	N	129.9997	99.9997	10.0000	1.0000	0.1000	0.0199	12/18	08:53	GRP	58	75	34
✓	N	129.9997	99.9997	10.0000	1.0000	0.1000	0.0199	12/19	08:12	GRP	55	72	31
✓	Y	129.9995	99.9996	10.0000	1.0000	0.1000	0.0199	12/20	09:16	GRP	57	71	41
✓	Y	129.9998	99.9997	10.0000	1.0000	0.1000	0.0199	12/21	10:35	ATM	55	70	36
✓	N	129.9997	99.9996	10.0000	1.0000	0.1000	0.0200	12/22	14:54	ATM	54	66	44
✓	N	129.9996	99.9996	10.0000	1.0000	0.1000	0.0200	12/23	09:15	ATM	57	70	44
✓	N	129.9996	99.9996	9.9999	0.9999	0.1000	0.0199	12/26	12:30	ATM	57	70	44
✓	N	129.9996	99.9997	10.0000	1.0000	0.1000	0.0200	12/27	10:30	ATM	56	72	34
✓	N	129.9998	99.9997	9.9999	0.9999	0.1000	0.0200	1/8/08	13:42	GRP	54	68	38
✓	N	129.9997	99.9997	10.0000	1.0000	0.1000	0.0200	1/9/08	09:42	GRP	55	70	36
✓	N	129.9997	99.9997	10.0000	1.0000	0.1000	0.0199	1/11/08	10:40	ATM	59	73	42
✓	Y	129.9996	99.9997	10.0000	1.0000	0.1000	0.0199	1/16/08	2:21	GRP	51	72	18
✓	N	129.9999	99.9998	10.0000	1.0000	0.1000	0.0199	1/17/08	12:37	GRP	56	71	37
✓	N	129.9998	99.9998	10.0000	1.0000	0.1000	0.0200	1/18/08	11:16	GRP	56	71	37
✓	Y	129.9995	99.9996	9.9999	0.9999	0.1000	0.0199	1/21/08	14:26	GRP	56	72	34
✓	N	129.9995	99.9996	10.0000	1.0000	0.1000	0.0199	1/22/08	15:13	GRP	56	71	37
✓	Y	129.9996	99.9996	9.9999	0.9999	0.1000	0.0199	1/23/08	08:05	GRP	54	69	36
✓	Y	129.9996	99.9996	10.0000	1.0000	0.1000	0.0200	1/24/08	07:58	GRP	54	70	33
✓	N	129.9998	99.9997	10.0000	1.0000	0.1000	0.0199	1/24/08	14:50	GRP	56	71	37
✓	N	129.9997	99.9996	10.0000	1.0000	0.1000	0.0200	1/31/08	15:05	GRP	55	69	38
✓	N	129.9997	99.9996	10.0000	1.0000	0.1000	0.0199	2/1/08	10:29	GRP	54	69	36
✓	N	129.9996	99.9996	9.9999	0.9999	0.1000	0.0199	2/2/08	16:20	ATM	56	72	41
✓	N	129.9996	99.9996	10.0000	1.0000	0.1000	0.0200	2/3/08	17:10	ATM	57	70	44

SCALE: SARTORIUS

ANALYTICAL BALANCE QC RECORD SHEET

WOODSTOVE DATA SHEET 4-4

MODEL: CP222AS

FROM: 12/30/08

SN: 170550374

THROUGH: 2/17/09

Level	Recall	140 g	100 g	10 g	1.0 g	100 mg	20 mg	Weight	Date	Time	Tech	Wet Bulb	Dry Bulb	% RH
✓	N	139.9993	99.9993	9.9999	1.0000	0.1000	0.0199	0.0199	12/30/08	1430	ARM	58	72	42
✓	N	139.9995	99.9995	9.9999	1.0000	0.1000	0.0199	0.0199	12/30/08	1057	GRP	60	76	38
✓	N	139.9994	99.9994	9.9999	1.0000	0.1000	0.0200	0.0200	12/31/08	1019	ATM	59	72	45
✓	N	139.9994	99.9994	9.9999	1.0000	0.1000	0.0200	0.0200	12/31/08	1112	ARM	59	72	45
✓	N	139.9994	99.9994	9.9999	1.0000	0.1000	0.0200	0.0200	12/31/08	1050	ARM	60	75	37
✓	N	139.9994	99.9994	9.9999	1.0000	0.1000	0.0199	0.0199	12/31/08	1157	PDG	58	75	34
✓	N	139.9994	99.9994	9.9999	1.0000	0.1000	0.0199	0.0199	1/6/09	1845	ATM	60	75	37
✓	N	139.9995	99.9995	9.9999	1.0000	0.1000	0.0199	0.0199	1/7/09	1530	GRP	58	70	47
✓	N	139.9994	99.9994	9.9999	1.0000	0.1000	0.0199	0.0199	1/8/09	1356	PDG	60	72	49
✓	Yes	139.9993	99.9993	9.9999	1.0000	0.1000	0.0200	0.0200	1/09/09	1023	PDG	58	72	42
✓	Yes	139.9993	99.9993	9.9999	1.0000	0.1000	0.0199	0.0199	1/11/09	1128	SRP	55	72	31
✓	NO	139.9994	99.9994	9.9999	1.0000	0.1000	0.0199	0.0199	1/12/09	0845	PDG	59	75	38
✓	NO	139.9993	99.9993	9.9999	1.0000	0.1000	0.0200	0.0200	1/13/09	0825	JRP	58	74	37
✓	Yes	139.9993	99.9993	9.9999	1.0000	0.1000	0.0199	0.0199	1/14/09	1212	PDG	57	72	36
✓	NO	139.9993	99.9993	9.9999	1.0000	0.1000	0.0199	0.0199	1/14/09	1420	GRP	59	75	37
✓	Yes	139.9994	99.9994	9.9999	1.0000	0.1000	0.0199	0.0199	1/15/09	1128	GRP	58	74	37
✓	NO	139.9994	99.9994	9.9999	1.0000	0.1000	0.0199	0.0199	1/20/09	0950	PDG	58	74	37
✓	Yes	139.9993	99.9993	9.9999	1.0000	0.1000	0.0199	0.0199	1/20/09	1230	PDG	56	71	37
✓	NO	139.9993	99.9993	9.9999	1.0000	0.1000	0.0199	0.0199	1/20/09	1613	SRP	57	73	35
✓	NO	139.9993	99.9993	9.9999	1.0000	0.1000	0.0200	0.0200	1/22/09	1136	ATM	57	72	38
✓	NO	139.9993	99.9993	9.9999	1.0000	0.1000	0.0199	0.0199	1/23/09	1150	PDG	58	75	33
✓	YES	139.9992	99.9992	9.9999	1.0000	0.1000	0.0200	0.0200	1/26/09	1359	SRP	56	71	35
✓	NO	139.9994	99.9994	9.9999	1.0000	0.1000	0.0199	0.0199	1/27/09	1230	PDG	57	72	31
✓	NO	139.9993	99.9993	9.9999	1.0000	0.1000	0.0200	0.0200	1/29/09	1452	ATM	61	75	41
✓	YES	139.9993	99.9993	9.9999	1.0000	0.1000	0.0199	0.0199	1/29/09	1436	GRP	58	77	29
✓	NO	139.9995	99.9995	9.9999	1.0000	0.1000	0.0199	0.0199	1/30/09	1256	PDG	60	72	49
✓	NO	139.9993	99.9993	9.9999	1.0000	0.1000	0.0199	0.0199	2/1/09	1200	ATM	59	74	37
✓	NO	139.9993	99.9993	9.9999	1.0000	0.1000	0.0199	0.0199	2/2/09	1350	GRP	58	77	29
✓	Yes	139.9995	99.9995	9.9999	1.0000	0.1000	0.0199	0.0199	2/5/09	1118	PDG	59	72	45
✓	NO	139.9995	99.9995	9.9999	1.0000	0.1000	0.0199	0.0199	2/6/09	1150	GRP	57	74	33
✓	NO	139.9994	99.9994	9.9999	1.0000	0.1000	0.0200	0.0200	2/9/09	1018	ATM	49	70	19
✓	NO	139.9994	99.9994	9.9999	1.0000	0.1000	0.0199	0.0199	2/16/09	1501	PDG	61	78	36
✓	NO	139.9993	99.9993	9.9999	1.0000	0.1000	0.0200	0.0200	2/17/09	1139	SRP	56	72	35

WOODSTOVE DATA SHEET 4-4 ANALYTICAL BALANCE QC RECORD SHEET

SCALE: SARTORIUS

FROM: 2/10/09

MODEL: CP224S

THROUGH:

SN: 17050374

Level	Recall	140 g		100 g		10 g		1.0 g		100 mg		20 mg		Wet		Dry	
		brated	Weights	Weight	Weight	Weight	Weight	Weight	Weight	Weight	Weight	Weight	Weight	Weight	Tech	Bulb	Bulb
Y	Y	139.9993	99.9993	99.9994	9.9999	1.0000	0.1000	0.0199	0.0199	2/10/09	1800	ATM	55	70	36		
Y	Y	139.9993	99.9994	99.9994	9.9999	1.0000	0.1000	0.0199	0.0199	2/19/09	1248	TRP	56	73	32		
Y	Y	139.9993	99.9994	99.9994	9.9999	0.9999	0.1000	0.0199	0.0199	2/20/09	1018	PDG	57	74	33		
Y	Y	139.9993	99.9994	99.9994	9.9999	1.0000	0.1000	0.0200	0.0200	2/21/09	1519	ATM	60	77	35		
Y	Y	139.9993	99.9993	99.9993	9.9999	1.0000	0.1000	0.0199	0.0199	2/22/09	1222	ATM	77	59	37		
Y	Y	139.9994	99.9994	99.9994	9.9999	0.9999	0.1000	0.0199	0.0199	2/23/09	1406	PDG	58	70	48		
Y	No	139.9994	99.9997	99.9997	9.9999	1.0000	0.1000	0.0800	0.0800	2/24/09	0953	ATM	59	76	35		
Y	Yes	139.9995	99.9995	99.9995	9.9999	1.0000	0.1000	0.0899	0.0899	2/25/09	123	PDG	60	76	38		
Y	Yes	139.9994	99.9994	99.9994	9.9999	1.0000	0.1000	0.0199	0.0199	2-26/09	1258	TRP	55	70	36		
Y	Yes	139.9993	99.9993	99.9993	9.9999	1.0001	0.1001	0.0200	0.0200	2/20/09	1220	ATM	57	74	33		
Y	Yes	139.9995	99.9995	99.9995	9.9999	0.9999	0.1000	0.0199	0.0199	3/3/09	1431	PDG	59	76	35		
Y	NO	139.9993	99.9995	99.9995	9.9999	1.0000	0.1000	0.0199	0.0199	3/4/09	1556	TRP	56	70	40		
Y	NO	139.9994	99.9994	99.9994	9.9999	1.0001	0.1001	0.0200	0.0200	3/5/09	1350	ATM	60	75	40		
Y	NO	139.9993	99.9993	99.9993	9.9999	1.0000	0.1000	0.0200	0.0200	8/9/09	0850	ATM	57	71	41		
Y	Yes	139.9993	99.9993	99.9993	10.0000	1.0001	0.1000	0.0200	0.0200	3/8/09	1323	ATM	55	70	36		
Y	Yes	139.9993	99.9993	99.9993	9.9999	1.0000	0.1000	0.0199	0.0199	3/10/09	1212	PDG	50	75	10		



Woodstove Particulate  
Catch Processing Sheet  
Woodstove Data Sheet #5  
EPA M5G-1

Unit: Kuma Ashwood  
Run: EPA 6  
Date: 2/27/09  
Technicians: ATM/...  
Revised 1/16/98-Data Sheet #5

Filters

Filter # (Front) 716 Beaker # 26  
Final Wt. .6888 g MI 55  
Tare Wt. .6690 g Desc. Acetone  
Net Wt. .0198 g ✓

Final Wt. 71.7927 g ✓  
Tare Wt. 71.7877 g ✓  
Net Wt. 1.0050 g ✓

Filter # (Rear) 715 Beaker # \_\_\_\_\_  
Final Wt. .6750 g MI \_\_\_\_\_  
Tare Wt. .6744 g Desc. \_\_\_\_\_  
Net Wt. .0006 g ✓

Final Wt. \_\_\_\_\_ g  
Tare Wt. \_\_\_\_\_ g  
Net Wt. \_\_\_\_\_ g

Acetone Blank Calculation:

Blank Date: 12/8/07

Blank Beaker # 25 Final Wt. 72.6511 g  
MI 50 Tare Wt. 72.6512 g  
Desc. Acetone Net Wt. - .0001 g = 0.0000  
.0000 g ÷ 50 ml = .0000 g/ml

Blank Residue Value Calculation:

.0000 g/ml acetone X 55 ml acetone = .0000 g  
Blank Residue Value

Total Particulate Catch Calculation

Filter: .0198 g ✓  
Filter: .0006 g ✓  
Beakers: .0050 g - .0000 g = .0050 g ✓  
Total Catch Blank Residue Value  
Total Catch = .0254 g ✓

Unit KUMA Ashwood  
 Run # EPA 6  
 Date 2/27/09  
 Technician ASTM JLP PDG  
 WST6-Form1, Rev8/96

MISCELLANEOUS TEST DATA  
 WOODSTOVE DATA SHEET #8

Useable Firebox Dimensions: See QC Section Useable Volume: 2.094 ft<sup>3</sup>

Dilution Tunnel Draft (If applicable): Start .000 Stop .000 " Hg  
 Test Chamber Air Velocity: Start: 00.0 Stop: 0.00 Avg: .000 ft/min

Wet Bulb/ Start: WB: 56 °F DB: 73 °F .95 % Amb Moisture 32 %RH  
 Dry Bulb Stop: WB: 57 °F DB: 73 °F 1.05 % Amb Moisture 35 %RH  
 $\bar{X} = 1.00$  % Ambient Moisture  $\bar{X} = 33.5$  % Relative Humidity (RH)

Empty Stove Wt: 440.2 lbs.  
 Empty Stove Wt with Stack (Inc. Oil Seal) Wet: 765.5 lbs. Dry: 765.6 lbs. 767.6  
 Empty Stove Wt with Stack and Ash Ash: — lbs. Total: — lbs.

Kindling Wt. TOTAL 5.2 Paper: 0.4 lbs. Wood: 7.8 lbs.

Pre Burn Fuel Wt. 11.454 + 14.138 + 10.686 Total: 36.278 lbs.  
 Total Kindling and Pre Burn Fuel Wt 41.478 lbs.

Coal Bed Wt-lbs: Range (3.3 - 2.7) 768.9 - 768.3 lbs. Actual: 2.7 lbs.  
768.13

Allowable Amount of Charcoal that can be removed:  
 Coal Bed Wt. Range 3.3 + 2.5  $12 \times .25 =$  0.7 lbs.  
 Upper Wt. Lower Wt.

Test Fuel Wt-lbs: Ideal 14.7 lbs. Range: 16.1 - 13.2 lbs. Actual: 13.314 lbs.

Test Fuel Size (pcs.) (.75 x 1.5 x 5" Flanges) 1,888 lbs. 16 Pcs.  
 2 x 4's x 16.4375 " 3 Pcs 6.252 lbs. 46.96 %  
 4 x 4's x ↓ " 2 Pcs 7.062 lbs. 53.04 %

4.9966 Kg

Est. Dry Burn Rate (Kg/Hr.)  $\frac{13.314 - (13.314 \times .17264)}{2.2046} \times \frac{60}{250} =$  1.1992 Est. Dry Burn Rate (Kg/Hr)

Est EPA Heat Output (HO<sub>E</sub>) (19,140) x 63 x 1.1992 = 14,460 Est Heat Output (HO<sub>E</sub>) BTU's/Hr  
 (Avg BTU's/Hr) 100

Comments: 240 mins = 1.2491 Kg/hr.

Stove Operating Data  
Woodstove Test Data Sheet #9  
Cold Start

Unit: Common Ashwood  
Run: EPA 6  
Date: 2/27/09  
Technician(s): AFM JRP POG  
Data Sheet #9-Rev 1/98-Pg.2

Fire Started: 10:03

Warm up and Preburn: Primary Air: Wide open from ignition until the start of preburn when the primary air control(s) was (were) adjusted to the run setting of 0.5235" open. At the run setting until the start of the test.

2.5" on Threaded Rod  
Secondary Air: No Controls. Naturally Drafted

Secondary Burn Bypass: N/A

Charcoal Bed Preparation: Broke up, raked and leveled the coal bed prior to the addition of each warm up/pre burn fuel charge. Starting 1:30 before the start of the test, broke up, raked and leveled the coal bed. In stove for 25 seconds.

Test: Door wide open during loading 1 min 1 sec, then closed

Primary Air: Wide open from the start of the test (0:00) until 4:45. Adjusted to the run setting of 0.5235" between 4:45 and 5:00. At the run setting of 0.5235" at 5:00 into the run.

Secondary Air: No Controls. Naturally Drafted.

Secondary Burn Bypass: N/A

Fan: ON/OFF during the warm up, ON/OFF Low during the preburn, ON/OFF at the start of test, ON/OFF for the first 30 minutes of test, ON/OFF Low at 30 minutes into test, ON/OFF for the rest of test.

Test Run Anomalies: Much better start than Run 5.

WOODSTOVE OPERATING DATA  
 WOODSTOVE DATA SHEET #9A-1

Wood Data: Kindling: A mix of the below grades

	Size	Mill	Grade	Species
Pre Burn	2X4	Forest Grove	#2 & BTR	D. Fir, Sfo. Gran
Test Fuel	2X4	Forest Grove	#2 & BTR	D. Fir, Sfo. Gran
	4X4	Forest Grove	#1	D. Fir, Sfo. Gran

All grades WCLB Rules unless otherwise noted.

Warm up Information:

1st Warm up/Pre Burn Fuel charge (11.454 lbs) added at 1020.  
 2nd Warm up/Pre Burn Fuel charge (14.138 lbs) added at 1115.  
 3rd Warm up/Pre Burn Fuel charge (10.686 lbs) added at 1216.  
 4th Warm up/Pre Burn Fuel charge (\_\_\_\_\_ lbs) added at \_\_\_\_\_.  
 5th Warm up/Pre Burn Fuel charge (\_\_\_\_\_ lbs) added at \_\_\_\_\_.  
 6th Warm up/Pre Burn Fuel charge (\_\_\_\_\_ lbs) added at \_\_\_\_\_.  
 7th Warm up/Pre Burn Fuel charge (\_\_\_\_\_ lbs) added at \_\_\_\_\_.  
 8th Warm up/Pre Burn Fuel charge (\_\_\_\_\_ lbs) added at \_\_\_\_\_.

1<sup>st</sup> Rick 4-12", 4-16" 2X4's.  
 2<sup>nd</sup> Rick 8-16" 2X4's

3<sup>rd</sup> Rick 4-12", 3-16" 2X4's

The coals were scooped out of the stove immediately prior to adding the Third pre burn/warm up fuel charge. The stove lost 0 lbs. 2.0 lbs. of coals were put back in the stove after the scoop.

All pre burn/warm up fuel pieces were either 12 or 16 inches long. All preburn pieces/fuel charges were "ricked" in the stove. The pieces in the bottom layer in each rick contained 2 pcs that were 12 or 16 inches long and were loaded flat and perpendicular to the door. The pieces in the second layer in each rick were loaded on their side (edge) approximately parallel to the door and contained 3 or 4 pcs 16 inches long. The third layer (and fourth layer if present) was loaded flat, perpendicular to the door and contained 2 pcs 12 or 16 inches long. The majority of the pieces in each rick were in the second layer which had an approximate 0.5-1.0" space between pieces. (The loading directions indicate the direction of the longest dimension on each piece relative to the loading door opening.) Each pre burn/warm up fuel charge normally weighs within the weight range allowed for the actual test fuel charge

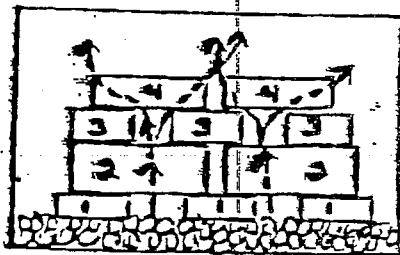
WOODSTOVE OPERATING DATA  
WOODSTOVE DATA SHEET #9A-2

Unit EX-1000-18207 WUC  
Run # EPIG  
Date 2/27/09  
Technician ATM URP PDG  
Page 2 of 4  
WS17-Form2-A, Rev 6/90

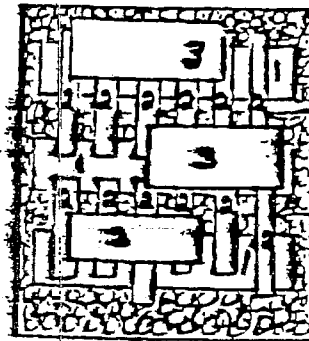
Warm up Information (cont.):

Each warm up/preburn fuel charge was ricked in exactly (as much as possible) the same manner and the weight of each rick was usually within the allowable weight range for the test fuel charge. The physical arrangement and alignment of each rick was designed to accomplish three (3) things: (1) The bottom layer was nestled firmly into the coal bed and was as close to being level with the bottom of the stove as possible, thus providing a stable loading platform for the rest of the rick, keeping it in a ricked state (as opposed to a col-lapsed or fallen down state) until the rick reached the charcoal stage and sags or collapses of its own accord. (2) It enhances the flow of primary air through the ricked preburn fuel charge, for the primary air would flow through the spaces between the pieces in the first layer and then up through the spaces between the pieces in the second, third and, if present, fourth layers. (3) It maximized, as much as possible, the surface to volume ratio of each preburn fuel charge, thereby allowing the fire immediate access to as much wood surface as possible and, thereby, insuring uniform charcoalization. All three of these enhance combustion and so get the stove as hot as possible during the warm up period, thereby maximizing the amount of heat (BTU's) stored in the stove. The actual preburn was not started until the stove surface temperatures had maximized and stabilized, thus indicating that the amount of heat stored in the stove had peaked. For this stove, the thermal storage was monitored using the Stove Top TIC

surface temperature(s) and the peak value(s) obtained were 1062 of.



Front View



Top View

The arrows indicate the direction of the air flow through the rick.

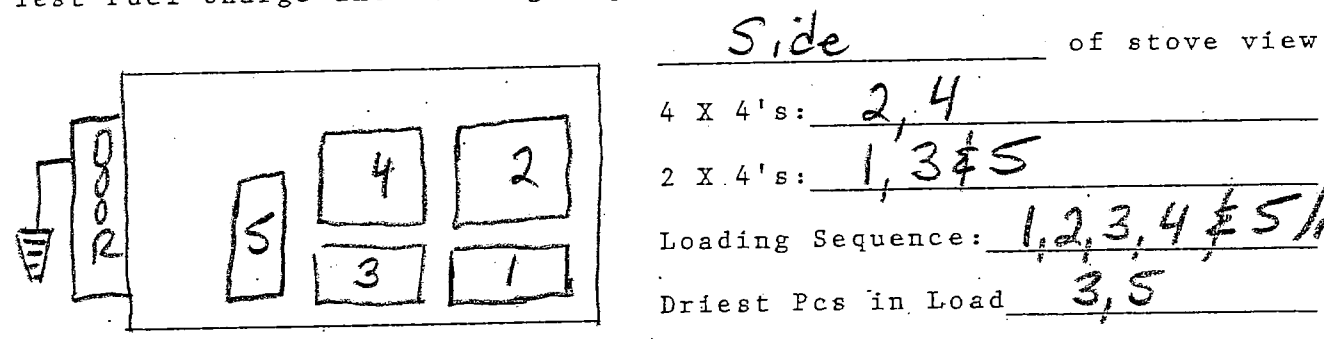
The primary air was adjusted to the run setting of 0.5235" open 3.6 lbs above the upper charcoal bed weight. 2.500" on the threaded rod.

Additional Comments: Test Start Sequence: ① Turned Fan OFF  
② Adjusted Primary Air Control to Wide Open ③ Opened door  
④ Loaded Fuel Charge ⑤ Cleared coals away from in front of the LPAO ⑥ closed door

TOTAL ELAPSED Time: 1:00  
Photo Taken @ ~ 2:30

Test Fuel Charge Loading Information:

Test Fuel Charge and Loading Sequence Diagram



Loaded the test fuel charge on an essentially level, Medium sized, hot coal bed (in appearance, color and temperature

for a Med load (1.0-1.25) burn rate. Load: 1:01 Ignition: 1:00  
1:05 VC (vertical column of flame) up to baffle.

1:10 Secondaries Igniting  
2:30 Photo, Secondaries approximately full width of  
of PC4, Front Tube starting to ignite.

4:45-5:00 Primary Air Control (PAE) adjusted to ON setting.

5:00 Flames decreasing. Maintained a hot pocket of coals under and behind pcs with a thin VC up to baffle w/ secondaries at top and sides of VC

6:05 13.1 / 1.44 (% CO<sub>2</sub> / % CO)

7:20 Big Pop, Blew a small piece of wood/charcoal

WOODSTOVE OPERATING DATA  
 WOODSTOVE DATA SHEET #9A-4

Additional Comments: (7:20 cont.) out of the bottom of pc 5, the VC is widening at base a little, still have secondaries

- 8:12 VC increasing  
 9:15 Medium (M) Smoke  
 10:38 7.0 / 1.04 M  
 11:14 Flames on the bottom edge of 5 left of center  
 12:39 Velocity in secondaries are lifting off the tube.  
 13:03 7.75 / 1.25 M <sup>Left end</sup>  
 15:22 Secondaries full width of pc 4 8.8 / 1.30 MH  
 16:10 " forward past front tube in center  
 17:41 10:46 / 1.12 M / MH  
 18:04 Secondaries almost to right end of P<sub>4</sub>  
 18:23 11.0 / 1.16. Flames on center top front edge of 5  
 18:42 Bal M / ML  
 19:15 Out 11.28 / 1.21  
 19:49 In Bal again 12.29 / 1.22 L / ML Front tube is igniting.  
 20:48 13.0 / 1.19 L  
 24:00 Lots of small pops  
 25:00 15.9 / 1.12 L / ML  
 30:00 Fan On Low 16.02 / 1.04

Unit: Kuma Asst  
 Run: EPH 6  
 Date: 2/27/04  
 Technician: ATM JRP POG  
 WST1-Form7-Rev11/89

FUEL MOISTURE  
 WOODSTOVE TEST DATA SHEET #10

5 kg = 11.024 lbs      1 kg = 2.204 lbs.  
 Room Temperature: 61.1 °F      Correction Factor: 1.0

NOTE: Record readings to the nearest 0.5% moisture  
 Uncor Values are corrected for temperature: Yes  No   
 Time Test Fuel Moisture Readings taken at: 10:50  
 Calibration Checks: X  Y  12.0 11.8 22.0 22.0

Pc #	Dimen	Use	Top		Bottom		Side		Piece Avg Corrected
			Uncor	Cor	Uncor	Cor	Uncor	Cor	
1	3 pcs	K	7.5	7.85	8.0	8.4	8.0	8.4	8.217
2									
3									
4	2x4-9'	P	22	23.7	22	23.7	21	22.6	23.333
5			18	19.2	19	20.3	19	20.3	19.933
6			20	21.4	20	21.4	20.5	22.0	21.600
7			19	20.3	19.5	20.9	19	20.3	20.500
8	✓	✓	19.5	20.9	19.5	20.9	19	20.3	20.700
9									(106.066)
10									
11									
12	2x4-	T	19	20.3	19	20.3	19	20.3	20.300
13			21.5	23.1	21.5	23.1	21.5	23.1	23.100
14	✓	✓	19	20.3	19	20.3	19	20.3	20.300
15									
16	4x4-	T	17.5	18.6	20.5	22.0	18.5	19.8	20.133
17	✓	✓	19.5	20.9	19	20.3	19	20.3	20.500
18									(104.333)
19	SPACERS	T	19	20.3	19	20.3	18	19.2	19.933
20									(OUT SPACERS)

1.408  
 1.898  
 1.592  
 3.044  
 3.476  
 1.888

	Kindling	Pretest Fuel	Test Load
% Moisture - Dry Basis:	8.217 %	21.2132 %	20.8666 %
% Moisture - Wet Basis:	7.593 %	17.501 %	17.2642 %

To obtain Wet from Dry:  $\frac{100 \times \% \text{ Dry Rdg.}}{100 + \% \text{ Dry Rdg.}} = \% \text{ Moisture, Wet Basis}$   
13.314      7.062

Acceptable Ranges: 16-20% wet; 19-25% dry  
 (17.5 - 22.5 on Meter [Uncor reading] at 70°F)

Key for Use: K= Kindling P= Pretest Fuel T= Test Fuel

1 11.454  
 2 14.138  
 3 10.686



WOOD DENSITY DETERMINATION  
WOODSTOVE TEST DATA SHEET #11

2X4

Unit: KUMA Ashwood  
Run#: EPA 6  
Date: 2/27/09  
Technician: ATM JRP PDG  
WST2-form11-Rev 6/90

Wood Piece: Nominal Dimensions: 3.5" x 3.5" x 1.5"

Depth (D): 3.875 cm

Width (W): 8.945 cm

Length (L): 9.005 cm

8.975 cm

9.000 cm

8.960 cm

Length  $\bar{X}$  = 8.9850 cm

Volume: 311.437 cm<sup>3</sup>  
(D X W X L)

MOISTURE: Room Temperature: 61.1 °F Correction Factor: +1.0

Uncorrected Meter Readings Corrected for temperature: Yes  No

NOTE: Record moisture meter readings to the nearest 0.5%

	Uncor	Cor	%
Top:	20	21.4	%
Bottom:	21.5	23.1	%
Side:	20	21.4	%
$\bar{X}$ :		21.967	%

Avg % Moisture (Dry) 21.967 %

Aug % Moisture (Wet) 18.011 %

Scale: Leveled In  Out

Zeroed: In  Out

Wet Weight: 179.1 g Dry Weight: 146.5 g

% Moisture Dried Basis: 18.202 %  
[1 - (Dry Wt ÷ Wet Wt)] X 100

	Date	Time	Temp
Into Dryer	<u>2/27/09</u>	<u>1540</u>	<u>190</u> °F
Out of Dryer	<u>4/2/09</u>	<u>1245</u>	<u>196</u> °F

(Minimum Time in Dryer: 24 hrs.) Minimum Dryer Temp 100°C (212°F)

Density = 146.5 g (dry wt) ÷ 311.437 cm<sup>3</sup> (volume) = 0.4704 g/cm<sup>3</sup>

Pellet Fuel Moisture Content Determination

Tare Beaker Wt. \_\_\_\_\_ g

Wet Wt: \_\_\_\_\_ g - \_\_\_\_\_ g = \_\_\_\_\_ g

Gross Wet Wt. Tare Beaker Wt. Net Wet Wt.

Dry Wt: \_\_\_\_\_ g - \_\_\_\_\_ g = \_\_\_\_\_ g

Gross Dry Wt. Tare Beaker Wt. Net Dry Wt.

% Moisture Dried Basis: \_\_\_\_\_ %  
[1 - (Net Dry Wt ÷ Net Wet Wt.)] X 100













PRE AND POST TEST ZERO/SPAN CHECK  
WOODSTOVE DATA SHEET #15-1

Site: Myren Consulting, Woodstock, VA Date: 2/27/09 Analyte: CO<sub>2</sub>

Source: Kuma Ashwood Run #: EPA 6

Zero Cyl #: TC3AAM154 Conc. 00.0 % CO<sub>2</sub> Cyl Press: 1490 psi

Certified by: Oxarc Date: 11/12/07

Span Cyl #: AS90457 Conc. 125 % CO<sub>2</sub> Cyl Press: 1460 psi

Certified by: Matheson Tri Gas Date: 2/2/09

Analyzer: Make: Horiba Model: FIR-2000 SN: 607024

Range: 0 - 25.0% CO<sub>2</sub> Analyzer Output: 0 - 1.0 v.

Flow: 1.5 SCFH Measured by: Rotameter  X Flowmeter:

EPA Span Value = 25.0% CO<sub>2</sub>  
EPA Control Limits = + 2.5% of 25.0% CO<sub>2</sub> = + 0.625% CO<sub>2</sub>

Pre Run Audit: By: A.T. Myren Time: 1255 Temp: 74 °F

Audit Results

Point #	Expected Response			Actual Response			+ Conc. Difference	Δ %
	Meter	DVM	%	Meter	DVM	%		
Zero	00.0	.000	00.0	00.0	.000	05.453	+0.05453	+0.22
Span	50.0	.500	125	50.0	.499	12.386	-0.1142	-0.91

Comments:

Post Run Audit: By: A.T. Myren Time: 1343 Temp: 73 °F

Audit Results

Point #	Expected Response			Actual Response			+ Conc. Difference	Δ %
	Meter	DVM	%	Meter	DVM	%		
Zero	00.0	.000	00.0	00.0	.001	07.925	+0.07925	+0.32
Span	50.0	.500	125	50.0	.500	12.4105	-0.08953	-0.72

Comments:

+ Conc. Difference = Act % - Exp (Std) %  
 Zero % Difference =  $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Full Scale Value}} \times 100$   
 Span % Difference =  $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Exp \% (ppm)}} \times 100$



PRE AND POST TEST ZERO/SPAN CHECK  
WOODSTOVE DATA SHEET #15-3

Colville

Site: Myren Consulting, Woodinville, WA Date: 2/27/09 Analyte: CO

Source: Kuma Ashwood Run #: EPA 6

Zero Cyl #: TC 3AAM154 Conc. 00.0 % CO Cyl Press: 1490 psi

Certified by: Oxarc Date: 11/12/07

Span Cyl #: AS 90457 Conc. 20 % CO Cyl Press: 1460 psi

Certified by: Matheson Tri Gas Date: 2/2/09

Analyzer: Make: HORIBA Model: MEXA 311-6E SN: GE-30075

Range: 0 - 10.0% CO Analyzer Output: 0 - 10 V

Flow: 1.5 SCFH Measured by: Rotameter: X Flowmeter:

EPA Span Value = 5.0% CO  
EPA Control Limits = +2.5% of 5.0% CO = + 0.125% CO

Pre Run Audit: By: A.P. Myren Time: 1255 Temp: 74 °F

Audit Results

Point #	Expected Response			Actual Response			+ Conc. Difference	Δ %
	Meter	DVM	%	Meter	DVM	%		
Zero	00.0	00.0	00.0	00.0	.000	00.0443	-0.00443	-0.04
Span	2.00	.200	2.00	2.00	.199	1.9959	-0.0041	-0.21

Comments:

Post Run Audit: By: A.P. Myren Time: 1835 Temp.: 73 °F

Audit Results

Point #	Expected Response			Actual Response			+ Conc. Difference	Δ %
	Meter	DVM	%	Meter	DVM	%		
Zero	00.0	00.0	00.0	0.00	.000	00.0443	-0.00443	-0.04
Span	2.00	.200	2.00	1.98	.198	1.9858	-0.01416	-0.71

Comments:

+ Conc. Difference = Act % - Exp (Std) %  
 Zero % Difference =  $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Full Scale Value}} \times 100$   
 Span % Difference =  $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Exp \% (ppm)}} \times 100$

Unit: Kumar Ashwood  
 Run: PPA-C  
 Date: 2/27/09  
 Technicians: ATM JRP PDG  
 WS 6-Form3-Rev11/89

QUALITY CHECKS  
 WOODSTOVE DATA SHEET #16

Ambient = Tr: \_\_\_\_\_ °F T/C#30: \_\_\_\_\_ °F  
 Thermocouple Check (at ambient): T/C#1: \_\_\_\_\_ °F; T/C#2: 69.0 °F;  
 T/C #3: 68.0 °F; T/C #4: 60.2 °F; T/C #5: 60.8 °F;  
 T/C #6: 60.0 °F; T/C #7: 59.5 °F; T/C #8: 60.3 °F;  
 T/C #9: 60.1 °F; T/C #10: 62.2 °F; T/C #11: 61.1 °F;  
 T/C #12: \_\_\_\_\_ °F; T/C #13: 60.9 °F; T/C #14: 57.2 °F;  
 T/C #15: 62.2 °F; T/C #16: 60.0 °F; T/C #17: 61.6 °F;  
 T/C #18: \_\_\_\_\_ °F; T/C #19: \_\_\_\_\_ °F; T/C #20: \_\_\_\_\_ °F;  
 T/C #21: \_\_\_\_\_ °F; T/C #22: \_\_\_\_\_ °F; T/C #23: \_\_\_\_\_ °F;  
 T/C #24: \_\_\_\_\_ °F; T/C #25: \_\_\_\_\_ °F; T/C #26: \_\_\_\_\_ °F;

Comments: \_\_\_\_\_

Thermocouple Readout: Pretest Zero/Span Check and Calibration:  
 Zero (°F) : -0.2 °F Adj to: \_\_\_\_\_ °F Post Test Check Zero (0°F): 0.9 °F % Difference +0.20  
 Span (2000°F): 1999.9 °F Adj to: \_\_\_\_\_ °F Span (2000°F): 2002.3 °F +0.01

(Allowable % Difference = 1.5%. Use formulas on Woodstove Data Sheet #15 to calculate % Difference) In degrees Absolute.

Thermocouple Readout Pretest Linearity Check  
 0°F = -0.2 °F; 200°F = 201.6 °F; 400°F = 399.0 °F;  
 600°F = 601.3 °F; 800°F = 801.5 °F; 1000°F = 1000.7 °F;  
 1200°F = 1198.4 °F; 1400°F = 1399.4 °F; 1600°F = 1599.8 °F;  
 1800°F = 1800.0 °F; 2000°F = 1999.9 °F

Combustion Gas (CO<sub>2</sub>, O<sub>2</sub>, CO) Train Leak Check: Pre  Post  OK PDI  
 Draft (Static) Gauge Zero Check: Pre  Post  OK PDI

Scale Check Pre (Wt, #'s): 770.5 / 765.5 = 5.0 lbs / 5.0 lbs = OK (ATM)  
 Post (Wt, #'s): 773.9 / 768.9 = 5.0 lbs / 5.0 lbs = OK (ATM)

Stack cleaned prior to the run: Yes \_\_\_\_\_ No   
 Tunnel cleaned prior to the run: Yes \_\_\_\_\_ No

MYREN CONSULTING CERTIFICATION TEST DATA

DILUTION TUNNEL CALCULATIONS  
 1'25'09, Md=28.56, Bws=4%

6" Tunnel

File Name:	Run Time (min)	PITOT DELTAP (- INCH H2O)	TNL TEMP (°F)	GAS METER RDG (ft3)	GAS METER TEMP (°F)	GAS METER DELTA H (In. H2O)	TUNNEL VELOCITY (ft/min)	PROP RATE (%)	dDGM vol std (ft3)	Tunnel Static (- Inch H2O)	SQUARE ROOT DELTA P	DRY GAS METER RDG (m3)
Manufacturer: KUMA	0	0.041	95	735.3000	69	0.900	854.68		5.096	0.160	0.2025	
Model Number: ASHWOOD	10	0.042	101	740.6540	72	0.900	869.71	101.8	5.096	0.163	0.2049	
Lab Name: MYREN	20	0.043	96	745.9640	75	0.900	876.08	98.2	5.025	0.167	0.2074	
Test Date: 3/2/09	30	0.040	97	751.3800	79	0.900	845.71	102.5	5.088	0.153	0.2000	
Run Number: EPA 7	40	0.040	99	756.6810	82	0.900	847.23	99.3	4.952	0.153	0.2000	
Meter Box Y Factor: 1.0177	50	0.039	100	761.8460	84	0.900	837.31	97.4	4.807	0.144	0.1975	
Barometric pressure (in): 28.138	60	0.041	99	767.7670	86	0.900	857.75	108.0	5.491	0.150	0.2025	
Gas meter temp (ave): 87	70	0.040	98	772.5000	88	0.900	846.47	86.7	4.373	0.152	0.2000	
delta H(ave): 0.900	80	0.040	97	777.8390	88	0.900	845.71	97.7	4.933	0.151	0.2000	
Gas meter initial reading: 735.3000	90	0.040	97	783.1730	89	0.900	845.71	97.3	4.919	0.153	0.2000	
Gas meter final reading: 887.7790	100	0.040	97	788.5270	89	0.900	845.71	97.6	4.938	0.153	0.2000	
Front catch (acetone) mg: 10.8	110	0.040	96	793.8720	90	0.900	844.95	97.0	4.921	0.154	0.2000	
first filter catch (mg): 24.8	120	0.040	94	799.2370	90	0.900	843.43	97.2	4.939	0.153	0.2000	
second filter catch (mg): -6.6	130	0.040	92	804.5940	90	0.900	841.90	96.9	4.932	0.153	0.2000	
Tunnel Flow (Qsd) (dscfm): 139.323	140	0.039	91	809.9620	90	0.900	830.56	98.2	4.942	0.150	0.1975	
Emission Rate(g/hr): 1.719	150	0.039	91	815.3390	90	0.900	830.56	98.4	4.950	0.153	0.1975	
Emission Rate(M5H): 2.853	160	0.040	91	820.7090	90	0.900	841.14	97.0	4.944	0.154	0.2000	
Avg. of Delta P Sq. Roots: 0.2012	170	0.040	91	826.0750	91	0.900	841.14	96.6	4.931	0.155	0.2000	
Vs (Avg.)(ft/min): 824.439	180	0.040	91	831.4540	91	0.900	841.14	96.8	4.943	0.154	0.2000	
Tunnel Avg. Temperature (F): 93.500	190	0.040	90	836.8340	91	0.900	840.38	96.8	4.944	0.153	0.2000	
Test time(min): 285	200	0.040	91	842.2120	91	0.900	841.14	96.8	4.942	0.155	0.2000	
Fuel Load(lb. wet): 13.330	210	0.040	91	847.5900	91	0.900	841.14	96.8	4.942	0.154	0.2000	
Wood moisture(%wet): 16.838	220	0.040	91	852.9670	91	0.900	841.14	96.8	4.941	0.154	0.2000	
Burn rate(dry kg/hr): 1.059	230	0.040	91	858.3480	91	0.900	841.14	96.9	4.945	0.155	0.2000	
Sample Volume (dscf): 141.021	240	0.040	91	863.7200	91	0.900	841.14	96.7	4.936	0.156	0.2000	
Avg. Tunnel Static (-inch H2O): 0.1544	250	0.040	90	869.0700	91	0.900	840.38	96.2	4.916	0.157	0.2000	
Room Blank Catch (mg/dscf): 0	260	0.040	90	874.4100	91	0.900	840.38	96.1	4.907	0.155	0.2000	
Emission Factor (g/kg): 1.6239	270	0.040	90	879.7630	91	0.900	840.38	96.3	4.919	0.156	0.2000	
Pitot Correction Factor: 0.97195	280	0.040	89	885.1100	91	0.900	839.61	96.1	4.913	0.155	0.2000	
front filter number: 718	285	0.040	88	887.7790	91	0.900	838.85	95.8	2.453	0.157	0.2000	
back filter number: 717				0.0000			0.00	0.0	0.000			
Beaker Number: 27	310			0.0000			0.00	0.0	0.000			
PRELIMINARY RESULTS	320			0.0000			0.00	0.0	0.000			
FINAL RESULTS:	330			0.0000			0.00	0.0	0.000			
DATA SUMMARY	340			0.0000			0.00	0.0	0.000			
MODEL: ASHWOOD	350			0.0000			0.00	0.0	0.000			
RUN: EPA 7	360			0.0000			0.00	0.0	0.000			
DATE: 3/2/09	370			0.0000			0.00	0.0	0.000			
DBR: 1.059	380			0.0000			0.00	0.0	0.000			
EMISSION RATE (g/hr)(M5H): 2.8534				0.0000			0.00	0.0	0.000			
EMISSION FACTOR (g/kg): 1.6239				0.0000			0.00	0.0	0.000			
AVG. % PROPORTIONALITY: 97.453				0.0000			0.00	0.0	0.000			

13.33  
16.838

**METHOD 5G - 1 EPA PARTICULATE SAMPLING DATA** Rev. 2/09

DATE: 3/2/09 PAGE 1 OF 2 UNIT: Kuma Ashwood RUN: EPA 7

METER BOX: 45G-P METER Y: 1.0177 FILTER #'S: (F) 718 (R) 717

.015/.015  
PRE TEST LEAK CHECK: .000 CFM @ -15.75 IN HG FILTER SIZE: 110 mm

.843/.843  
POST TEST LEAK CHECK: .000 CFM @ -15.8 IN HG PROBE LENGTH 21.0 IN

TIME		METER READING (FT <sup>3</sup> )	PITOT		TUNNEL TEMP (°F)	METER TEMP (°F)	GAS METER Δh	VAC (in Hg)
CLOCK	ELAPSED		ΔP	Pg				
1355	00	735.300	.041	-1.60	95	69	0.90	0
1405	10	740.654	.042	-1.63	101	72	1.90	0
15	20	745.964	.043	-1.67	96	75	1.90	0
25	30	751.380	.040	-1.53	97	79	1.90	0
35	40	756.681	.040	-1.53	99	82	1.90	0
45	50	761.846	.039	-1.44	100	84	1.90	0
55	60	767.767	.041	-1.50	99	86	1.90	0
1455	70	772.500	.040	-1.52	98	88	1.90	0
15	80	777.839	.040	-1.51	97	88	1.90	0
25	90	783.173	.040	-1.53	97	89	1.90	0
35	100	788.527	.040	-1.53	97	89	1.90	0
45	110	793.872	.040	-1.54	96	90	1.90	0
55	120	799.237	.040	-1.53	94	90	1.90	0
1505	30	804.594	.040	-1.53	92	90	1.90	0
15	40	809.962	.039	-1.50	91	90	1.90	0
25	50	815.339	.039	-1.53	91	90	1.90	0
35	60	820.709	.040	-1.54	91	90	1.90	0
45	70	826.075	.040	-1.55	91	91	1.90	0
55	180	831.454	.040	-1.54	91	91	1.90	0
1705	90	836.834	.040	-1.53	90	91	1.90	0

BP

00	<u>28.16</u>	<u>28.12</u>	
60	<u>28.14</u>		
120	<u>28.15</u>		
180	<u>28.14</u>		
240	<u>28.12</u>		
		AVG. =	<u>28.139</u>

Pre Test Filter  
Check Weighing  
F .6729  
R .6539

End of Test Weight  
F .6985 R .6438  
.6723 .6536  
.0262

METHOD 5G -1 EPA PARTICULATE SAMPLING DATA

Rev. 2/09

DATE: 3/2/09 PAGE 2 OF 2 UNIT: KUMMA ASHWOOD RUN: EPA7

METER BOX: 450-P METER Y: 1.0177 FILTER #'S: (F) 716 (R) 717

1.015 / 1.015  
PRE TEST LEAK CHECK: 1.000 CFM @ -15.75 IN HG FILTER SIZE: 110 mm

1.843 / 1.843  
POST TEST LEAK CHECK: 1.000 CFM @ -15.8 IN HG PROBE LENGTH 21.0 IN

TIME		METER READING (FT <sup>3</sup> )	PITOT		TUNNEL TEMP (°F)	METER TEMP (°F)	GAS METER Δh	VAC (in Hg)
CLOCK	ELAPSED		AP	Pg				
1715	2:00	842.212	1040	-1155	91	91	190	0
25	10	847.590	1040	-1154	91	91	190	0
35	20	852.967	1040	-1154	91	91	190	0
45	30	858.348	1040	-1155	91	91	190	0
55	240	863.720	1040	-1156	91	91	190	0
1805	50	869.070	1040	-1157	90	91	190	0
15	60	874.410	1040	-1155	90	91	190	0
25	70	879.763	1040	-1156	90	91	190	0
35	80	885.110	1040	-1155	89	91	190	0
40	<del>90</del> 285	887.779	1040	-1157	88	91	190	0
	00							
	10							
	20							
	30							
	40							
	50							
	60							
	70							
	80							
	90							

BP

00 28.16    285 28.12  
60 28.14    \_\_\_\_\_  
120 28.15    \_\_\_\_\_  
180 28.14    \_\_\_\_\_  
240 28.12    AVG. = 28.138

Pre Test Filter  
 Check Weighing  
 F 1.6729  
 R 1.6539

End of Test Weight  
 F 1.6723    R 1.6536

MYREN CONSULTING, INC.

Dilution Tunnel Traverse Data with 8 Traverse Points

Unit: Kuma Ashwood

Run #: EPA 7

Date: 3.2.09

Technicians: ATM GAP pg6

#12 Rev 2/16/09

Point	Location	Ap	$\sqrt{\Delta P_{trav}}$	Ap	$\sqrt{\Delta P_{cent}}$	#12 T <sub>trav</sub>	#12 T <sub>cent</sub>	Pg
W-1	0.5"	$\frac{.036}{.040}$	$\frac{.1897}{.2000}$	$\frac{.041}{.041}$	$\frac{.2025}{.2025}$	$\frac{105}{99}$	$\frac{99}{99}$	$\frac{-155}{-155}$
Center	Center							
3	4.5	$\frac{.040}{.039}$	$\frac{.2000}{.1975}$			$\frac{99}{99}$		
4	5.5	$\frac{.034}{.039}$	$\frac{.1944}{.1975}$			$\frac{102}{101}$		
S-1	0.5							
2	1.5	$\frac{.039}{.040}$	$\frac{.1975}{.2000}$	$\frac{.040}{.040}$	$\frac{.2000}{.2000}$	$\frac{99}{99}$	$\frac{100}{100}$	$\frac{-154}{-154}$
Center	Center							
3	4.5	$\frac{.038}{.039}$	$\frac{.1949}{.1975}$			$\frac{99}{99}$		
4	5.5							
Totals			$\frac{1.5640}{1.955}$		$\frac{.4075}{.2012}$	$\frac{603}{100.375}$	$\frac{199}{99.5}$	$\frac{-1309}{-1545}$
Average						$\frac{560.375}{559.5}$		

$\circ R = (^\circ F + 460)$

$P_s = BP + (-Pg/13.6) = \frac{28.75}{13.6} + \frac{(-15.15)}{13.6} = \frac{26.164}{13.6}$  "Hg

LEAK CHECKS:

Pre Test: Pg Leg: OK GAP

Post Test: Pg Leg: OK GAP

Velocity Head Leg: OK GAP

Velocity Head Leg: OK GAP

DILUTION TUNNEL GAS VELOCITY & VOLUMETRIC FLOW RATE CALCULATIONS

Rev 4/19/08

UNIT: KUMAR HSHWOOD DATE: 3/2/09 RUN #: EPA-7 TECHNICIAN(S): AMM BRP  
PPB

Average Gas Velocity in the Dilution Tunnel Vstrav (EPA M2 EQN 2-9, ASTM E 2515-07 EQN 7)

$$(9) V_{strav} = (85.49) (0.99 \text{ cp}) (1.1955) \times \sqrt{\Delta P \text{ "H}_2\text{O}} = 500.375 \text{ Ts } ^\circ\text{A} \text{ (10)}$$

$$= 13.81053 \text{ fps}$$

$$(2) (2) (20.164 \text{ Ps "Hg}) (28.56 \text{ lb./ lb. mole}) \text{ (2)}$$

$$(9A) V_s = (13.81053 \text{ fps}) (60) = 828.632 \text{ fpm (2)}$$

Gas Velocity in the Center of the Dilution Tunnel - Vscnt (EPA M2 EQN 2-9, ASTM E 2515-07 EQN 7)

$$(9) V_{scnt} = (85.49) (0.99 \text{ cp}) (1.2013) \times \sqrt{\Delta P \text{ "H}_2\text{O}} = 559.5 \text{ Ts } ^\circ\text{A} \text{ (10)}$$

$$= 14.20915 \text{ fps}$$

$$(2) (2) (20.164 \text{ Ps "Hg}) (28.56 \text{ lb./ lb. mole}) \text{ (2)}$$

$$(9A) V_s = (14.20915 \text{ fps}) (60) = 852.549 \text{ fpm (2)}$$

EPA M5G1 Section 4.2.2, ASTM E 2515-07 EQN 1 Adjustment Factor for Center of Tunnel Pitot Tube Location

$$F_p = V_{strav} / V_{scnt} = 13.81053 \div 14.20915 = .97195$$

Average Stack Gas Dry Volumetric Flow Rate - Qsd (EPA M2 EQN 2-10, ASTM E 2515-07 EQN 3)

$$(10) Q_{sd} = 3600 (1 - 0.04 \text{ Hws}) (13.81053 \text{ fps}) (1.1963 \text{ ft}^2) (528 \text{ } ^\circ\text{A}) (28.164 \text{ Ps "Hg}) / (560.375 \text{ Ts } ^\circ\text{A}) (29.92 \text{ " Hg}) = 8309.833 \text{ dscfhr (or dscfh) (2)}$$

$$(1) 8309.833 \text{ dscfhr (or dscfh)}$$

$$(10A) 8309.833 \text{ dscfhr} \div 60 = 138.497 \text{ dscfm (or dscfm) (1)}$$

Note: Number in ( ) under blank lines denotes number of decimals to be used. If a blank calls for an answer already calculated, use the number of decimals previously specified for that answer.

WOODSTOVE DATA SHEET #4-1: INITIAL FILTER WEIGHTS (TARE WEIGHTS)

Into Dessicator: Date 1-27-09 Time 1149 By PDG Front Half X Back Half X  
 Manufacturer: Pall P/N. 60115 Size: 110 Lot.No.: 70726 Grade: A/E Glass

Filter #	First Wt	2009 Date	Time	By	Second Wt	Date	Time	By	Third Wt	2009 Date	Time	By
700	.6873	1-22	1331	GRP	.6877	1-23	1417	PDG				
701	.6871		1330	GRP	.6878		1419	PDG	.6877	1-26	1421	GRP
702	.6816		1329	GRP	.6825		1420	PDG	.6824	1-26	1420	GRP
703	.6761		1328	GRP	.6762		1421	PDG				
704	.6727		1327	GRP	.6732		1422	PDG				
705	.6833		1326	GRP	.6837		1423	PDG				
706	.6946		1325	GRP	.6948		1424	PDG				
707	.6773		1324	GRP	.6777		1425	PDG				
708	.6701		1323	GRP	.6702		1426	PDG				
709	.6799		1322	GRP	.6809		1427	PDG	.6806	1-26	1419	GRP
710	.6587		1321	GRP	.6590		1428	PDG				
711	.6654		1320	GRP	.6656		1429	PDG				
712	.6678		1319	GRP	.6692		1430	PDG				
713	.6864		1318	GRP	.6866		1431	PDG				
714	.6651		1318	GRP	.6655		1432	PDG				
715	.6741		1317	GRP	.6744		1433	PDG				
716	.6692		1316	GRP	.6690		1434	PDG				
717	.6531		1315	GRP	.6536		1435	PDG				
718	.6721		1314	GRP	.6723		1436	PDG				
719	.6769		1313	GRP	.6769		1437	PDG				
720	.6627		1312	GRP	.6628		1438	PDG				
721	.6567		1311	GRP	.6569		1439	PDG				
722	.6539		1310	GRP	.65340		1440	PDG				
723	.6552		1309	GRP	.6552		1441	PDG				
724	.6655		1308	GRP	.66516		1442	PDG				

Checked by ATM Date: 1/27/09 Time 1632

QA REWEIGH

Filter #	WT	Date	Time	By
703	.6761	1/27/09	1639	ATM
708	.6705		1640	ATM
713	.6749	✓	1642	ATM

BALANCE ROOM ENVIRONMENTAL CONDITIONS

WB	DB	%RH	Date	Time	By
57	72	38	1-22-09	1138	ATM
58	25	33	1/24-09	1158	PDG
56	76	25	1-26-09	1359	GRP

Post 1-22 1423 1-26  
 0.0000 0.0000 0.0000  
 100.0000 99.9994 99.9993

58 72 31 1/27/09 1530 PDG



WOODSTOVE DATA SHEET #4-2:  
INITIAL BEAKER WEIGHTS (TARE WEIGHTS)

Into Dessicator: Date: 01.26.09 Time: 15:38 By: JRP

Beaker #	First Wt	2009 Date	Time	By	Second Wt	2009 Date	Time	By	Third Wt	Date	Time	By
20	73.3181	1/27	1532	PDG	73.3176	1-29	1459	JRP		1/30		
21	71.0021		1534	PDG	71.0018		1458	JRP				
22	71.8343		1535	PDG	71.8338		1457	JRP				
23	70.9390		1536	PDG	70.9389		1455	JRP				
27	72.3310		1538	PDG	72.3307		1500	JRP				
31	69.6672		1539	PDG	69.6669		1501	JRP				
32	53.6002		1541	PDG	53.5993		1502	JRP	53.5998		1505	PDG
37	53.7267		1542	PDG	53.7262		1504	JRP				
38	53.2525		1544	PDG	53.2516		1505	JRP	53.2520		1306	PDG
39	53.1509		1545	PDG	53.1493		1506	JRP	53.1496		1311	PDG
40	53.4626		1547	PDG	53.4620		1507	JRP				
41	52.8371		1549	PDG	52.8367		1508	JRP				
42	53.8699		1550	PDG	53.8692		1509	JRP	53.8696		1302	PDG

Checked By: [Signature] Date: 2/1/09 Time: 1810

QA REWEIGH

Beaker #	WT	Date	Time	By
20	73.3181	2/1/09	1215	ATM
31	69.6671		1717	ATM
42	53.8699	X	1219	ATM

BALANCE ROOM ENVIRONMENTAL CONDITIONS

WB	DB	%RH	2009 Date	Time	By
55	72	31	1/27	1530	PDG
58	77	29	1-29	1436	JRP
60	72	49	1/30	1256	PDG

1/27 0.0000 29.0001  
1-29 0.0000 29.0001  
1/30 0.0000 29.0001  
2/1 0.0000 29.0001

58 74 37 2/1 1200 ATM

WOODSTOVE DATA SHEET #4-2:  
INITIAL BEAKER WEIGHTS (TARE WEIGHTS)

Blank done 12/9/07

Into Dessicator: Date: 10/12/07 Time: 0801 By: GRP

Beaker #	First Wt	Date	Time	By	Second Wt	Date	Time	By	Third Wt	Date	Time	By
22	71.8343	10/22/07	1358	GRP	71.8332	11/10/07	1938		71.8330	11-11-07	1748	Jm
24	73.2192		1400	GRP	73.2190	11/10/07	1940		73.2193	11-11-07	1746	Jm
25	72.6516		1401	GRP	72.6512	11/10/07	1944		Blank			
26	71.7895		1403	GRP	71.7888	11/10/07	1939		71.7886	11-11-07	1747	Jm
27	72.3316		1402	GRP	72.3314	11/10/07	1945					
28	70.5979		1404	GRP	70.5975	11/10/07	1941		70.5977	11-11-07	1745	Jm
39	53.1508		1405	GRP	53.1500	11/10/07	1942					
37	53.7237	11/10/07	1945	GRP	53.7238	11/11/07	1743	Jm				

Checked By: \_\_\_\_\_ Date: \_\_\_\_\_ Time: \_\_\_\_\_

QA REWEIGH

Beaker #	WT	Date	Time	By
27	72.3315	11-11	1740	Jm
25	72.6515	11-11	1741	Jm
39	53.1509	11-11	1744	Jm

BALANCE ROOM ENVIRONMENTAL CONDITIONS

WB	DB	%RH	Date	Time	By
57	68	50	10/22/07	1344	GRP
			11/10		

Post weighing  
0.0000g  
0.0000g  
0.0000g

1st  
0.0000  
0.0000g

2nd





WOODSTOVE DATA SHEET 4-4 ANALYTICAL BALANCE QC RECORD SHEET  
 SCALE: SARTORIUS  
 MODEL: CP224S  
 SN: 17050374

FROM: 12/20/08  
 THROUGH: 2/17/09

Level	Recali	140 g	100 g	10 g	1.0 g	100 mg	20 mg	Weight	Weight	Date	Time	Tech	Wet Bulb	Dry Bulb	% RH
✓	N	139.9993	99.9995	9.9999	1.0000	0.1000	0.0199	12/20/08	1430	ADM	58	72	42		
✓	N	139.9995	99.9995	9.9999	1.0000	0.1000	0.0199	12/20/08	057	GRP	60	76	38		
✓	N	139.9994	99.9994	9.9999	1.0000	0.1000	0.0200	12/21/08	1019	ATM	59	72	43		
✓	N	139.9994	99.9994	9.9999	1.0000	0.1000	0.0200	12/21/08	1142	ATM	59	72	45		
✓	N	139.9994	99.9994	9.9999	1.0000	0.1000	0.0200	12/21/08	1050	ATM	60	75	34		
✓	N	139.9994	99.9994	10.0000	1.0000	0.1000	0.0199	12/21/08	1157	PDG	58	75	34		
✓	N	139.9994	99.9994	9.9999	1.0000	0.1000	0.0199	12/21/08	1045	ATM	60	75	37		
✓	N	139.9995	99.9996	9.9999	1.0000	0.1000	0.0199	12/21/08	1530	GRP	58	70	48		
✓	N	139.9994	99.9994	9.9999	1.0000	0.1000	0.0199	12/21/08	1356	PDG	60	72	49		
✓	Yes	139.9993	99.9994	9.9999	1.0000	0.1000	0.0200	12/21/08	1023	PDG	58	72	42		
✓	Yes	139.9993	99.9993	9.9999	1.0000	0.1000	0.0199	12/21/08	1128	JRP	55	72	31		
✓	NO	139.9994	99.9995	9.9999	1.0000	0.1000	0.0199	12/21/08	0845	PDG	59	75	38		
✓	NO	139.9993	99.9993	9.9999	1.0000	0.1000	0.0200	12/21/08	0825	JRP	58	74	37		
✓	Yes	139.9994	99.9994	9.9999	1.0000	0.1000	0.0199	12/21/08	1212	PDG	07	76	36		
✓	NO	139.9993	99.9993	9.9999	1.0000	0.1000	0.0199	12/21/08	1420	GRP	59	75	37		
✓	NO	139.9992	99.9993	10.0000	1.0000	0.1000	0.0199	12/21/08	1128	GRP	58	74	37		
✓	Yes	139.9994	99.9995	9.9999	1.0000	0.1000	0.0199	12/21/08	0950	PDG	58	74	37		
✓	NO	139.9993	99.9994	10.0000	1.0000	0.1000	0.0199	12/21/08	1230	PDG	56	71	37		
✓	NO	139.9993	99.9993	9.9999	1.0000	0.1000	0.0199	12/21/08	1613	JRP	57	73	35		
✓	NO	139.9994	99.9994	9.9999	1.0000	0.1000	0.0200	12/21/08	1130	ATM	57	72	38		
✓	NO	139.9993	99.9993	9.9999	1.0000	0.1000	0.0199	12/21/08	1150	PDG	58	75	33		
✓	YES	139.9992	99.9993	10.0000	1.0000	0.1000	0.0200	12/21/08	1359	JRP	06	76	35		
✓	NO	139.9994	99.9995	10.0000	1.0000	0.1000	0.0199	12/21/08	1530	PDG	58	72	41		
✓	NO	139.9993	99.9993	10.0000	1.0000	0.1000	0.0199	12/21/08	1452	ATM	61	75	41		
✓	YES	139.9993	99.9994	10.0000	1.0000	0.1000	0.0199	12/21/08	1430	GRP	58	77	29		
✓	NO	139.9995	99.9995	9.9999	1.0000	0.1000	0.0199	12/21/08	1256	PDG	60	72	49		
✓	NO	139.9993	99.9994	9.9999	1.0000	0.1000	0.0199	12/21/08	1200	ATM	58	74	37		
✓	NO	139.9993	99.9993	9.9999	1.0000	0.1000	0.0199	12/21/08	1350	GRP	58	77	29		
✓	Yes	139.9995	99.9996	9.9999	1.0000	0.1000	0.0199	2/15/09	1118	PDG	59	72	45		
✓	NO	139.9995	99.9995	9.9999	1.0000	0.1000	0.0199	2/16/09	1150	GRP	57	74	33		
✓	NO	139.9994	99.9994	10.0000	1.0000	0.1000	0.0200	2/17/09	1015	ATM	49	70	19		
✓	NO	139.9994	99.9994	9.9999	1.0000	0.1000	0.0199	2/16/09	1551	PDG	61	78	36		
✓	NO	139.9993	99.9994	9.9999	1.0000	0.1000	0.0200	2/17/09	1139	JRP	56	72	35		

WOODSTOVE DATA SHEET 4-4 SCALE QC RECORD SHEET

SCALE: SARTORIUS

MODEL: CP224S

SN: 17050374

FROM: 9/27/2007  
THROUGH: 12/7/2007

Level	Recali	130 g	100 g	10 g	1.0 g	100 mg	20 mg	Date	Time	Tech	Wet Bulb	Dry Bulb	% RH
✓	N	129.9998	99.9998	10.0000	1.0000	0.1000	0.0199	9/27/07	1402	9RP	55	67	45
✓	Y	129.9995	99.9996	10.0001	1.0000	0.1000	0.0200	9/28/07	1335	9RP	57	69	46
✓	Y	129.9996	99.9996	9.9999	1.0000	0.1000	0.0200	10/1/07	1505	ATM	58	70	48
✓	N	129.9995	99.9996	10.0000	1.0001	0.1000	0.0199	10/2/07	1611	9RP	56	68	46
✓	N	129.9997	99.9997	9.9999	1.0001	0.1000	0.0199	10/3/07	1122	9RP	56	68	46
✓	N	129.9996	99.9996	10.0000	1.0000	0.0999	0.0199	10/4/07	0905	9RP	55	67	45
✓	Y	129.9996	99.9996	10.0000	1.0000	0.1000	0.0199	10/5/07	0750	9RP	51	62	45
✓	N	129.9997	99.9997	9.9999	1.0000	0.1000	0.0199	10/5/07	1513	9RP	56	69	43
✓	Y	129.9996	99.9996	10.0000	1.0001	0.1001	0.0200	10/9/07	0905	ATM	58	71	44
✓	N	129.9996	99.9997	10.0000	1.0001	0.1001	0.0200	10/12/07	1259	ATM	58	70	48
✓	Y	129.9995	99.9996	9.9999	1.0000	0.1000	0.0199	10/22/07	1344	9RP	57	68	50
✓	Y	129.9996	99.9997	9.9999	1.0000	0.1000	0.0199	10/24/07	1338	9RP	53	63	50
✓	N	129.9995	99.9995	10.0000	1.0000	0.1000	0.0200	10/31/07	0933	ATM	56	70	40
✓	Y	129.9996	99.9997	10.0000	1.0000	0.1000	0.0199	10/30/07	1457	9RP	55	70	36
✓	Y	129.9996	99.9996	9.9999	1.0000	0.1000	0.0199	10/31/07	1528	9RP	57	75	30
✓	Y	129.9996	99.9996	9.9999	1.0000	0.0999	0.0199	11/2/07	1238	9RP	58	67	33
✓	Y	129.9996	99.9996	10.0000	1.0001	0.1000	0.0199	11/5/07	0730	9RP	57	73	36
✓	Y	129.9996	99.9997	10.0000	1.0000	0.1001	0.0201	11/9/07	1350	ATM	58	70	48
✓	Y	129.9997	99.9997	9.9999	1.0000	0.1000	0.0200	11/10/07	1835	ATM	58	71	44
✓	N	129.9997	99.9996	9.9999	1.0000	0.1000	0.0199	11/11/07	1810	ATM	55	69	39
✓	N	129.9996	99.9996	9.9999	1.0000	0.1000	0.0199	11/12/07	0822	9RP	54	67	41
✓	N	129.9996	99.9996	10.0000	1.0000	0.1000	0.0199	11/16/07	1224	ATM	58	72	41
✓	N	129.9998	99.9997	9.9999	0.9999	0.1000	0.0200	11/14/07	1710	9RP	58	73	39
✓	QC	Services Audit 11/14/07											
✓	Y	129.9997	99.9997	10.0000	1.0000	0.1000	0.0200	11/15/07	1350	ATM	59	72	45
✓	N	129.9996	99.9996	9.9999	0.9999	0.1000	0.0200	11/16/07	1600	9RP	58	71	44
✓	N	129.9996	99.9996	10.0000	1.0000	0.1000	0.0199	11/10/07	1758	ATM	60	74	43
✓	Y	129.9997	99.9997	10.0000	1.0001	0.1001	0.0200	11/19/07	1143	ATM	56	70	40
✓	Y	129.9995	99.9996	10.0000	1.0000	0.1000	0.0199	11/20/07	1416	9RP	54	69	35
✓	N	129.9996	99.9996	10.0000	1.0000	0.1000	0.0200	11/21/07	1110	ATM	57	70	44
✓	N	129.9995	99.9996	10.0000	1.0000	0.1000	0.0199	12/3/07	0730	9RP	55	69	40
✓	N	129.9996	99.9996	10.0000	1.0000	0.0999	0.0200	12/6/07	1125	ATM	54	67	44
✓	Y	129.9996	99.9996	10.0000	1.0000	0.1000	0.0200	12/7/07	1348	9RP	55	69	40

WOODSTOVE DATA SHEET 4-4 SCALE QC RECORD SHEET

SCALE: SARTORIUS  
 MODEL: CP224S  
 SN: 17050374

FROM: 12/2/07  
 THROUGH: 2/3/08

Level	Recali.	130 g	100 g	10 g	1.0 g	100 mg	20 mg	Date	Time	Tech	Wet Bulb	Dry Bulb	% RH
✓	N	129.9996	99.9996	10.0000	1.0000	0.1000	0.0200	12/8	12:15	ATM	57	73	35
✓	N	129.9996	99.9996	10.0000	1.0000	0.1001	0.0200	12/8	19:10	ATM	57	72	38
✓	N	129.9997	99.9996	10.0000	1.0000	0.1000	0.0199	12/9	19:35	ATM	55	72	31
✓	Y	129.9996	99.9996	10.0000	1.0000	0.1000	0.0200	12/10	19:53	ATM	56	72	34
✓	N	129.9997	99.9997	10.0000	1.0000	0.1000	0.0199	12/11	16:18	GRP	57	76	28
✓	N	129.9997	99.9996	10.0000	1.0000	0.0999	0.0199	12/12	15:05	GRP	56	74	30
✓	N	129.9996	99.9996	9.9999	0.9999	0.1000	0.0199	12/13	13:07	GRP	55	73	29
✓	Y	129.9996	99.9996	9.9999	0.9999	0.1000	0.0199	12/14	13:21	GRP	57	75	31
✓	N	129.9998	99.9998	9.9999	1.0001	0.1000	0.0199	12/15	16:02	GRP	57	75	31
✓	Y	129.9996	99.9997	9.9999	1.0000	0.1000	0.0199	12/17	08:17	GRP	55	73	29
✓	N	129.9997	99.9997	10.0000	1.0000	0.1000	0.0199	12/18	08:53	GRP	58	75	34
✓	N	129.9997	99.9997	10.0000	1.0000	0.1000	0.0199	12/19	08:12	GRP	55	72	31
✓	Y	129.9997	99.9997	10.0000	1.0001	0.0999	0.0199	12/20	09:16	GRP	57	71	41
✓	Y	129.9998	99.9997	10.0000	1.0000	0.1000	0.0199	12/21	10:35	ATM	55	70	36
✓	N	129.9997	99.9996	10.0000	1.0000	0.1000	0.0200	12/22	14:34	ATM	54	66	44
✓	N	129.9996	99.9996	10.0000	1.0000	0.1000	0.0200	12/23	09:15	ATM	57	76	44
✓	N	129.9996	99.9996	9.9999	1.0000	0.1000	0.0199	12/26	12:30	ATM	57	70	47
✓	N	129.9997	99.9997	10.0000	1.0000	0.1000	0.0200	12/27	10:30	ATM	56	72	34
✓	N	129.9998	99.9997	9.9999	1.0000	0.1000	0.0200	1/8/08	13:42	GRP	54	68	38
✓	N	129.9997	99.9997	10.0000	1.0001	0.1000	0.0200	1/9/08	07:42	GRP	55	70	36
✓	N	129.9998	99.9998	10.0000	1.0000	0.1000	0.0199	1/11/08	10:40	ATM	59	73	42
✓	Y	129.9996	99.9997	10.0000	1.0000	0.1000	0.0199	1/16/08	12:21	GRP	51	72	18
✓	N	129.9999	99.9998	10.0000	1.0000	0.1000	0.0199	1/17/08	12:37	GRP	56	71	37
✓	N	129.9998	99.9998	10.0000	1.0000	0.0999	0.0200	1/18/08	11:16	GRP	56	71	37
✓	Y	129.9995	99.9996	9.9999	1.0001	0.1000	0.0199	1/21/08	14:26	GRP	56	72	34
✓	N	129.9996	99.9996	10.0000	1.0001	0.1000	0.0199	1/22/08	15:13	GRP	56	71	37
✓	Y	129.9996	99.9996	9.9999	1.0000	0.1000	0.0199	1/23/08	08:05	GRP	54	69	36
✓	Y	129.9996	99.9996	10.0000	1.0000	0.1000	0.0200	1/24/08	07:58	GRP	54	70	33
✓	N	129.9998	99.9997	10.0000	1.0000	0.1000	0.0199	1/24/08	14:50	GRP	56	71	37
✓	N	129.9997	99.9996	10.0000	1.0000	0.1000	0.0200	1/31/08	15:05	GRP	55	69	38
✓	N	129.9996	99.9996	10.0000	1.0000	0.1000	0.0199	2/11/08	10:29	GRP	54	69	36
✓	N	129.9996	99.9996	9.9999	1.0000	0.1000	0.0199	2/20/08	16:20	ATM	56	72	41
✓	N	139.9996	99.9997	10.0000	1.0000	0.1000	0.0200	2/23/08	17:10	ATM	57	70	44

WOODSTOVE DATA SHEET 4-4 ANALYTICAL BALANCE QC RECORD SHEET

SCALE: SARTORIUS

MODEL: CP224S

SN: 17050374

FROM: 2/10/09

THROUGH:

Level	Recall	140 g	100 g	10 g	1.0 g	100 mg	20 mg	Date	Time	Tech	Wet Bulb	Dry Bulb	% RH
Yes	Y	139.9993	99.9994	9.9999	1.0000	0.1000	0.0199	2/10/09	1800	ATM	55	70	36
Yes	Y	139.9993	99.9994	9.9999	1.0000	0.1000	0.0199	2/10/09	1848	PRP	56	73	32
Yes	Y	139.9993	99.9994	9.9999	0.9999	0.1000	0.0199	2/20/09	1018	PD6	57	74	33
Yes	Y	139.9993	99.9994	10.0000	1.0000	0.1000	0.0200	2/21/09	1519	ATM	60	77	35
Yes	Y	139.9993	99.9994	9.9999	1.0000	0.1000	0.0199	2/22/09	1222	ATM	47	59	37
Yes	Y	139.9994	99.9994	9.9999	0.9999	0.1000	0.0199	2/23/09	1406	PD7	58	70	48
Yes	No	139.9994	99.9994	9.9999	1.0000	0.1000	0.0200	2/24/09	0953	ATM	59	76	35
Yes	Yes	139.9995	99.9995	9.9999	1.0000	0.1000	0.0199	2/25/09	1023	PD9	60	76	38
Yes	Yes	139.9994	99.9994	9.9999	1.0000	0.1000	0.0199	2-26/09	1258	JRP	55	70	36
Yes	Yes	139.9993	99.9993	9.9999	1.0000	0.1000	0.0200	2/29/09	1320	ATM	57	74	33
Yes	Yes	139.9995	99.9995	9.9999	0.9999	0.1000	0.0199	3/3/09	1431	PD6	59	76	35
Yes	NO	139.9993	99.9995	9.9999	1.0000	0.1000	0.0199	3/4/09	1556	PRP	56	72	40
Yes	NO	139.9994	99.9994	9.9999	1.0000	0.1000	0.0200	3/5/09	1350	ATM	60	75	40
Yes	NO	139.9993	99.9993	9.9999	1.0000	0.1000	0.0200	3/7/09	0850	ATM	57	71	41
Yes	Yes	139.9993	99.9993	10.0000	1.0000	0.1000	0.0200	3/8/09	1323	ATM	55	70	36
Yes	Yes	139.9993	99.9993	9.9999	1.0000	0.1000	0.0199	3/10/09	1212	PD9	58	75	40



Woodstove Particulate  
Catch Processing Sheet  
Woodstove Data Sheet #5  
EPA M5G-1

Unit: Kama Ashwood  
Run: EPA 7  
Date: 3/2/09  
Technicians: ATM JRP PDC  
Revised 1/16/98-Data Sheet #5

Filters

Filter # (Front) 718 Beaker # 27  
Final Wt. .6971 g ~~MI~~ 55 ml  
Tare Wt. .6723 g Desc. Acetone  
Net Wt. .0248 g

Final Wt. 72.3415 g  
Tare Wt. 72.3307 g  
Net Wt. .0108 g

Filter # (Rear) 717 Beaker # \_\_\_\_\_  
Final Wt. .6470 g ~~MI~~  
Tare Wt. .6536 g Desc. \_\_\_\_\_  
Net Wt. -.0066 g

Final Wt. \_\_\_\_\_ g  
Tare Wt. \_\_\_\_\_ g  
Net Wt. \_\_\_\_\_ g

Acetone Blank Calculation:

Blank Date: 12/8/07

Blank Beaker # 25 Final Wt. 72.6511 g  
MI 50 Tare Wt. 72.6512 g  
Desc. Acetone Net Wt. -0.0001 g = 0.0000  
1.0000 g + 50 ml = 1.0000 g/ml

Blank Residue Value Calculation:

1.0000 g/ml acetone X 55 ml acetone = 1.0000 g  
Blank Residue Value

Total Particulate Catch Calculation

Filter: .0248 g  
Filter: -.0066 g  
Beakers: .0108 g -- 1.0000 g = .0108 g  
Total Catch Blank Residue Value  
Total Catch = .0290 g

Unit Kuma Ashwood  
 Run # EPA  
 Date 3/20/9  
 Technician ANN JRP PDE  
 WST6-Form1, Rev8/96

MISCELLANEOUS TEST DATA  
 WOODSTOVE DATA SHEET #8

Useable Firebox Dimensions: See QC Section Useable Volume: 2.094 ft<sup>3</sup>

Dilution Tunnel Draft (If applicable): Start .000 Stop .000

Test Chamber Air Velocity: Start: 00.0 Stop: 00.0 Avg: 00.0

Wet Bulb/ Start: WB: 57 °F DB: 69 °F 1.15 % Amb Moisture 47 %RH

Dry Bulb Stop: WB: 60 °F DB: 75 °F 1.25 % Amb Moisture 40 %RH

$\bar{X} = 1.20$  % Ambient Moisture  $\bar{X} = 43.5$  % Relative Humidity (RH)

Empty Stove Wt: 440.2 lbs.

Stove Wt with Stack (Inc. Oil Seal) Wet: 765.5 lbs. Dry: 765.6 lbs.

Empty Stove Wt with Stack and Ash Ash: --- lbs. Total: --- lbs.

Kindling Wt. Total 5.1 Paper: .3 lbs. Wood: 4.8 lbs.

Pre Burn Fuel Wt. 11.994 + 12.942 + 10.690 Total: 35.626 lbs.

Total Kindling and Pre Burn Fuel Wt 40.726 lbs.

Coal Bed Wt-lbs: Range (3.3 - 2.7) 766.9 - 766.3 lbs. Actual 2.9 lbs.

Allowable Amount of Charcoal that can be removed:

Coal Bed Wt. Range 3.3 + 2.7 / 2 x .25 = 0.70 lbs.

Test Fuel Wt-lbs: Ideal 14.7 lbs. Range: 16.1 - 13.2 lbs. Actual: 13.330 lbs.

Test Fuel Size (pcs.) (.75 x 1.5 x 5" Flanges) 1.348 lbs. 16 Pcs.

2 x 4's x 16.4375 " 3 Pcs 6.584 lbs. 49.39 %

4 x 4's x 16.4375 " 2 Pcs 6.746 lbs. 50.61 %

5.0283 kg

Est. Dry Burn Rate (Kg/Hr.)  $\frac{13.330 - (13.330 \times .16838)}{2.2046} \times \frac{60}{295} = \frac{1.0586}{1}$  Est. Dry Burn Rate (Kg/Hr)

Est EPA Heat Output (HO<sub>E</sub>) (19,140) x  $\frac{68}{100}$  x 1.0586 = 12,765 Est Heat Output (HO<sub>E</sub>) BTU's/Hr

Comments:

Stove Operating Data  
Woodstove Test Data Sheet #9  
Cold Start

Unit: Kuma Ashwood  
Run: EPA 7  
Date: 3/2/09  
Technician(s): ATM JRP ADG  
Data Sheet#9-Rev 1/98-Pg.2

Fire Started: 10:15

Warm up and Preburn: Primary Air: Wide open from ignition until the start of preburn when the primary air control(s) was (were) adjusted to the run setting of 2.475 on thr. rot. At the run setting until the start of the test.  
.467 PAC

Secondary Air: No Controls. Naturally drafted

Secondary Burn Bypass: N/A

Charcoal Bed Preparation: Broke up, raked and leveled the coal bed prior to the addition of each warm up/pre burn fuel charge. Starting 1130 before the start of the test, broke up, raked and leveled the coal bed. In stove for 30 seconds.

Test: Door wide open during loading 1 min 1 sec, then closed.

Primary Air: Wide open from the start of the test (0:00) until 4:45. Adjusted to the run setting of 0.467" between 4:45 and 5:00. At the run setting of 0.467" at 5:00 into the run.

Secondary Air: No Controls. Naturally drafted.

Secondary Burn Bypass: N/A

Fan: ON/OFF during the warm up, ON/OFF Low during the preburn, ON/OFF at the start of test, ON/OFF for the first 30 minutes of test, ON/OFF low at 30 minutes into test, ON/OFF for the rest of test.

Test Run Anomalies: Another good start & Run

WOODSTOVE OPERATING DATA  
 WOODSTOVE DATA SHEET #9A-1

Wood Data: Kindling: A mix of the below grades

	Size	Mill	Grade	Species
Pre Burn	2X4	Forest Grove	# 2 $\frac{1}{2}$ BTR	D. Fir S.E. Gen
Test Fuel	2X4	Forest Grove	# 2 $\frac{1}{2}$ BTR	D. Fir S.E. Gen
	4X4	"	# 1	"

All grades WCLB Rules unless otherwise noted.

Warm up Information:

1st Warm up/Pre Burn Fuel charge (11.994 lbs) added at 10:29.  
 2nd Warm up/Pre Burn Fuel charge (12.942 lbs) added at 11:21.  
 3rd Warm up/Pre Burn Fuel charge (10.690 lbs) added at 12:18.  
 4th Warm up/Pre Burn Fuel charge (\_\_\_\_\_ lbs) added at \_\_\_\_\_.  
 5th Warm up/Pre Burn Fuel charge (\_\_\_\_\_ lbs) added at \_\_\_\_\_.  
 6th Warm up/Pre Burn Fuel charge (\_\_\_\_\_ lbs) added at \_\_\_\_\_.  
 7th Warm up/Pre Burn Fuel charge (\_\_\_\_\_ lbs) added at \_\_\_\_\_.  
 8th Warm up/Pre Burn Fuel charge (\_\_\_\_\_ lbs) added at \_\_\_\_\_.

1<sup>st</sup> Rick 4-12", 4-16" 2x4's      3<sup>rd</sup> Rick 4-12", 3-16" 2x4's  
 2<sup>nd</sup> Rick 8-16" 2x4's

The coals were scooped out of the stove immediately prior to adding the 3<sup>rd</sup> pre burn/warm up fuel charge. The stove lost 00 lbs. 20 lbs. of coals were put back in the stove after the scoop.

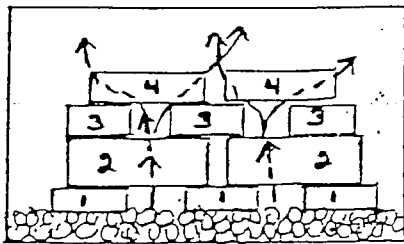
All pre burn/warm up fuel pieces were either 12 or 16 inches long. All preburn pieces/fuel charges were "ricked" in the stove. The pieces in the bottom layer in each rick contained 2 pcs that were 12x16 inches long and were loaded flat and perpendicular to the door. The pieces in the second layer in each rick were loaded on their side (edge) approximately parallel to the door and contained 3<sup>rd</sup> pcs 16 inches long. The third layer (and fourth layer if present) was loaded flat, perpendicular to the door and contained 2 pcs 12x16 inches long. The majority of the pieces in each rick were in the second layer which had an approximate 0.5-1.0" space between pieces. (The loading directions indicate the direction of the longest dimension on each piece relative to the loading door opening.) Each pre burn/warm up fuel charge normally weighs within the weight range allowed for the actual test fuel charge.

WOODSTOVE OPERATING DATA  
WOODSTOVE DATA SHEET #9A-2

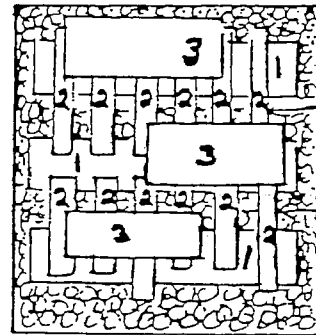
Unit: Kuma Ashwood  
Run # EPA 7  
Date 7/2/09  
Technician ATM JRP PGG  
Page 2 of 4  
WST7-Form2-A, Rev 6/90

Warm up Information (cont.):

Each warm up/preburn fuel charge was ricked in exactly (as much as possible) the same manner and the weight of each rick was usually within the allowable weight range for the test fuel charge. The physical arrangement and alignment of each rick was designed to accomplish three (3) things: (1) The bottom layer was nestled firmly into the coal bed and was as close to being level with the bottom of the stove as possible, thus providing a stable loading platform for the rest of the rick, keeping it in a ricked state (as opposed to a col-lapsed or fallen down state) until the rick reached the charcoal stage and sags or collapses of its own accord. (2) It enhances the flow of primary air through the ricked preburn fuel charge, for the primary air would flow through the spaces between the pieces in the first layer and then up through the spaces between the pieces in the second, third and, if present, fourth layers. (3) It maximized, as much as possible, the surface to volume ratio of each preburn fuel charge, thereby allowing the fire immediate access to as much wood surface as possible and, thereby, insuring uniform charcoalization. All three of these enhance combustion and so get the stove as hot as possible during the warm up period, thereby maximizing the amount of heat (BTU's) stored in the stove. The actual preburn was not started until the stove surface temperatures had maximized and stabilized, thus indicating that the amount of heat stored in the stove had peaked. For this stove, the thermal storage was monitored using the Stove TOP T/C surface temperature(s) and the peak value(s) obtained were 1102 °F. 1102



Front View



Top View

The arrows indicate the direction of the air flow through the rick.

The primary air was adjusted to the run setting of 0.467" open 4.0 lbs above the upper charcoal bed weight.

Additional Comments:

② Adjusted Primary Air Control to Wide Open ③ opened door ④ loaded fuel ⑤ Cleared coals away from in front of the LPAO ⑥ closed door

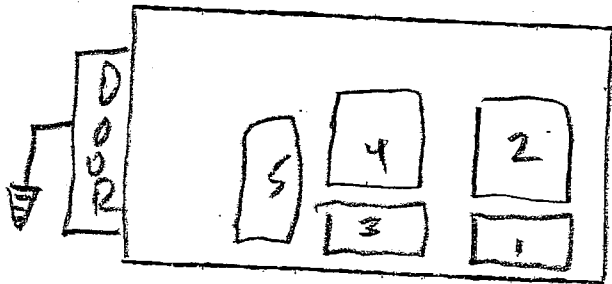
Test Start Sequence:

① Turned Fan OFF

Total Elapsed Time: 1101  
Photo @ 1:55

Test Fuel Charge Loading Information:

Test Fuel Charge and Loading Sequence Diagram



SIDE

of stove view

4 X 4's: 2 & 4

2 X 4's: 1, 3 & 5

Loading Sequence: 1, 2, 3, 4 & 5 LAST

Driest Pcs in Load 5, 3

Loaded the test fuel charge on an essentially level; Medium sized, Aug to hot coal bed (in appearance, color and temperature for a M.Low (1.0-1.25) burn rate. Load: 1:01 Ignition: 1101

1:01 Door Closed.

1:05 Vertical Column of Flame (VC) up to baffle.

1:55 Photo

2:36 Flames full width of front of pc 5.

3:10 Secondaries forward past the front tube.

4:45-5:00 Primary Air Control adjusted to the run setting  
5:00 Flames decreasing, Maintained a hot pocket of coals underneath and behind pc 5 with a small VC with Secondaries above 4.

6:00 Secondaries have decreased and are flashing on/off behind the VC.

6:44 7.5 / 1.21 (%CO<sub>2</sub> / %CO) M/MH, VC flicks to baffle.

WOODSTOVE OPERATING DATA  
WOODSTOVE DATA SHEET #9A-4

Additional Comments:

- 7:50 UC pulsing up and down, Secondary flashes above 4.  
9:10 Small pop  
9:25 No Secondaries M/MH  
10:08 Secondaries flashing on/off again.  
10:30 6.0/1.09 M/MH  
11:00 Steady secondaries above pc 4  
12:14 UC widening at base, especially to the L.  
15:43 7.2/1.14 M/MH  
16:03 Secondaries flashing to both L and R of center  
17:46 Secondaries to the L end of 4  
18:42 9.43/1.33 Secondaries flashing forward past  
front tube left of center.  
19:38 flames on the center top edge of pc 5 9.68/1.32  
20:28 Velocity in Secondaries - are lifting off the tubes.  
20:34 9.9/1.29  
21:02 Secondaries forward past the front tube 10.33/1.25  
M/MH  
23:08 BIG POP. All Flames out for ~ 3 Seconds.  
23:54 NO real UC - due to pop. Only secondaries - top  
down burn MH.  
25:28 10.91/1.19 M/MH  
25:52 Another big pop  
26:27 Gas Balance 10.8/1.08  
27:14 Real UC again  
28:00 UC out again. Secondaries really increasing.  
whole right side of dove glass is black.  
30:00 Fan On Low.

Unit: Kamm Ashwood  
 Run: EPA 7  
 Date: 3/2/09  
 Technician: AM JRP PUB

FUEL MOISTURE  
 WOODSTOVE TEST DATA SHEET #10

WST1-Form7-Rev11/89

5 kg = 11.024 lbs      1.0 kg = 2.204 lbs.

Room Temperature: 60.1 °F      Correction Factor: +1.0

NOTE: Record readings to the nearest 0.5% moisture  
 Uncor Values are corrected for temperature: Yes  No   
 Time Test Fuel Moisture Readings taken at: 11:15  
 Calibration Checks: X  Y  12.0 11.8 22.0 22.1

Pc #	Dimen	Use	Top		Bottom		Side		Piece Avg Corrected
			Uncor	Cor	Uncor	Cor	Uncor	Cor	
1	3 pcs	K	7.5	7.85	7.5	7.85	7.75	8.08	7.927
2									
3									
4	2x4-8'	P	19	20.3	18	19.2	18	19.2	19.567
5			18	19.2	18	19.2	18.5	19.8	19.400
6			19	20.3	19	20.3	19.5	20.9	20.500
7			20.5	22.0	20.5	20.0	22	23.7	22.567
8	↓	↓	20.5	20.0	20	21.4	20	21.4	21.600
9									103.634
10									
11	2x4-16 3/4	T	18	19.2	18	19.2	18	19.2	19.200
12			18.5	19.8	18	19.2	18	19.2	19.400
13			22	23.7	21	22.5	20.5	22.0	22.767
14									
15	4x4-16 3/4	T	20	21.4	18	19.2	18	19.2	19.933
16			19	20.3	19	20.3	18	19.2	19.933
17									101.233
18									
19	Spooks	T	19	20.3	18	19.2	18	19.2	19.567
20									OUT Spooks

1.02  
 1.666  
 2.536

2.880  
 3.548

1.348

Kindling	Pretest Fuel	Test Load
7.927%	20.7268%	20.2466%
7.345%	17.1684%	16.838%

% Moisture - Dry Basis:  
 4x4  
 % Moisture - Wet Basis:  
 13.330      6.746

To obtain Wet from Dry:  $\frac{100 \times \% \text{ Dry Rdg.}}{100 + \% \text{ Dry Rdg.}} = \% \text{ Moisture, Wet Basis}$   
 50.284 kg      1 11.994

Acceptable Ranges: 16-20% wet; 19-25% dry  
 (17.5 - 22.5 on Meter [Uncor reading] at 70°F)      2 12.942  
 3 10.690

Key for Use: K= Kindling    P= Pretest Fuel    T= Test Fuel  
 245 = 1.231



WOOD DENSITY DETERMINATION  
WOODSTOVE TEST DATA SHEET #11

Unit: KUMA ASHWOOD  
Run#: FPA 4  
Date: 3/2/09  
Technician: Ann JRP POG  
WST2-form11-Rev 6/90

Wood Piece: 2x4 Nominal Dimensions: 1.5 x 3.5 x 3.5"  
Depth (D): 3.820 cm  
Width (W): 8.860 cm  
Length (L): 8.915 cm  
8.925 cm  
8.975 cm  
9.025 cm  
Length  $\bar{X}$  = 8.960 cm  
Volume: 303.253 cm<sup>3</sup>  
(D X W X L)

MOISTURE: Room Temperature: 60.1 °F Correction Factor: +10

Uncorrected Meter Readings Corrected for temperature: Yes  No

NOTE: Record moisture meter readings to the nearest 0.5%

	Uncor	Cor
Top:	<u>18</u>	<u>19.2</u> %
Bottom:	<u>18</u>	<u>19.2</u> %
Side:	<u>18</u>	<u>19.2</u> %
$\bar{X}$ :		<u>19.2</u> %

Avg % Moisture (Dry) 19.200 %

Avg % Moisture (Wet) 16.102 %

Scale: Levelled In  Out

Zeroed: In  Out

Wet Weight: 159.2 g Dry Weight: 137.9 g

% Moisture Dried Basis: 13.379 %  
[1 - (Dry Wt ÷ Wet Wt)] X 100

	Date	Time	Temp
Into Dryer	<u>3/2/09</u>	<u>1640</u>	<u>192</u> °F
Out of Dryer	<u>4/3/09</u>	<u>1245</u>	<u>196</u> °F

(Minimum Time in Dryer: 24 hrs.) Minimum Dryer Temp 100°C (212°F)

Density = 137.9 g (dry wt) ÷ 303.253 cm<sup>3</sup> (volume) = 0.4546 g/cm<sup>3</sup>

Pellet Fuel Moisture Content Determination

Tare Beaker Wt. \_\_\_\_\_ g

Wet Wt: \_\_\_\_\_ g - \_\_\_\_\_ g = \_\_\_\_\_ g

Gross Wet Wt. Tare Beaker Wt. Net Wet Wt.

Dry Wt: \_\_\_\_\_ g - \_\_\_\_\_ g = \_\_\_\_\_ g

Gross Dry Wt. Tare Beaker Wt. Net Dry Wt.

% Moisture Dried Basis: \_\_\_\_\_ %  
[1 - (Net Dry Wt ÷ Net Wet Wt.)] X 100

Pre Burn ( )  
 4.0 lbs. wt. 772.9 lbs.  
 Test Sheet wt. Range 768.9 - 766.3 lbs.

PRE BURN DATA  
 RECORD SHEET #13  
 WST2-Form16

BAFOI PRESSURE 11.9  
 28.17

Unit: Kuma Ashwood  
 Run: GPA 7  
 Page: 1 of 1

Date: 3/2/09  
 Technician(s): Atm JEP PDG

Minute	Scale Weight	Burn Rate	Stack	Stove Top	Left Side	Back	Right Side	Bottom	Firebox	2nd Burn Catalytic	Room Temp	Static	RAKE FWD Comments
0	772.9	0	685	1001	586	285	576	344	1019	1363	81	-2074	Primary Air Set at 2.445 ✓
5	772.7	0.7	499	956	600	398	587	356	993	1356	80	-2066	Secondary Air Set at Fixed Fan: 4.50 COPD ✓
10	771.5	1.7	454	696	603	405	592	303	986	1369	80	-2064	TUNNEL ON AT: 1814 ✓
15	770.9	1.6	436	697	604	406	589	367	991	1390	79	-2063	Buckets Filled ✓
20	770.5	1.4	407	647	606	407	587	368	994	1400	78	-2059	ANALYZERS SPANNED ✓
25	770.0	1.5	387	612	611	411	591	368	995	1400	79	-2057	Pumps turned on at: 1343 ✓
30	769.7	1.3	365	777	620	418	591	366	1006	1359	80	-2053	510.0 AT 11.1 ✓
35	769.5	1.2	332	715	617	426	586	354	1000	1304	79	-2050	529.0 - 11.0 ✓
40	769.3	1.2	313	663	606	436	577	363	965	1271	79	-2048	Check WB/DB: 516.6 - 12.4 ✓
45	769.1	1.2	297	621	593	440	566	363	975	1201	79	-2045	503.2 - 13.4 ✓
50	769.0	1.1	263	584	579	437	554	362	949	1096	78	-2043	488.0 - 15.2 ✓
55	768.9	1.1	262	517	561	430	540	362	696	1146	78	-2043	Probe IN TUNNEL
60	768.8	1.1	269	556	540	416	523	362	627	1007	77	-2040	TUNNEL AP 474.2 - 13.4 ✓
65	768.7	1.1	260	507	520	406	505	362	567	946	76	-2039	410.0 - 14.1 ✓
70	768.6	1.1	255	497	503	399	490	361	597	916	76	-2036	449.0 - 12.0 ✓
75	768.5	1.1	251	490	487	390	477	360	587	905	76	-2036	436.0 - 11.1 ✓
80													
85													
90													

RAKE FWD @ 3010.0 or 11.1

Sheet 435 - 440 ° F





Myren Consulting Inc Data Sheet P3 of 5 Unit KUMMA ASHWOOD Date 3/2/09 Run 9A7  
 Test Env 706.5 AT 436.8 Barometric Pressure 26.15 hg Gas Flows @ 1.5" Technician(s) ATM JRP

Time E/T min	Scale Wt.	Lbs. Left	Burn Rate	CO <sub>2</sub> %	CO <sub>2</sub> v.	CO <sub>2</sub> %	O <sub>2</sub> v.	O <sub>2</sub> %	CO v.	CO %	Gas Bal	Opacity & Notes	Wet B		Calc Wet B	Dry B		Snack Temp #3	Static Press	
													#1	#2		#1	#2			
155	771.1	2.6	12	1402	999			10.53	1076	176	13.1	Clear						286	-043	
160	771.0	2.5	11	1349	816.6			11.79	1007	187	10.0	"						291	-040	
185	770.9	2.4	11	1325	810.9			12.29	1105	105	9.7	"						264	-039	
190	770.8	2.3	11	1320	796			12.33	1121	121	6.6	"						256	-038	
195	770.7	2.2	11	1310	772			12.47	1143	143	5.4							248	-037	
200	770.6	2.1	11	1312	776			12.39	1150	150	5.2							244	-036	
205	770.5	2.0	11	1306	762			12.54	1148	148	5.1							240	-035	
210	770.4	1.9	11	1310	772			12.37	1162	162	4.8	"						236	-034	
215	770.3	1.8	11	1306	762			12.43	1171	171	4.5							233	-033	
220	770.2	1.7	11	1304	757			12.39	1169	169	4.0							230	-033	
225	770.1	1.6	11	1297	739			12.53	1195	195	3.8							226	-032	
230	770.1	1.6	0	1292	727			12.63	1200	200	3.6							223	-031	
Tot																				

(2959) 6.931

Time E/T	Top #4	Left #5	Back #6	Right #7	Bottom #8	Firebox #9	2 <sup>nd</sup> burn #10	Amb. #11	Tnd. #12	C Gas H Box #13	C Gas Imper #14	Part. Fill #15	Part. Cond. #16	Cent. 2nd #17	Tube 1 #18	Tube 2 #19	Tube 3 #20	
																		155
160	570	525	380	4910	296	845	1073	76	92	221	36	60	37	1223				
185	575	516	361	490	296	834	1022	76	92	221	36	60	37	1133				
190	579	506	364	483	296	816	976	76	91	221	36	60	37	1096				
195	499	497	368	475	296	801	943	76	91	221	36	60	37	1054				
200	482	490	367	469	295	791	920	76	91	220	37	60	37	1051				
205	469	484	369	463	295	781	914	76	91	219	37	60	37	1050		420.0	-16.8	
210	455	476	391	456	296	767	909	76	91	217	37	60	37	1041		415.2	-21.6	
215	445	474	392	451	295	756	894	76	91	216	37	60	37	1022				
220	436	469	389	446	295	746	879	76	91	216	37	60	37	1010		407.0	-29.8	
225	426	466	389	442	295	740	869	77	91	219	37	60	37	1004				
230	421	462	390	438	295	731	858	77	91	220	37	61	37	996		401.2	-35.6	
Tot																		

(587) 590.463.5610 3575.9477 (11432) 915

Myren C Julging Inc Data Sheet P4 of 5 Unit Kuma Ats Date 3 / 2 / 09 Run 0A7  
 Test End 7:08.5  $\Delta T$  636.6 Barometric Pressure 28.14 Technician(s) Am JRP

Time E/T min	Scale Wt.	Lbs. Left	Burn Rate	CO <sub>2</sub> v.	CO <sub>2</sub> %	O <sub>2</sub> v.	O <sub>2</sub> %	CO v.	CO %	Gas Bal	Opacity & Notes	Calc Wet B	Wet B #1	Dry B #2	Stack Temp #3	Stack Static Press
180	770.10	1.5	1	287	715		12.71	2.09	2.09	3.4					220	-0.31
185	769.9	1.4	1	282	702		12.62	2.12	2.12	3.3					218	-0.30
190	769.8	1.3	1	282	702		12.69	2.16	2.16	3.2					212	-0.30
195	769.7	1.2	1	274	683		13.08	1.99	1.99	3.4					215	-0.30
200	769.7	1.2	0	261	650		13.34	2.12	2.12	3.1					213	-0.29
205	769.6	1.1	1	263	655		13.24	2.22	2.22	3.0					211	-0.29
210	769.5	1.0	1	256	638		13.39	2.25	2.25	2.8					211	-0.28
215	769.4	1.9	1	260	648		13.31	2.23	2.23	2.9					209	-0.28
220	769.4	1.9	0	262	653		13.24	2.26	2.26	2.9					208	-0.26
225	769.3	1.8	1	255	636		13.38	2.32	2.32	2.7					206	-0.26
230	769.2	1.7	1	246	613		13.53	2.47	2.47	2.5					206	-0.26
235	769.1	1.6	1	237	591		13.79	2.39	2.39	2.5					204	-0.27
Tot																

2533.346

Time E/T	Top #4	Left #5	Back #6	Right #7	Bottom #8	Firebox #9	2 <sup>nd</sup> burn #10	Amb. #11	Tnl. #12	C Gas. H.Box #13	C Gas Impgr #14	Part. Filt. #15	Part. Cond. #16	Cent. 2nd #17	Tube 1 #18	Tube 2 #19	Tube 3 #20
180	413	456	389	433	294	720	636	76	91	220	36	61	37	922			
185	407	453	391	430	294	712	629	77	91	222	37	61	37	922		395.0	-41.8
190	399	447	389	425	292	704	615	76	90	220	36	61	36	921			
195	396	446	386	422	292	719	620	77	91	216	36	61	37	637		388.4	-46.4
200	392	443	382	420	293	711	611	77	91	216	37	62	37	658			
205	386	439	378	417	293	703	605	77	91	216	37	62	37	650		383.0	-53.8
210	384	435	371	414	282	693	601	77	91	216	37	62	37	644			
215	381	430	366	411	290	685	595	77	91	217	37	62	37	641		375.6	-61.2
220	378	427	364	409	290	691	586	77	91	218	37	63	37	627			
225	375	423	364	406	289	685	574	77	91	219	37	62	37	615		371.4	-65.4
230	372	420	363	404	288	676	563	78	91	219	37	63	37	603			
235	366	416	362	401	286	666	554	78	91	219	37	63	37	592		367.0	-69.8
Tot																	

4653.92351505 9998.3495 8378 9589 921

Myren ( ) ulting Inc Data Sheet P5 of 5 Unit Kuma As Date 3 / 2 / 09 Run PA 7  
 Test End wt 7665 AT 436.8 Barometric Pressure 20.12 "hg Gas Flows @ 1.5" Technician(s) APW JRP 206

Time E/T min	Scale Wt.	Lbs. Left	Burn Rate	CO <sub>2</sub> v.	CO <sub>2</sub> %	O <sub>2</sub> v.	O <sub>2</sub> %	CO v.	CO %	Gas Bal	Opacity & Notes	Calc Wet B	Wet B #1	Dry B #2	Stack	
															Temp #3	Static Press
240	769.1	16	0	0.227	5.66		13.99	0.249	2.49	2.3					203	-0.27
245	769.0	15	1	0.220	5.49		14.10	0.262	2.62	2.1					201	-0.27
250	768.9	14	1	0.213	5.32		14.25	0.266	2.66	2.0					200	-0.27
255	768.9	14	0	0.211	5.27		14.30	0.267	2.67	2.0					196	-0.26
260	768.8	13	1	0.207	5.17		14.43	0.260	2.60	2.0					196	-0.26
265	768.7	12	1	0.206	5.15		14.47	0.257	2.57	2.0					197	-0.26
270	768.7	12	0	0.202	5.05		14.59	0.252	2.52	2.0					196	-0.26
275	768.6	11	1	0.205	5.12		14.49	0.258	2.58	2.0					196	-0.25
280	768.6	11	0	0.205	5.12		14.50	0.255	2.55	2.0					195	-0.25
285	768.5	0	1	0.200	5.00		14.64	0.252	2.52	2.0					192	-0.25
290																
295																
Tot																

ATG  
 Total  
 197.6  
 1533.2  
 2691.038

Time E/T min	Top #4	Left #5	Back #6	Right #7	Bottom #8	Firebox #9	2 <sup>nd</sup> burn #10	Amb. #11	Tnl. #12	C Gas H Box #13	C Gas Imgr #14	Part. Filt. #15	Part. Cond. #16	Cent 2nd #17	Tube 1 #18	Tube 2 #19	Tube 3 #20	
																		240
245	362	408	352	396	286	660	749	76	91	219	37	62	37	772				
250	358	403	347	394	285	653	735	76	90	219	37	62	37	758		361.2	-75.6	
255	354	398	344	392	283	641	726	77	90	216	37	62	37	750		354.2	-82.6	
260	352	394	340	391	283	635	721	77	90	219	37	62	37	745				
265	349	390	335	389	282	629	714	77	90	220	37	62	37	738		349.0	-87.8	
270	347	386	328	388	281	624	706	77	90	220	37	62	38	731		346.0	-90.8	
275	344	381	323	386	279	617	701	77	90	221	38	62	38	725		342.6	-94.2	
280	342	376	319	385	276	605	700	77	89	221	38	62	38	721		340.4	-96.4	
285	338	373	313	382	275	596	693	76	86	219	37	61	37	711		336.2	-100.6	
290	351	393	335	390	281	632	720	77	90					AT				
295	358	402	347	397	285	644	741	77	90	Total				Start	436.8			
Tot	493	542	347	444	301	741	1013	77	AVG	558				End	336.2		0.07	-100.6

269.6  
 214.4

PRE AND POST TEST ZERO/SPAN CHECK  
WOODSTOVE DATA SHEET #15-1

Site: Myren Consulting, Woodinville, WA <sup>colville</sup> Date: 3/2/09 Analyter: CO2

Source: Kuma Ashwood Run #: EPA7

Zero Cyl #: TC 3AAM154 Conc. 00.0 % CO<sub>2</sub> Cyl Press: 1500 psi

Certified by: Oxarc Date: 11/12/07

Span Cyl #: AS90457 Conc. 12.5 % CO<sub>2</sub> Cyl Press: 1440 psi

Certified by: Matheson Tri Gas Date: 2/2/09

Analyzer: Make: Horiba Model: FIR-2000 SN: 607024

Range: 0 - 25.0% CO<sub>2</sub> Analyzer Output: 0 - 1.0 v.

Flow: 1.5 SCFH Measured by: Rotameter;  Flowmeter:

EPA Span Value = 25.0% CO<sub>2</sub>  
EPA Control Limits = + 2.5% of 25.0% CO<sub>2</sub> = + 0.625% CO<sub>2</sub>

Pre Run Audit: By: A. Myren Time: 1247 Temp: 79 °F

Audit Results

Point #	Expected Response			Actual Response			+ Conc. Difference	Δ %
	Meter	DVM	%	Meter	DVM	%		
Zero	00.0	.000	00.0	00.0	.000	0.05453	+0.05453	+0.22
Span	50.0	1.500	12.50	50.0	.500	12.4105	-0.0895	-0.72

Comments:

Post Run Audit: By: A. Myren Time: 1912 Temp: 75 °F

Audit Results

Point #	Expected Response			Actual Response			+ Conc. Difference	Δ %
	Meter	DVM	%	Meter	DVM	%		
Zero	00.0	.000	00.0	00.0	.001	0.0792	+0.0792	+0.32
Span	50.0	1.500	12.50	49.5	1.499	12.3858	-0.1142	-0.91

Comments:

+ Conc. Difference = Act % - Exp (Std) %  
 Zero % Difference =  $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Full Scale Value}} \times 100$   
 Span % Difference =  $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Exp \% (ppm)}} \times 100$



PRE AND POST TEST ZERO/SPAN CHECK  
WOODSTOVE DATA SHEET #15-3

Colville

Site: Myren Consulting, Woodinville, WA Date: 3/2/09 Analyte: CO

Source: Kuma Ashwood Run #: EPA 7

Zero Cyl #: FC 3AAM154 Conc. 00.0 % CO Cyl Press: 1500 psi

Certified by: Oxarc Date: 11/12/07

Span Cyl #: AS 90457 Conc. 2.0 % CO Cyl Press: 1440 psi

Certified by: Matheson Tri Gas Date: 2/2/09

Analyzer: Make: FlexiB Model: Mex A 3116S SN: GE 30075

Range: 0 - 10.0% CO Analyzer Output: 0 - 1.0 V

Flow: 1.5 SCFH Measured by: Rotameter:  Flowmeter:

EPA Span Value = 5.0% CO  
EPA Control Limits = +2.5% of 5.0% CO = + 0.125% CO

Pre Run Audit: By: A.T. Myren Time: 1247 Temp: 79 °F

Audit Results

Point #	Expected Response			Actual Response			+ Conc. Difference	Δ %
	Meter	DVM	%	Meter	DVM	%		
Zero	00.0	00.0	00.0	0.00	.000	-0.00443	-0.00443	-0.04
Span	2.00	.200	2.00	2.00	.200	2.0059	+0.00595	+0.30

Comments:

Post Run Audit: By: A.T. Myren Time: 1912 Temp.: 75 °F

Audit Results

Point #	Expected Response			Actual Response			+ Conc. Difference	Δ %
	Meter	DVM	%	Meter	DVM	%		
Zero	00.0	00.0	00.0	0.00	.001	.00563	+0.00563	+0.06
Span	2.00	.200	2.00	1.99	.198	1.9858	-0.01416	-0.71

Comments:

+ Conc. Difference = Act % - Exp (Std) %  
 Zero % Difference =  $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Full Scale Value}} \times 100$   
 Span % Difference =  $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Exp \% (ppm)}} \times 100$

Unit: Kuma Ashwood  
 Run: EPA 7  
 Date: 3/2/09  
 Technicians: AM JEP PDG  
 WST6-Form3-Rev11/89

QUALITY CHECKS  
 WOODSTOVE DATA SHEET #16

Ambient = Tr: \_\_\_\_\_ °F T/C#30: \_\_\_\_\_ °F  
 Thermocouple Check (at ambient): T/C#1: — °F; T/C#2: 65.6 °F;  
 T/C #3: 62.9 °F; T/C #4: 61.5 °F; T/C #5: 61.8 °F;  
 T/C #6: 61.7 °F; T/C #7: 61.3 °F; T/C #8: 61.9 °F;  
 T/C #9: 62.2 °F; T/C #10: 64.9 °F; T/C #11: 60.1 °F;  
 T/C #12: 62.7 °F; T/C #13: 63.3 °F; T/C #14: 58.4 °F;  
 T/C #15: 62.2 °F; T/C #16: 58.2 °F; T/C #17: 64.8 °F;  
 T/C #18: — °F; T/C #19: \_\_\_\_\_ °F; T/C #20: \_\_\_\_\_ °F;  
 T/C #21: \_\_\_\_\_ °F; T/C #22: \_\_\_\_\_ °F; T/C #23: \_\_\_\_\_ °F;  
 T/C #24: \_\_\_\_\_ °F; T/C #25: \_\_\_\_\_ °F; T/C #26: \_\_\_\_\_ °F;

Comments: \_\_\_\_\_

Thermocouple Readout: Pretest Zero/Span Check and Calibration:  
 Zero (0°F) : -0.1 °F Adj to: — °F Post Test Check Zero (0°F): 0.8 °F % Difference +0.17  
 Span (2000°F): 2000.3 °F Adj to: — °F Span (2000°F): 2001.6 °F +0.07

(Allowable % Difference = 1.5%. Use formulas on Woodstove Data Sheet #15 to calculate % Difference) IN degrees absolute

Thermocouple Readout Pretest Linearity Check  
 0°F = 0.3 °F; 200°F = 201.8 °F; 400°F = 399.2 °F;  
 600°F = 601.5 °F; 800°F = 801.6 °F; 1000°F = 1000.8 °F;  
 1200°F = 1198.4 °F; 1400°F = 1399.4 °F; 1600°F = 1600.0 °F;  
 1800°F = 1800.2 °F; 2000°F = 2000.3 °F

Combustion Gas (CO<sub>2</sub>, O<sub>2</sub>, CO) Train Leak Check: Pre OK Post OK PDG  
 Draft (Static) Gauge Zero Check: Pre OK Post OK PDG

Scale Check Pre (Wt, #'s): 771.3 - 766.3 = 5.0 lbs / 5.0 lbs = 0% (AM)  
 Post (Wt, #'s): 773.2 - 768.2 = 5.0 lbs / 5.0 lbs = 0% (PDG)

Stack cleaned prior to the run: Yes \_\_\_\_\_ No ✓  
 Tunnel cleaned prior to the run: Yes \_\_\_\_\_ No ✓

MYREN CONSULTING CERTIFICATION TEST DATA

DILUTION TUNNEL CALCULATIONS

1/25/09, Md=28.56, Bws=4%

6" Tunnel

EPA 2

File Name: KUMA

Manufacturer: KUMA

Model Number: ASHWOOD

Lab Name: MYREN

Test Date: 2/17/09

Run Number: EPA 2

Meter Box Y Factor: 1.0177

Barometric pressure (in): 28.224

Gas meter temp (ave): 90

delta H(ave): 0.900

Gas meter initial reading: 45.9000

Gas meter final reading: 158.4970

Front catch (acetone) mg: 9.4

first filter catch (mg): 11.2

second filter catch (mg): -7.1

Tunnel Flow (Qsd) (dscfm): 141.094

Emission Rate(g/hr): 1.099

Emission Rate(M5H) : 1.968

Avg. of Delta P Sq. Roots: 0.2073

Vs (Avg.)(ft/min): 849.029

Tunnel Avg. Temperature (F): 104.545

Test time(min): 210

Fuel Load(lb. wet): 13.306

Wood moisture(%wet): 16.921

Burn rate(dry kg/hr): 1.433

Sample Volume (dscf): 103.981

Avg. Tunnel Static (-inch H2O): 0.1740

Room Blank Catch (mg/dscf): 0

Emission Factor (g/kg): 0.7672

Pitot Correction Factor: 0.9633

front filter number: 708

back filter number: 707

Beaker Number: 22

PRELIMINARY RESULTS

AUDITED

FINAL RESULTS:

DATA SUMMARY

MODEL: ASHWOOD

RUN: EPA 2

DATE: 2/17/09

DBR: 1.433

EMISSION RATE (g/hr)(M5H) 1.9685

EMISSION FACTOR (g/kg): 0.7672

AVG. % PROPORTIONALITY: 95.756

RUN TIME (min)	PITOT DELTAP (- INCH H2O)	TNL TEMP (°F)	GAS METER RDG (ft3)	GAS METER TEMP (°F)	GAS METER DELTA H (in.H2O)	TUNNEL VELOCITY (ft/min)	PROP RATE (%)	dDGM vol std (ft3)	Tunnel Static (- Inch H2O)	SQUARE ROOT DELTA P	DRY GAS METER RDG (m3)
0	0.040	104	45.9000	73	0.900	849.72			0.167	0.2000	
10	0.045	116	51.3280	76	0.900	910.82	101.4	5.143	0.178	0.2121	
20	0.043	115	56.5780	79	0.900	889.57	99.1	4.947	0.171	0.2074	
30	0.043	116	61.8290	82	0.900	890.34	98.1	4.920	0.170	0.2074	
40	0.043	116	67.1200	85	0.900	890.34	97.8	4.931	0.171	0.2074	
50	0.043	115	72.4280	88	0.900	889.57	96.9	4.919	0.171	0.2074	
60	0.043	113	77.7470	90	0.900	888.02	96.3	4.912	0.173	0.2074	
70	0.043	111	83.0820	91	0.900	886.47	96.0	4.917	0.172	0.2074	
80	0.043	110	88.4500	92	0.900	885.69	96.2	4.939	0.173	0.2074	
90	0.043	107	93.8260	93	0.900	883.36	95.7	4.937	0.173	0.2074	
100	0.043	104	99.1990	94	0.900	881.02	95.1	4.926	0.175	0.2074	
110	0.044	103	104.5870	94	0.900	890.42	94.2	4.939	0.175	0.2098	
120	0.044	101	109.9890	94	0.900	888.84	94.2	4.952	0.177	0.2098	
130	0.045	100	115.3740	95	0.900	898.08	92.5	4.928	0.177	0.2121	
140	0.041	99	120.7610	94	0.900	856.47	97.2	4.938	0.177	0.2025	
150	0.043	97	126.1540	94	0.900	875.54	94.8	4.944	0.176	0.2074	
160	0.043	97	131.5480	95	0.900	875.54	94.5	4.936	0.177	0.2074	
170	0.043	96	136.9390	94	0.900	874.75	94.7	4.942	0.174	0.2074	
180	0.044	95	142.3290	94	0.900	884.07	93.5	4.941	0.177	0.2098	
190	0.043	95	147.7250	94	0.900	873.96	94.7	4.947	0.174	0.2074	
200	0.043	95	153.1200	94	0.900	873.96	94.7	4.946	0.174	0.2074	
210	0.044	95	158.4970	94	0.900	884.07	93.3	4.929	0.177	0.2098	
220			0.0000			0.00	0.0	0.000		0.0000	
230			0.0000			0.00	0.0	0.000		0.0000	
240			0.0000			0.00	0.0	0.000		0.0000	
250			0.0000			0.00	0.0	0.000		0.0000	
260			0.0000			0.00	0.0	0.000		0.0000	
270			0.0000			0.00	0.0	0.000		0.0000	
280			0.0000			0.00	0.0	0.000		0.0000	
290			0.0000			0.00	0.0	0.000		0.0000	
300			0.0000			0.00	0.0	0.000		0.0000	
310			0.0000			0.00	0.0	0.000		0.0000	
320			0.0000			0.00	0.0	0.000		0.0000	
330			0.0000			0.00	0.0	0.000		0.0000	
340			0.0000			0.00	0.0	0.000		0.0000	
350			0.0000			0.00	0.0	0.000		0.0000	
360			0.0000			0.00	0.0	0.000		0.0000	
370			0.0000			0.00	0.0	0.000		0.0000	
380			0.0000			0.00	0.0	0.000		0.0000	

DATE: 2/17/09 PAGE 1 OF 2 UNIT: Kama Ashwood RUN: EPA2

METER BOX: 456-P METER Y: 1.0177 FILTER #'S: (F) 708 (R) 707

.721/.7215  
PRE TEST LEAK CHECK: .0005 CFM @ -16.1 IN HG FILTER SIZE: 110 mm

.559/1.560  
POST TEST LEAK CHECK: .001 CFM @ -15.5 IN HG PROBE LENGTH 21.5 IN

TIME		METER READING	PITOT		TUNNEL TEMP	METER TEMP	GAS METER	VAC
CLOCK	ELAPSED	(FT <sup>3</sup> )	ΔP	Pg	(°F)	(°F)	Δh	(in Hg)
1340	00	45.900	-1040	-167	104	73	0.90	0
	10	51.328	1045	-1178	116	76	1.90	0
1400	20	56.578	1043	-1171	115	79	1.90	0
	30	61.829	1043	-1170	116	82	1.90	0
	40	67.120	1043	-1171	116	85	1.90	0
	50	72.428	1043	-1171	115	88	1.90	0
	60	77.747	1043	-1173	113	90	1.90	0
	70	83.082	1043	-1172	111	91	1.90	0
1500	80	88.450	1043	-1173	110	92	1.90	0
	90	93.826	1043	-1173	107	93	1.90	0
	100	99.199	1043	-1175	104	94	1.90	0
	110	104.587	1044	-1175	103	94	1.90	0
	120	109.969	1044	-1177	101	94	1.90	0
	130	115.374	1045	-1177	100	95	1.90	0
1600	140	120.761	1044	-1177	99	94	1.90	0
	150	126.154	1043	-1176	97	94	1.90	0
	160	131.548	1043	-1177	97	95	1.90	0
	170	136.939	1043	-1174	96	94	1.90	0
	180	142.329	1044	-1177	95	94	1.90	0
	190	147.725	1043	-1174	95	94	1.90	0

BP

00	26.21	_____	_____
60	26.22	_____	_____
120	28.22	_____	_____
180	28.23	_____	_____
210	26.24	_____	_____
AVG. =		26.224	

Pre Test Filter  
Check Weighing  
F .6709  
R .6781

End of Test Weight  
F .6835 R .6722  
.6702 .6777  
.0133

METHOD 5G -1

PARTICULATE SAMPLING DATA

Rev. 2/09

DATE: 2/17/09 PAGE 2 OF 2 UNIT: Kuma Ashwood RUN: EPA 2

METER BOX: 45G-P METER Y: 1.0177 FILTER #'S: (F) 708 (R) 707

PRE TEST LEAK CHECK: <sup>1.721 / 1.725</sup> 10005 CFM @ -16.1 IN HG FILTER SIZE: 110 mm

POST TEST LEAK CHECK: <sup>1.559 / 1.560</sup> 1001 CFM @ 75.5 IN HG PROBE LENGTH 21.5 IN

TIME		METER READING (FT <sup>3</sup> )	PITOT		TUNNEL TEMP (°F)	METER TEMP (°F)	GAS METER Δh	VAC (in Hg)
CLOCK	ELAPSED		ΔP	Pg				
1700	200	153.120	1043	-174	95	94	190	0
10	210	158.497	1044	-177	95	94	190	0
	20							
	30							
	40							
	50							
	60							
	70							
	80							
	90							
	00							
	10							
	20							
	30							
	40							
	50							
	60							
	70							
	80							
	90							

BP

00	28.21	_____	_____
60	28.22	_____	_____
120	28.22	_____	_____
180	28.23	_____	_____
240	28.24	_____	_____

AVG. = \_\_\_\_\_

Pre Test Filter  
Check Weighing  
F 16709  
R 16781

End of Test Weight  
F 16702 R 16777

MYREN CONSULTING, INC.

Dilution Tunnel Traverse Data with 8 Traverse Points

Unit: KUMUL Ashwood

Run #: EPA 2

Date: 2/17/09

Technicians: ATM JEP POG

Rev 4/2/08

Point	Location	$\Delta p$	$\sqrt{\Delta p_{trav}}$	$\Delta p$	$\sqrt{\Delta p_{cent}}$	$T_{trav}$	$T_{cent}$	Pg
-------	----------	------------	--------------------------	------------	--------------------------	------------	------------	----

W-1	0.5'	<u>.040</u>	<u>.2000</u>	<u>.040</u>	<u>.2074</u>	<u>105</u>	<u>105</u>	<u>- .166</u>
2	1.5	<u>.041</u>	<u>.2025</u>	<u>.043</u>	<u>.2074</u>	<u>105</u>	<u>105</u>	<u>- .166</u>
Center	Center							
3	4.5	<u>.041</u>	<u>.2098</u>	<u>.042</u>	<u>.2049</u>	<u>104</u>	<u>104</u>	<u>- .168</u>
4	5.5	<u>.034</u>	<u>.1844</u>	<u>.040</u>	<u>.2049</u>	<u>104</u>	<u>104</u>	
S-1	0.5	<u>.036</u>	<u>.1897</u>	<u>.040</u>	<u>.2049</u>	<u>104</u>	<u>104</u>	
2	1.5	<u>.041</u>	<u>.2025</u>	<u>.042</u>	<u>.2049</u>	<u>104</u>	<u>104</u>	
Center	Center							
3	4.5	<u>.042</u>	<u>.2049</u>	<u>.042</u>	<u>.2049</u>	<u>104</u>	<u>104</u>	
4	5.5	<u>.038</u>	<u>.1949</u>	<u>.040</u>	<u>.2049</u>	<u>104</u>	<u>104</u>	

Totals 1.5887 .4123 835 209 -.334

Average .1986 .20615 101.375 104.5 -.167

$^{\circ}R = (^{\circ}F + 460)$

$P_s = BP + (-Pg/13.6) = 28.21 + (-.167/13.6) = 28.198" Hg$

LEAK CHECKS:

Pre Test: Pg Leg: ✓ GRP Velocity Head Leg: ✓ GRP

Post Test: Pg Leg: ✓ PPG Velocity Head Leg: ✓ PPG

Rev 4/19/08

DILUTION TUNNEL GAS VELOCITY & VOLUMETRIC FLOW RATE CALCULATIONS

UNIT: KUMA Ashwood DATE: 2/17/09 RUN #: EPA 2 TECHNICIAN(S): ATM JEP  
PDG

Average Gas Velocity in the Dilution Tunnel  $V_{strav}$  (EPA M2 EQN 2-9, ASTM E 2515-07 EQN 7)

$$(9) V_{strav} = (85.49) \left( \frac{0.99 \text{ cp}}{1} \right) \left( \frac{1986}{\Delta P} \right) \times \sqrt{\Delta P} \text{ "H}_2\text{O} \left( \frac{564.375}{(0)} \right) \left( \frac{T_s}{^\circ A} \right) = 14,071.0 \text{ fps}$$

$$(9A) V_s = \left( \frac{14,071.0 \text{ fps}}{(2)} \right) (60) = \frac{844,261}{(2)} \text{ fpm}$$

Gas Velocity in the center of the Dilution Tunnel -  $V_{scent}$  (EPA M2 EQN 2-9, ASTM E 2515-07 EQN 7)

$$(9) V_{scent} = (85.49) \left( \frac{0.99 \text{ cp}}{1} \right) \left( \frac{20615}{\Delta P} \right) \times \sqrt{\Delta P} \text{ "H}_2\text{O} \left( \frac{564.5}{(0)} \right) \left( \frac{T_s}{^\circ A} \right) = 14,607.6 \text{ fps}$$

$$(9A) V_s = \left( \frac{14,607.6 \text{ fps}}{(2)} \right) (60) = \frac{876,453}{(2)} \text{ fpm}$$

EPA M5G1 Section 4.2.2, ASTM E 2515-07 EQN 1 Adjustment Factor for Center of Tunnel Pitot Tube Location

$$F_p = V_{strav} / V_{scent} = \frac{14,071.0}{14,607.6} = 0.9633$$

Average Stack Gas Dry Volumetric Flow Rate -  $Q_{sd}$  (EPA M2 EQN 2-10, ASTM E 2515-07 EQN 3)

$$(10) Q_{sd} = 3600 (1 - 0.04 Bws) \left( \frac{14,071 \text{ fps}}{(2)} \right) \left( \frac{1963 \text{ ft}^2}{(3)} \right) \left( \frac{28.198 \text{ Ps "Hg}}{(2)} \right) \left( \frac{564.375 T_s}{(0)} \right) (29.92" \text{ Hg}) =$$

$$\frac{8,416,700}{(1)} \text{ dscfh (or dscfh)}$$

$$(10A) \frac{8,416,700}{(1)} \text{ dscfh} \div 60 = \frac{140,278}{(1)} \text{ dscfm (or dscfm)}$$

Note: Number in { } under blank lines denotes number of decimals to be used. If a blank calls for an answer already calculated, use the number of decimals previously specified for that answer.

WOODSTOVE DATA SHEET #4-1: INITIAL FILTER WEIGHTS (TARE WEIGHTS)

Into Dessicator: Date 1-22-09 Time 1149 By PDG Front Half X Back Half X

Manufacturer: Pall P/N. 60115 Size: 110 Lot.No.: 70726 Grade: A/E GLASS

Filter #	First Wt	2009 Date	Time	By	Second Wt	Date	Time	By	Third Wt	2009 Date	Time	By
700	.6873	1-22	1331	GRP	.6877	1-23	1417	PDG				
701	.6871		1330	GRP	.6878		1419	PDG	.6877	1-26	1421	GRP
702	.6816		1329	GRP	.6825		1420	PDG	.6824	1-26	1420	GRP
703	.6761		1328	GRP	.6762		1421	PDG				
704	.6727		1327	GRP	.6732		1420	PDG				
705	.6833		1326	GRP	.6837		1423	PDG				
706	.6946		1325	GRP	.6948		1424	PDG				
707	.6773		1324	GRP	.6777		1425	PDG				
708	.6701		1323	GRP	.6702		1426	PDG				
709	.6799		1322	GRP	.6809		1427	PDG	.6806	1-26	1419	GRP
710	.6587		1321	GRP	.6590		1428	PDG				
711	.6654		1320	GRP	.6656		1429	PDG				
712	.6688		1319	GRP	.6692		1430	PDG				
713	.6864		1318	GRP	.6866		1431	PDG				
714	.6651		1318	GRP	.6655		1432	PDG				
715	.6741		1317	GRP	.6744		1433	PDG				
716	.6592		1316	GRP	.6590		1434	PDG				
717	.6531		1315	GRP	.6536		1435	PDG				
718	.6621		1314	GRP	.6623		1436	PDG				
719	.6769		1313	GRP	.6769		1437	PDG				
720	.6627		1312	GRP	.6628		1438	PDG				
721	.6567		1311	GRP	.6569		1439	PDG				
722	.6539		1310	GRP	.65340		1440	PDG				
723	.6552		1309	GRP	.6552		1441	PDG				
724	.6655		1308	GRP	.6656		1442	PDG				

Checked by A.T. Meyer Date: 1/27/09 Time 1632

QA REWEIGH

Filter #	WT	Date	Time	By
703	.6761	1/27/09	1639	ATM
708	.6705	✓	1640	ATM
715	.6749	✓	1642	ATM

BALANCE ROOM ENVIRONMENTAL CONDITIONS

WB	DB	%RH	Date	Time	By
57	72	38	1-22-09	1138	ATM
58	75	33	1-23-09	1158	PDG
56	76	25	1-26-09	1359	GRP

58 72 31 1/27/09 1530 PDG

Post 0.0000 100.0000  
 P-22 0.0000  
 W23 0.0000  
 1.26 0.0000  
 99.9994 99.9993  
 99.9993



WOODSTOVE DATA SHEET #4-2:  
INITIAL BEAKER WEIGHTS (TARE WEIGHTS)

Into Dessicator: Date: 01.26.09 Time: 15:38 By: GRP

Beaker #	First Wt.	2009 Date	Time	By	Second Wt.	2009 Date	Time	By	Third Wt.	Date	Time	By
20	73.3181	1/27	1532	PDG	73.3176	1-29	1459	GRP		1/30		
21	71.0021		1534	PDG	71.0018		1458	GRP				
22	71.8343		1535	PDG	71.8338		1457	GRP				
23	70.9390		1536	PDG	70.9389		1455	GRP				
27	72.3310		1538	PDG	72.3307		1500	GRP				
31	69.6672		1539	PDG	69.6669		1501	GRP				
32	53.6002		1541	PDG	53.5993		1502	GRP	53.5998		1505	PDG
37	53.7267		1542	PDG	53.7262		1504	GRP				
38	53.2525		1544	PDG	53.2516		1505	GRP	53.2520		1306	PDG
39	53.1509		1545	PDG	53.1493		1506	GRP	53.1496		1311	PDG
40	53.4626		1547	PDG	53.4622		1507	GRP				
41	52.8371		1549	PDG	52.8367		1508	GRP				
42	53.8699		1550	PDG	53.8692		1509	GRP	53.8696		1302	PDG

Checked By: ATM Date: 2/1/09 Time: 12:10

QA REWEIGH

Beaker #	WT	Date	Time	By
20	73.3181	2/1/09	1215	ATM
21	69.6671		1217	ATM
42	53.8699		1219	ATM

BALANCE ROOM ENVIRONMENTAL CONDITIONS

WB	DB	%RH	2009 Date	Time	By
55	72	31	1/27	1530	PDG
58	77	29	1-29	1436	GRP
60	72	49	1/30	1256	PDG
58	74	37	2/1	1200	ATM

1/27 0.0000 09.0000  
1-29 0.0000 09.0000  
1/30 0.0000 09.0000  
2/1 0.0000 09.0000

POST

WOODSTOVE DATA SHEET #4-2:  
INITIAL BEAKER WEIGHTS (TARE WEIGHTS)

Blank done 12/9/07

Into Dessicator: Date: 10/12/07 Time: 0801 By: GRP

Beaker #	First Wt	Date	Time	By	Second Wt	Date	Time	By	Third Wt	Date	Time	By
22	71.8343	10/22/07	1358	GRP	71.8332	11/10/07	1938		71.8330	11-11-07	1746	Jm
24	73.2192		1400	GRP	73.2190	11/10/07	1940		73.2193	11-11-07	1746	Jm
25	72.6516		1401	GRP	72.6512	11/10/07	1944		← Blank			
26	71.7895		1403	GRP	71.7888	11/10/07	1939		71.7886	11-11-07	1747	Jm
27	72.3316		1402	GRP	72.3314	11/10/07	1945					
28	70.5979		1404	GRP	70.5975	11/10/07	1941		70.5977	11-11-07	1745	Jm
39	53.1508		1405	GRP	53.1500	11/10/07	1942					
37	53.7237	11/10/07	1945	MM	53.7238	11/11/07	1743					Jm

Checked By: \_\_\_\_\_ Date: \_\_\_\_\_ Time: \_\_\_\_\_

QA REWEIGH

Beaker #	WT	Date	Time	By
27	72.3315	11-11	1740	Jm
25	72.6515	11-11	1741	Jm
39	53.1509	11-11	1744	Jm

BALANCE ROOM ENVIRONMENTAL CONDITIONS

WB	DB	%RH	Date	Time	By
57	68	50	10/22/07	1344	GRP
			11/10		

Post weighing  
0.0000g  
1st  
0.0000  
2nd

WOODSTOVE DATA SHEET #4-3: CONSTANT FINAL WEIGHTS

FINAL BEAKER WEIGHTS

Beaker #	Into Dessic	2009 Date	Time	By	First	Date	Time	By	Second	Date	Time	By	Third	Date	Time	By
22	✓	2/20	1021	PDG	71.0432	2/21	1533	ATM	71.8448	2/22	1231	Jac	71.0436	2/23	1412	PDG
					71.9432	2/24	1000	ATM								

FINAL FILTER WEIGHTS

Filter #	Into Dessic	2009 Date	Time	By	First	Date	Time	By	Second	Date	Time	By	Third	Date	Time	By
F 708	.6835	2/17	1805	ATM	.6827	2/18	1816	ATM	.6815	2-19	1317	GRP	.6819	2/20	1043	PDG
R 707	.6722	2/17	1805	ATM	.6709	2/18	1815	ATM	.6706	2-19	1318	GRP				

lots of R Filter staged on Frnt

QA REWEIGH: FINAL WEIGHTS

Date	Beaker #	Final Wt	By
Date	Filter #	Final WT	By

SCALE ROOM ENVIRONMENTAL CONDITIONS

Weighing Session	2009 Date	Time	By	WB	DB	%RH
1	2/18	1600	ATM	85	70	36
2	2/19	1248	GRP	56	73	32
3	2/20	1018	PDG	57	74	33
4	2/22	1222	ATM	47	59	37
5	2/23	1406	PDG	80	20	46

SCALE ROOM ENVIRONMENTAL CONDITIONS

	2/24	0453	ATM	59	76	35
6						
7						
8						
9						
Comments						

Acadone  
Lot #  
041648

Blank  
done  
12/10/07

WST5-Form 9, Pg 1, Rev 4/90  
Unit 15000  
Run # 15000  
Date: 1/17/09

WOODSTOVE DATA SHEET #4-3: CONSTANT FINAL WEIGHTS

Table 7/6812

FINAL BEAKER WEIGHTS

Beaker #	Into Dessic	2007 Date	Time	By	First	Date	Time	By	Second	Date	Time	By	Third	Date	Time	By
35	✓	12/12	1546	JRP	72.6508	12/13	1342	JRP	72.6511	12/14	1349	JRP				

FINAL FILTER WEIGHTS

Filter #	Into Dessic	Date	Time	By	First	Date	Time	By	Second	Date	Time	By	Third	Date	Time	By

QA NEWZICK: FINAL WEIGHTS

Date	Beaker #	Final Wt	By
Date	Filter #	Final Wt	By

SCALE ROOM ENVIRONMENTAL CONDITIONS

Weighting Session	Date	Time	By	WB	DB	ZRH
1	12/13	1207	JRP	55	73	29
2	12/14	1321	JRP	57	75	31
3						
4						

SCALE ROOM ENVIRONMENTAL CONDITIONS

6	7	8	9	Comments

WOODSTOVE DATA SHEET 4-4 SCALE QC RECORD SHEET

SCALE: SARTORIUS  
 MODEL: CP224S  
 SN: 170550374

FROM: 9/27/2007  
 THROUGH: 12/7/2007

Level	Recall	130 g	100 g	10 g	1.0 g	100 mg	20 mg	Date	Time	Tech	Wet Bulb	Dry Bulb	% RH
✓	N	129.9998	99.9998	10.0000	1.0000	0.1000	0.0199	9/27/07	1402	GRP	55	67	45
✓	Y	129.9995	99.9996	10.0001	1.0000	0.1000	0.0200	9/28/07	1335	GRP	57	69	46
✓	Y	129.9996	99.9996	9.9999	1.0000	0.1000	0.0200	10/1/07	1505	ATM	56	70	48
✓	N	129.9995	99.9996	10.0000	1.0000	0.1000	0.0199	10/2/07	1611	GRP	56	68	46
✓	N	129.9997	99.9997	9.9999	1.0000	0.1000	0.0199	10/3/07	1122	GRP	56	68	46
✓	N	129.9996	99.9996	10.0000	1.0000	0.0999	0.0199	10/4/07	1005	GRP	55	67	45
✓	Y	129.9996	99.9996	10.0000	1.0000	0.1000	0.0199	10/5/07	0750	GRP	51	62	45
✓	N	129.9997	99.9997	9.9999	1.0000	0.1000	0.0199	10/5/07	1513	GRP	56	69	43
✓	Y	129.9996	99.9996	10.0000	1.0000	0.1000	0.0200	10/7/07	1505	ATM	58	71	44
✓	N	129.9996	99.9997	10.0000	1.0000	0.1000	0.0200	10/12/07	1259	ATM	58	70	48
✓	Y	129.9995	99.9996	9.9999	1.0000	0.1000	0.0199	10/22/07	1344	GRP	57	68	50
✓	Y	129.9996	99.9997	9.9999	1.0000	0.1000	0.0199	10/24/07	1338	GRP	53	63	50
✓	N	129.9995	99.9995	10.0000	1.0000	0.1000	0.0200	10/30/07	0933	ATM	56	70	40
✓	Y	129.9996	99.9997	10.0000	1.0000	0.1000	0.0199	10/30/07	1457	GRP	55	70	36
✓	Y	129.9996	99.9996	9.9999	1.0000	0.1000	0.0199	10/31/07	1528	GRP	57	75	30
✓	Y	129.9996	99.9996	9.9999	1.0000	0.0999	0.0199	11/2/07	1038	GRP	50	67	33
✓	Y	129.9996	99.9996	10.0000	1.0000	0.1000	0.0199	11/5/07	0730	GRP	57	73	35
✓	Y	129.9996	99.9997	10.0000	1.0000	0.1000	0.0200	11/9/07	1550	ATM	58	70	48
✓	N	129.9996	99.9997	10.0000	1.0000	0.1000	0.0200	11/10/07	1635	ATM	58	71	44
✓	Y	129.9997	99.9997	9.9999	1.0000	0.1000	0.0199	11/10/07	1810	ATM	55	69	39
✓	N	129.9997	99.9996	9.9999	1.0000	0.1000	0.0199	11/12/07	0822	GRP	54	67	41
✓	N	129.9996	99.9996	10.0000	1.0000	0.1000	0.0199	11/20/07	1226	ATM	58	72	41
✓	N	129.9998	99.9997	9.9999	0.9999	0.1000	0.0200	11/14/07	1710	GRP	58	73	39
✓	QC	Services Audit 11/17/07											
✓	Y	129.9997	99.9997	10.0000	1.0000	0.1000	0.0200	11/15/07	1350	ATM	59	72	45
✓	N	129.9996	99.9996	9.9999	0.9999	0.1000	0.0200	11/16/07	1600	GRP	58	71	44
✓	N	129.9996	99.9996	10.0000	1.0000	0.1000	0.0199	11/19/07	1758	ATM	60	74	43
✓	Y	129.9997	99.9997	10.0000	1.0000	0.1000	0.0200	11/19/07	1143	ATM	56	70	40
✓	Y	129.9995	99.9996	10.0000	1.0000	0.1000	0.0199	11/20/07	1416	GRP	54	69	35
✓	N	129.9996	99.9996	10.0000	1.0000	0.1000	0.0200	11/21/07	1110	ATM	57	70	44
✓	N	129.9995	99.9996	10.0000	1.0000	0.1000	0.0199	12/3/07	0730	GRP	55	69	40
✓	N	129.9996	99.9996	10.0000	1.0000	0.0999	0.0200	12/6/07	1125	ATM	54	67	44
✓	Y	129.9996	99.9996	10.0000	1.0000	0.1000	0.0200	12/17/07	1348	GRP	55	69	40

WOODSTOVE DATA SHEET 4-4 SCALE QG RECORD SHEET

SCALE: SARTORIUS  
 MODEL: CP224S  
 SN: 17050374

FROM: 12/2/07  
 THROUGH: 2/3/08

Level	Recali	130 g	100 g	10 g	1.0 g	100 mg	20 mg	Date	Time	Tech	Wet Bulb	Dry Bulb	% RH
✓	N	129.9996	99.9996	10.0000	1.0000	0.1000	0.0200	12/8	12:15	ATM	57	73	35
✓	N	129.9996	99.9996	10.0000	1.0000	0.1000	0.0200	12/8	19:10	ATM	57	72	38
✓	N	129.9997	99.9996	10.0000	1.0000	0.1000	0.0199	12/9	19:35	ATM	55	72	31
✓	Y	129.9996	99.9996	10.0000	1.0000	0.1000	0.0200	12/10	19:53	ATM	56	72	34
✓	N	129.9997	99.9997	10.0000	1.0000	0.1000	0.0199	12/11	16:18	GRP	57	76	28
✓	N	129.9997	99.9996	10.0000	1.0000	0.0999	0.0199	12/12	5:05	GRP	56	74	30
✓	N	129.9996	99.9996	9.9999	0.9999	0.1000	0.0199	12/13	3:07	GRP	55	73	29
✓	N	129.9996	99.9996	9.9999	0.9999	0.1000	0.0199	12/14	13:21	GRP	57	75	31
✓	N	129.9996	99.9996	9.9999	0.9999	0.1000	0.0199	12/15	16:02	GRP	57	75	31
✓	Y	129.9996	99.9997	9.9999	1.0000	0.1000	0.0199	12/17	08:17	GRP	55	73	29
✓	N	129.9997	99.9997	10.0000	1.0000	0.1000	0.0199	12/18	08:53	GRP	58	75	34
✓	N	129.9997	99.9997	10.0000	1.0000	0.1000	0.0199	12/19	08:12	GRP	55	72	31
✓	N	129.9997	99.9997	10.0000	1.0000	0.0999	0.0199	12/20	09:16	GRP	57	71	41
✓	Y	129.9995	99.9996	10.0000	1.0000	0.1000	0.0199	12/21	10:35	ATM	55	70	36
✓	Y	129.9998	99.9997	10.0000	1.0000	0.1000	0.0200	12/22	14:34	ATM	57	66	44
✓	N	129.9996	99.9996	10.0000	1.0000	0.1000	0.0200	12/23	09:15	ATM	57	70	44
✓	N	129.9996	99.9996	9.9999	1.0000	0.1000	0.0199	12/26	12:30	ATM	57	70	44
✓	N	129.9996	99.9997	10.0000	1.0000	0.1000	0.0200	12/27	10:30	ATM	56	72	34
✓	N	129.9997	99.9997	9.9999	1.0000	0.1000	0.0200	1/8/08	13:42	GRP	54	68	38
✓	N	129.9997	99.9997	10.0000	1.0000	0.1000	0.0200	1/9/08	07:42	GRP	55	70	36
✓	N	129.9997	99.9997	10.0000	1.0000	0.1000	0.0199	1/11/08	10:40	ATM	59	73	42
✓	Y	129.9996	99.9997	10.0000	1.0000	0.1000	0.0199	1/16/08	12:21	GRP	51	72	18
✓	N	129.9999	99.9998	10.0000	1.0000	0.1000	0.0199	1/17/08	12:37	GRP	56	71	37
✓	N	129.9998	99.9998	10.0000	1.0000	0.0999	0.0200	1/18/08	11:16	GRP	56	71	37
✓	Y	129.9995	99.9996	10.0000	1.0000	0.1000	0.0199	1/21/08	14:26	GRP	56	72	34
✓	N	129.9995	99.9996	10.0000	1.0000	0.1000	0.0199	1/22/08	15:13	GRP	56	71	37
✓	Y	129.9996	99.9996	9.9999	1.0000	0.1000	0.0199	1/23/08	08:05	GRP	54	69	36
✓	Y	129.9996	99.9996	10.0000	1.0000	0.1000	0.0200	1/24/08	07:58	GRP	54	70	33
✓	N	129.9998	99.9997	10.0000	1.0000	0.1000	0.0199	1/24/08	14:50	GRP	56	71	37
✓	N	129.9997	99.9996	10.0000	1.0000	0.1000	0.0200	1/31/08	15:05	GRP	55	69	38
✓	N	129.9996	99.9996	10.0000	1.0000	0.1000	0.0199	2/1/08	10:29	GRP	54	69	36
✓	N	129.9996	99.9996	9.9999	1.0000	0.1000	0.0199	2/2/08	16:20	ATM	58	72	41
✓	N	129.9996	99.9997	10.0000	1.0000	0.1000	0.0200	2/3/08	17:10	ATM	57	70	44

SCALE: SARTORIUS  
 MODEL: CP224S  
 SN: 17050374

WOODSTOVE DATA SHEET 4-4 ANALYTICAL BALANCE QC RECORD SHEET

FROM: 12/20/08  
 THROUGH: 2/17/09

Level	Recall	140 g	100 g	10 g	1.0 g	100 mg	20 mg	Date	Time	Tech	Wet Bulb	Dry Bulb	% RH
✓	N	139.9993	99.9993	9.9999	1.0000	0.1000	0.0199	12/20/08	1430	ADM	58	72	42
✓	N	139.9995	99.9995	9.9999	1.0000	0.1000	0.0199	12/23/08	1057	GRP	60	76	38
✓	N	137.9994	99.9994	9.9999	1.0001	0.1000	0.0200	12/24/08	1019	ATM	59	72	43
✓	N	139.9994	99.9994	9.9999	1.0000	0.1000	0.0200	12/24/08	1142	ATM	59	72	45
✓	N	139.9994	99.9994	9.9999	1.0000	0.1000	0.0200	12/24/08	1050	ATM	60	75	37
✓	N	139.9994	99.9994	9.9999	1.0000	0.1000	0.0199	1/6/09	1157	PDG	58	75	34
✓	N	139.9994	99.9994	9.9999	1.0000	0.1000	0.0199	1/6/09	1845	ATM	60	75	37
✓	N	139.9995	99.9996	9.9999	1.0000	0.1000	0.0199	1/7/09	1530	GRP	58	70	48
✓	N	139.9994	99.9994	9.9999	1.0000	0.1000	0.0199	1/8/09	1356	PDG	60	72	49
✓	Yes	139.9993	99.9994	9.9999	1.0000	0.1000	0.0200	1/09/09	1053	PDG	58	72	42
✓	Yes	139.9993	99.9993	9.9999	1.0000	0.1000	0.0199	1/11/09	1128	JRP	55	72	37
✓	NO	139.9994	99.9995	9.9999	1.0000	0.1000	0.0199	1/12/09	0845	PDG	59	75	38
✓	NO	139.9992	99.9993	9.9999	1.0000	0.1000	0.0200	1/13/09	0825	JRP	58	74	37
✓	Yes	139.9993	99.9994	9.9999	1.0000	0.1000	0.0199	1/14/09	1212	PDG	57	72	36
✓	NO	139.9992	99.9993	9.9999	1.0000	0.1000	0.0199	1/14/09	1420	GRP	59	75	37
✓	Yes	139.9994	99.9995	9.9999	1.0000	0.1000	0.0199	1/15/09	1126	GRP	57	74	37
✓	NO	139.9993	99.9994	9.9999	1.0000	0.1000	0.0199	1/20/09	0930	PDG	58	74	37
✓	NO	139.9993	99.9993	9.9999	1.0000	0.1000	0.0199	1/20/09	1230	PDG	56	71	35
✓	NO	139.9994	99.9994	9.9999	1.0000	0.1000	0.0200	1/20/09	1613	JRP	57	73	35
✓	NO	139.9993	99.9993	9.9999	1.0000	0.1000	0.0200	1/22/09	1130	ATM	57	72	38
✓	NO	139.9993	99.9993	9.9999	1.0000	0.1000	0.0199	1/23/09	1150	PDG	58	75	33
✓	YES	139.9992	99.9993	10.0000	1.0000	0.1000	0.0200	1/26/09	1359	JRP	56	76	35
✓	NO	139.9994	99.9995	10.0000	1.0000	0.1000	0.0199	1/27/09	1530	PDG	57	72	31
✓	NO	139.9993	99.9993	10.0000	1.0000	0.1000	0.0200	1/26/09	1452	ATM	61	75	41
✓	YES	139.9993	99.9994	10.0000	1.0000	0.1000	0.0199	1/29/09	1430	GRP	58	77	29
✓	NO	139.9995	99.9995	9.9999	1.0000	0.1000	0.0199	1/30/09	1256	PDG	60	72	49
✓	YES	139.9994	99.9994	9.9999	1.0000	0.1000	0.0199	2/1/09	1200	ATM	59	74	37
✓	NO	139.9993	99.9993	9.9999	1.0000	0.1000	0.0199	2/2/09	1350	GRP	58	77	29
✓	Yes	139.9995	99.9996	9.9999	1.0000	0.1000	0.0199	2/5/09	1118	PDG	59	72	45
✓	NO	139.9995	99.9995	9.9999	1.0000	0.1000	0.0199	2/6/09	1150	GRP	57	74	33
✓	NO	139.9994	99.9994	10.0000	1.0000	0.1000	0.0200	2/9/09	1016	ATM	49	70	19
✓	NO	139.9994	99.9994	9.9999	1.0000	0.1000	0.0199	2/16/09	1501	PDG	61	78	36
✓	NO	139.9993	99.9994	9.9999	1.0000	0.1000	0.0200	2/17/09	1139	JRP	56	72	35

SCALE: SARTORIUS  
 MODEL: CP224S  
 SN: 17050374

WOODSTOVE DATA SHEET 4-4 ANALYTICAL BALANCE QC RECORD SHEET

FROM: 2/10/09  
 THROUGH:

Level	Recali	140 g		100 g		10 g		1.0 g		100 mg		20 mg		Wet		Dry	
		Weights	Weight	Weights	Weight	Weights	Weight	Weights	Weight	Weights	Weight	Weights	Weight	Tech	Bulb	Bulb	& RH
Y	Y	139.9993	99.9994	99.9994	9.9999	1.0000	0.1000	0.0199	0.0199	2/10/09	1800	ATM	55	70	36		
Y	Y	139.9993	99.9994	99.9994	9.9999	1.0000	0.1000	0.0199	0.0199	2/10/09	1848	TRP	56	73	32		
Y	Y	139.9993	99.9994	99.9994	9.9999	1.0000	0.1000	0.0199	0.0199	2/20/09	1018	PDG	57	74	33		
Y	Y	139.9993	99.9994	99.9994	9.9999	1.0000	0.1000	0.0200	0.0200	2/21/09	1519	ATM	60	77	35		
Y	Y	139.9993	99.9994	99.9994	9.9999	1.0000	0.1000	0.0199	0.0199	2/22/09	1222	ATM	77	59	37		
Y	Y	139.9994	99.9994	99.9994	9.9999	1.0000	0.1000	0.0199	0.0199	2/23/09	1406	PDG	58	70	48		
Y	No	139.9994	99.9994	99.9994	9.9999	1.0000	0.1000	0.0200	0.0200	2/24/09	0953	ATM	59	76	35		
Y	Y	139.9995	99.9995	99.9995	9.9999	1.0000	0.1000	0.0199	0.0199	2/25/09	123	PDG	60	76	38		
Y	Y	139.9994	99.9994	99.9994	9.9999	1.0000	0.1000	0.0199	0.0199	2-26/09	1258	TRP	55	70	36		
Y	Y	139.9993	99.9993	99.9993	9.9999	1.0001	0.1001	0.0200	0.0200	2/26/09	1320	ATM	57	74	33		
Y	Y	139.9995	99.9995	99.9995	9.9999	0.9999	0.1000	0.0199	0.0199	3/3/09	1431	PDG	59	76	35		
Y	Y	139.9993	99.9993	99.9993	9.9999	1.0000	0.1000	0.0199	0.0199	3/4/09	1556	TRP	56	70	40		
Y	No	139.9994	99.9994	99.9994	9.9999	1.0001	0.1001	0.0200	0.0200	3/5/09	1350	ATM	60	75	30		
Y	No	139.9993	99.9993	99.9993	9.9999	1.0000	0.1000	0.0200	0.0200	3/9/09	0850	ATM	57	71	41		
Y	Y	139.9993	99.9993	99.9993	10.0000	1.0001	0.1000	0.0200	0.0200	3/16/09	1323	ATM	55	70	36		
Y	Y	139.9993	99.9993	99.9993	9.9999	1.0000	0.1000	0.0199	0.0199	3/16/09	1212	PDG	50	75	10		



Woodstove Particulate  
 Catch Processing Sheet  
 Woodstove Data Sheet #5  
 EPA M5G-1

Unit: Kuma Ashwood  
 Run: EPA 2  
 Date: 2/17/09  
 Technicians: ATM  
 Revised 1/16/98-Data Sheet #5

Filters

Filter # (Front) 708 Beaker # 22  
 Final Wt. .6814 g MI 55  
 Tare Wt. .6702 g Desc. Acetone  
 Net Wt. .0112 g

Final Wt. 71.8432 g  
 Tare Wt. 71.8338 g  
 Net Wt. .0094 g

Filter # (Rear) 707 Beaker # \_\_\_\_\_  
 Final Wt. .6706 g MI \_\_\_\_\_  
 Tare Wt. .6777 g Desc. \_\_\_\_\_  
 Net Wt. -.0071 g

Final Wt. \_\_\_\_\_ g  
 Tare Wt. \_\_\_\_\_ g  
 Net Wt. \_\_\_\_\_ g

Acetone Blank Calculation:

Blank Date: 12/8/07

Blank Beaker # 25  
 MI 50  
 Desc. Acetone

Final Wt. 72.6511 g  
 Tare Wt. 72.6512 g  
 Net Wt. -0.0001 g

= 0.0000

0.0000 g ÷ 50 ml = 0.00000 g/ml

Blank Residue Value Calculation:

0.00000 g/ml acetone X 55 ml acetone = 0.0000 g  
 Blank Residue Value

Total Particulate Catch Calculation

Filter: .0112 g  
 Filter: -.0071 g  
 Beakers: .0094 g - 0.0000 g = .0094 g  
 Total Catch Blank Residue Value  
 Total Catch = .0135 g

Unit Kuma Ashwood  
 Run # EPA 2  
 Date 2/17/09  
 Technician ATM JRP PDG  
 WST6-Form1, Rev8/96

MISCELLANEOUS TEST DATA  
 WOODSTOVE DATA SHEET #8

Useable Firebox Dimensions: See QC Section Useable Volume: 2.094 ft<sup>3</sup>

Dilution Tunnel Draft (If applicable): Start .000 Stop .000 <sup>"H<sub>2</sub>O</sup>

Test Chamber Air Velocity: Start: 00.0 Stop: 00.0 Avg: 00.0 ft/min

Wet Bulb/ Start: WB: 59 °F DB: 77 °F 1.05% Amb Moisture 33 %RH

Dry Bulb Stop: WB: 59 °F DB: 77 °F 1.05% Amb Moisture 33 %RH

$\bar{X} = 1.05$  % Ambient Moisture  $\bar{X} = 33.0$  % Relative Humidity (RH)

Empty Stove Wt: 440.2 lbs.

Empty Stove Wt with Stack (Inc. Oil Seal) Wet: 763.8 lbs. Dry: 763.8 lbs. <sup>Just</sup>

Empty Stove Wt with Stack and Ash Ash: — lbs. Total: — lbs.

Kindling Wt. Total 5.0 lbs. Paper: 0.3 lbs. Wood: 4.7 lbs.

Pre Burn Fuel Wt. 10.952 + 13.668 + 10.632 Total: 35.252 lbs.

Total Kindling and Pre Burn Fuel Wt 40.252 lbs.

Coal Bed Wt-lbs: Range (3.3 - 2.7) 768.1-766.5 lbs. Actual: 3.1 lbs. 766.9

Allowable Amount of Charcoal that can be removed:

Coal Bed Wt. Range  $\left( \frac{3.3}{\text{Upper Wt.}} + \frac{2.7}{\text{Lower Wt.}} / 2 \right) \times .25 = \underline{0.7}$  lbs.

Test Fuel Wt-lbs: Ideal 14.7 lbs. Range: 16.1-13.2 lbs. Actual: 13.306 lbs.

Test Fuel Size (pcs.) (.75 x 1.5 x 5" Flanges) 1314 lbs 16 Pcs.

2 x 4's x 16.0 " 3 Pcs 5.978 lbs. 44.93 %

4 x 4's x 16.0 " 2 Pcs 7.328 lbs. 55.07 %

5.0143 Kg.

Est. Dry Burn Rate (Kg/Hr.)  $\frac{13306 - (13306 \times .1692)}{2.2046} \times \frac{60}{210} = \underline{1.4327}$  Est. Dry Burn Rate (Kg/Hr)

Est EPA Heat Output (HO<sub>E</sub>) (19,140) X  $\frac{63}{100}$  X 1.4327 = 17,275 Est Heat Output (HO<sub>E</sub>) BTU's/Hr

Comments: 160 mins = 1.880  
235 " = 1.280  
240 " = 1.254

Stove Operating Data  
Woodstove Test Data Sheet #9  
Cold Start

Unit: Kuma Ashwood  
Run: EPA 2  
Date: 2/17/09  
Technician(s): AT Muren  
Data Sheet#9-Rev 1/98-Pg.2

Fire Started: 0956

Warm up and Preburn: Primary Air: Wide open from ignition until the start of preburn when the primary air control(s) was (were) adjusted to the run setting of .728" orifice. At the run setting until the start of the test. 2.736" on threaded rod

Secondary Air: No Controls, Naturally drafted

Secondary Burn Bypass: N/A

Charcoal Bed Preparation: Broke up, raked and leveled the coal bed prior to the addition of each warm up/pre burn fuel charge. Starting 1130 before the start of the test, broke up, raked and leveled the coal bed. In stove for 26 seconds.

Test: Door wide open during loading 1 min 02 sec, then closed,

Primary Air: Wide open from the start of the test (0:00) until 4:45. Adjusted to the run setting of .728" between 4:45 and 5:00. At the run setting of .728" at 5:00 into the run.

Secondary Air: No Controls, Naturally drafted.

Secondary Burn Bypass: N/A

Fan: ON/OFF during the warm up, ON/OFF Low during the preburn, ON/OFF at the start of test, ON/OFF for the first 30 minutes of test, ON/OFF Low at 30 minutes into test, ON/OFF for the rest of test.

Test Run Anomalies:

WOODSTOVE OPERATING DATA  
 WOODSTOVE DATA SHEET #9A-1

Wood Data: Kindling: A mix of the below grades

	Size	Mill	Grade	Species
Pre Burn	2X4	Forest Grove	# 2, Std # BTR	D. Fir, Sfc. GRN
Test Fuel	2X4	Forest Grove	# 2, Std # BTR	D. Fir, Sfc, GRN
	4X4	FOREST GROVE	No.1	D. Fir, Sfc, GRN

All grades WCLB Rules unless otherwise noted.

Warm up Information:

1st Warm up/Pre Burn Fuel charge (10.952 lbs) added at 1010.  
 2nd Warm up/Pre Burn Fuel charge (13.668 lbs) added at 1059.  
 3rd Warm up/Pre Burn Fuel charge (10.632 lbs) added at 1209.  
 4th Warm up/Pre Burn Fuel charge (\_\_\_\_\_ lbs) added at \_\_\_\_\_.  
 5th Warm up/Pre Burn Fuel charge (\_\_\_\_\_ lbs) added at \_\_\_\_\_.  
 6th Warm up/Pre Burn Fuel charge (\_\_\_\_\_ lbs) added at \_\_\_\_\_.  
 7th Warm up/Pre Burn Fuel charge (\_\_\_\_\_ lbs) added at \_\_\_\_\_.  
 8th Warm up/Pre Burn Fuel charge (\_\_\_\_\_ lbs) added at \_\_\_\_\_.

1<sup>st</sup> Rick 4-12" 4-16" 2X4's    3<sup>rd</sup> Rick 4-12", 3-16" 2X4's  
 2<sup>nd</sup> Rick 8-16" 2X4's

The coals were scooped out of the stove immediately prior to adding the 3<sup>rd</sup> pre burn/warm up fuel charge. The stove lost 0 lbs. 20 lbs. of coals were put back in the stove after the scoop.

All pre burn/warm up fuel pieces were either 12 or 16 inches long. All preburn pieces/fuel charges were "ricked" in the stove. The pieces in the bottom layer in each rick contained 2 pcs that were 12 or 16 inches long and were loaded flat and perpendicular to the door. The pieces in the second layer in each rick were loaded on their side (edge) approximately parallel to the door and contained 3 or 4 pcs 16 inches long. The third layer (and fourth layer if present) was loaded flat, perpendicular to the door and contained 2 pcs 12 or 16 inches long. The majority of the pieces in each rick were in the second layer which had an approximate 0.5-1.0" space between pieces. (The loading directions indicate the direction of the longest dimension on each piece relative to the loading door opening.) Each pre burn/warm up fuel charge normally weighs within the weight range allowed for the actual test fuel charge

WOODSTOVE OPERATING DATA  
WOODSTOVE DATA SHEET #9A-2

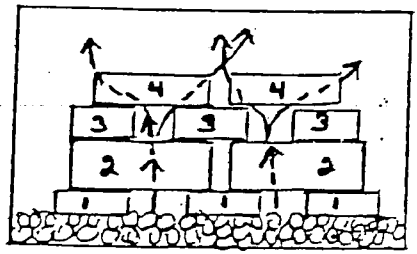
Unit: Kuma Ashwood  
Run # EPA 2  
Date 2/17/04  
Technician ATM  
Page 2 of 4  
WST7-Form2-A, Rev 6/90

Warm up Information (cont.):

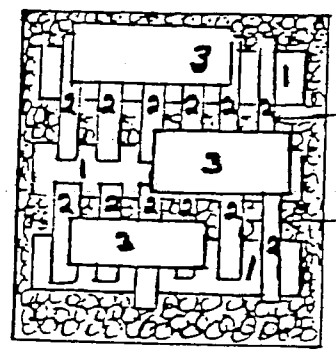
Each warm up/preburn fuel charge was ricked in exactly (as much as possible) the same manner and the weight of each rick was usually within the allowable weight range for the test fuel charge. The physical arrangement and alignment of each rick was designed to accomplish three (3) things: (1) The bottom layer was nestled firmly into the coal bed and was as close to being level with the bottom of the stove as possible, thus providing a stable loading platform for the rest of the rick, keeping it in a ricked state (as opposed to a collapsed or fallen down state) until the rick reached the charcoal stage and sags or collapses of its own accord. (2) It enhances the flow of primary air through the ricked preburn fuel charge, for the primary air would flow through the spaces between the pieces in the first layer and then up through the spaces between the pieces in the second, third and, if present, fourth layers. (3) It maximized, as much as possible, the surface to volume ratio of each preburn fuel charge, thereby allowing the fire immediate access to as much wood surface as possible and, thereby, insuring uniform charcoalization. All three of these enhance combustion and so get the stove as hot as possible during the warm up period, thereby maximizing the amount of heat (BTU's) stored in the stove. The actual preburn was not started until the stove surface temperatures had maximized and stabilized, thus indicating that the amount of heat stored in the stove had peaked. For this stove, the thermal storage was monitored using the Stove Top T/C

944  
1094

surface temperature(s) and the peak value(s) obtained were 1094 OF.



Front View



Top View

The arrows indicate the direction of the air flow through the rick.

The primary air was adjusted to the run setting of 0.728" OPEN 6.0 lbs above the upper charcoal bed weight.

WOODSTOVE OPERATING DATA  
WOODSTOVE DATA SHEET #9A-3

Unit Kuma Ashwood  
Run # EPA 2  
Date 2/17/09  
Technician BTM  
Page 3 of 4  
WST5-Form2-Rev11/89

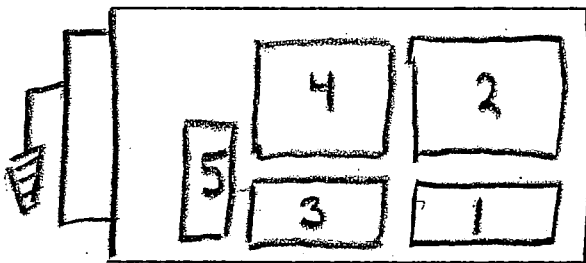
Additional Comments: Test Start Sequence: ① Turned Fan OFF, ② Adjusted Primary Air Control to wide Open, ③ Opened door, ④ Loaded Fuel ⑤ cleared coals away from in front of the LPAO ⑥ closed door,

TOTAL ELAPSED Time: 1102

Photo @ 1140

Test Fuel Charge Loading Information:

Test Fuel Charge and Loading Sequence Diagram



SIDE of stove view

4 X 4's: 2, 4

2 X 4's: 1, 3 & 5

Loading Sequence: 1, 2, 3, 4 & 5 last

Driest Pcs in Load 3, 5

Loaded the test fuel charge on an essentially level, medium sized, average coal bed (in appearance, color and temperature for a Med Hi burn rate. Load 1102 Ignition: 1100

1110 Vertical Column of Flame (VC) up to baffle

1140 Photo taken

1125 2<sup>nd</sup> igniting

2:10 Front Top Edge Pc 4 igniting

3:00 Seconds Full width of 4 - especially on L end

3:25 10.90/1.61 (% CO<sub>2</sub> / % CO) Gas Balance

4:45 - 5:00 Primary Air Control slowly adjusted to the run setting.

5:00 Flames decreased, Maintained a hot pocket of coals under pc 5 with a vertical column of flame (VC) up to baffle. 13.05/1.48 ML/L smoke. The back of the front tube was orange at 5:00.

WOODSTOVE OPERATING DATA  
WOODSTOVE DATA SHEET #9A-4

Additional Comments:

6:15 Secondaries above both Right and left ends of pc 4,  
with more on right end.

7:55 Back of front tube no longer orange, but  
tube is igniting in the center. Secondaries still  
the full width of pc 4.

26:22 Out of Balance - 16. - /1.70. Stackitis from  
pc 5 - pc 5 about burnt thru. Lots of velocity  
in the Secondaries.

30:00 Fan On Low 17.03 / 1.72

30:19 16.93 / 1.62

Unit: Kuma Ashwood  
 Run: EPA 2  
 Date: 2/17/09  
 Technician: JTM JRP PDG  
 WST1-Form7-Rev11/89

FUEL MOISTURE  
 WOODSTOVE TEST DATA SHEET #10

5kg. = 11.024 lbs. 1kg. = 2.204 lbs

Room Temperature: 64.3 °F Correction Factor: 40.5

NOTE: Record readings to the nearest 0.5% moisture  
 Uncor Values are corrected for temperature: Yes  No   
 Time Test Fuel Moisture Readings taken at: 10:45  
 Calibration Checks: X  Y  12.0 11.9 22.0 22.2

Pc #	Dimen	Use	Top		Bottom		Side		Piece Avg Corrected
			Uncor	Cor	Uncor	Cor	Uncor	Cor	
1	30CS	K	7.25	7.575	8.5	8.95	8.25	8.675	8.400
2									
3									
4	2x4-8'	P	21.5	23.1	19.5	20.9	18	19.2	21.067
5			18	19.2	18	19.2	18.5	19.8	19.400
6			18.5	19.8	18.5	19.8	19	20.9	20.167
7			20	21.4	21.5	23.1	20.5	22.0	22.167
8	↓	↓	21.0	22.6	20.0	21.4	20.0	21.4	21.800
9									(104.60)
10	"								
20	2x4-16.0	T	18	19.2	18.5	19.8	18.5	19.8	19.600
2,032			20	21.4	20	21.4	20.5	22.0	21.600
	↓	↓	18	19.2	18.5	19.8	19.5	20.9	19.967
14	"								
3,586	4x4-16.0	T	19.5	20.9	19.5	20.9	19.5	20.9	20.900
3,416	k	k	20.5	22.0	18.5	19.8	16.5	17.5	19.767
17									(101.834)
18									
1,314	SPRINGS	T	18	19.2	18	19.2	19	19.2	19.200
20									(OUT SPRINGS)

	Kindling	Pretest Fuel	Test Load
% Moisture - Dry Basis:	8.400 %	20.9202 %	20.3668 %
% Moisture - Wet Basis:	7.749 %	17.301 %	16.921 %

To obtain Wet from Dry:  $\frac{100 \times \% \text{ Dry Rdg.}}{100 + \% \text{ Dry Rdg.}} = \% \text{ Moisture, Wet Basis}$   
 1 10.952  
 2 13.668  
 3 10.632

Acceptable Ranges: 16-20% wet; 19-25% dry  
 (17.5 - 22.5 on Meter [Uncor reading] at 70°F)

Key for Use: K= Kindling P= Pretest Fuel T= Test Fuel



WOOD DENSITY DETERMINATION  
WOODSTOVE TEST DATA SHEET #11

Unit: Kuma Ash wood  
Run#: EPA 2  
Date: 2/17/09  
Technician: A. J. MYREN  
WST2-form11-Rev 6/90

Wood Piece: 2x4 Nominal Dimensions: 1.5" x 3.5" x 3.5"  
Depth (D): 3.875 cm  
Width (W): 8.860 cm  
Length (L): 8.790 cm  
8.885 cm  
8.520 cm  
8.555 cm  
Length  $\bar{X}$  = 8.6875 cm  
Volume: 298.264 cm<sup>3</sup>  
(D X W X L)

MOISTURE: Room Temperature: 64.3 °F Correction Factor: +0.5  
Uncorrected Meter Readings Corrected for temperature: Yes  No

NOTE: Record moisture meter readings to the nearest 0.5%

	Uncor	Cor	%
Top:	17.5	18.6	%
Bottom:	18.0	19.2	%
Side:	16.5	17.5	%
$\bar{X}$ :		18.433	%

Avg % Moisture (Dry) 18.433 % ✓  
Avg % Moisture (Wet) 15.564 % ✓  
Scale: Levelled In  Out   
Zeroed: In  Out

Wet Weight: 150.8 g Dry Weight: 127.2 g

% Moisture Dried Basis: 15.65 %  
[1 - (Dry Wt ÷ Wet Wt)] X 100

Into Dryer: Date 2/17/09 Time 12:05 Temp 190 °F  
Out of Dryer: Date 3/2/09 Time 09:15 Temp 192 °F  
(Minimum Time in Dryer: 24 hrs.) Minimum Dryer Temp 100°C (212°F)

Density = 127.2 g (dry wt) ÷ 298.264 cm<sup>3</sup> (volume) = 0.4265 g/cm<sup>3</sup>

Pellet Fuel Moisture Content Determination

Tare Beaker Wt. \_\_\_\_\_ g  
Wet Wt: \_\_\_\_\_ g - \_\_\_\_\_ g = \_\_\_\_\_ g  
Gross Wet Wt. Tare Beaker Wt. Net Wet Wt.  
Dry Wt: \_\_\_\_\_ g - \_\_\_\_\_ g = \_\_\_\_\_ g  
Gross Dry Wt. Tare Beaker Wt. Net Dry Wt.

% Moisture Dried Basis: \_\_\_\_\_ %  
[1 - (Net Dry Wt ÷ Net Wet Wt.)] X 100

Pre Burn Test wt.  
610 lbs. up 770.1 lbs.  
Test Start wt. Range  
2671.1 - 7661.5 lbs.

PRE BURN DATA  
RECORD SHEET #13  
WST2-Form 1.6

BAFO'S PRESSURE 1114  
28.22

Unit: Kuma Ashwood Date: 2-17-09  
Run: EPA Technician(s): ATM JRP  
Page: 1 of 1 PPG

Minute	Scale Weight	Burn Rate	Stack	Stove Top	Left Side	Back	Right Side	Bottom	Firebox	2nd Burn	Room Temp	Static	Comments
0	773.1	0	449	906	594	451	588	412	911	1394	81	-064	Primary Air Set at 1.736"
5	772.3	1.8	436	898	587	440	576	411	925	1753	80	-062	Secondary Air Set at 1.736"
10	771.4	1.9	431	869	584	430	570	409	950	1330	81	-062	Fan: On Low
15	770.6	1.8	426	899	585	424	566	405	941	1257	81	-062	TUNNEL ON AT: 1301
20	769.7	1.9	428	914	589	420	562	400	946	1768	81	-062	Buckets ICED ✓
25	769.0	1.7	421	916	594	415	564	396	989	1332	81	-060	ANALYZERS SPANNED ✓
30	768.4	1.6	409	905	603	414	565	391	1005	1379	81	-058	Pumps turned on at:
35	768.0	1.4	383	873	609	416	573	386	1013	1458	82	-050	571.8 AT AT
40	767.8	1.2	343	765	604	426	575	384	1012	1340	83	-050	555.2 - -16.6
45	767.6	1.2	322	724	595	454	575	362	1002	1214	83	-047	Check WB/DB: 54.610 - 9.12
50	767.4	1.2	306	674	585	454	571	361	990	1145	83	-044	533.0 - 13.0
55	767.3	1.1	292	626	572	456	562	360	960	1045	83	-043	519.2 - -13.8
60	767.2	1.1	279	583	557	451	549	361	943	1010	83	-042	Probe IN TUNNEL
65	767.1	1.1	275	582	546	446	542	361	921	990	82	-040	TUNNEL AP 504.2 - 15.0
70	767.0	1.1	269	536	537	440	532	361	899	966	82	-038	495.8 - 6.7
75	766.9	1.1	243	518	526	432	522	361	883	947	82	-036	485.6 - 10
80													475.8 - 9.8
85													
90													
													Stack 475 (480)

Hot Box On ✓







Myren Consulting Inc Data Sheet P4 of 4 Unit Kuma Astwood Date 2/17/09 Run EP1  
 Test En 766.9 AT 475.8 Barometric Pressure 28.73 g Gas Flows @ 1.5" Technician(s) ATM TRP DG

Time	ET	Scale Wt.	Lbs. Left	Burn Rate	CO <sub>2</sub>		O <sub>2</sub>		CO		Gas Bal	Opacity	Notes	Temp #3	Stack Static Press
					v.	%	v.	%	v.	%					
180	1640	767.5	16	0	1280	6.97	13.15	1.56	1.56	4.5		Clear	227	-033	
185	45	767.4	15	1	1292	7.27	12.84	1.58	1.58	4.6		"	224	-032	
190	50	767.3	14	1	1296	7.37	12.78	1.56	1.56	4.7		"	224	-032	
195	55	767.2	13	1	1297	7.39	12.73	1.56	1.56	4.7		"	223	-031	
200	1710	767.1	12	1	1292	7.27	12.89	1.49	1.49	4.9		"	222	-031	
205	05	767.0	11	1	1293	6.80	13.35	1.50	1.50	4.5		"	221	-030	
210	10	766.9	0	1	1253	6.31	13.77	1.65	1.65	3.8		✓	220	-030	
215															
220															
225															
230															
235															
Total															

Total  
 AVG ÷ 43

Time	ET	Top #4	Left #5	Back #6	Right #7	Bottom #8	Firebox #9	2nd burn #10	Amb. #11	Thl #12	C Gas #13	C Gas Imppr #14	Part. Filt #15	Part. Cond. #16	Center Secondary
185	45	421	468	436	453	322	753	849	61	95	220	38	63	38	692
190	50	416	466	434	450	322	749	847	60	95	222	36	63	39	696
195	55	415	463	436	448	321	744	846	60	95	223	36	63	39	902
200	1700	412	460	437	446	321	741	855	60	95	223	38	63	38	912
205	05	410	457	440	445	320	731	829	60	95	223	38	63	39	862
210	10	407	453	436	443	319	721	817	60	95	223	38	63	39	846
215															
220															
225															
230															
235															
Total															

Dullin  
 SHIRT 475.8  
 SHOES 412.0  
 AOT -63.8

Total  
 AVG ÷ 43

47.4  
 420.0-55  
 414.6-5  
 414.4-4  
 412.0  
 -6

PRE AND POST TEST ZERO/SPAN CHECK  
WOODSTOVE DATA SHEET #15-1

Colville

Site: Myren Consulting, [REDACTED], WA Date: 2/17/09 Analyte: CO<sub>2</sub>

Source: Kuma Ashwood Run #: EPA 2

Zero Cyl #: TC 30AM154 Conc. 00.0 % CO<sub>2</sub> Cyl Press: 1540 psi

Certified by: Oxarc Date: 11/12/07

Span Cyl #: AS90457 Conc. 12.5 % CO<sub>2</sub> Cyl Press: 1475 psi

Certified by: Matheson Tri Gas Date: 2/2/2009

Analyzer: Make: Horiba Model: PIR-2000 SN: 607024

Range: 0 - 25.0% CO<sub>2</sub> Analyzer Output: 0 - 1.0 v.

Flow: 1.5 SCFH Measured by: Rotameter: X Flowmeter:     

EPA Span Value = 25.0% CO<sub>2</sub>  
EPA Control Limits = + 2.5% of 25.0% CO<sub>2</sub> = + 0.625% CO<sub>2</sub>

Pre Run Audit: By: A.A. Myren Time: 1255 Temp: 80 °F

Audit Results

Point #	Expected Response			Actual Response			+ Conc. Difference	Δ %
	Meter	DVM	%	Meter	DVM	%		
Zero	00.0	.000	00.0	00.0	.001	.07925	+0.07925	+0.32
Span	50.0	.500	12.5	49.75	.499	12.3858	-0.1142	-0.91

Comments:

Post Run Audit: By: A.A. Myren Time: 1755 Temp: 84 °F

Audit Results

Point #	Expected Response			Actual Response			+ Conc. Difference	Δ %
	Meter	DVM	%	Meter	DVM	%		
Zero	00.0	.000	00.0	00.0	.001	.07925	+0.07925	+0.32
Span	50.0	.500	12.5	49.75	.501	12.4352	-0.06482	-0.52

Comments:

+ Conc. Difference = Act % - Exp (Std) %  
 Zero % Differece =  $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Full Scale Value}} \times 100$   
 Span % Difference =  $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Exp \% (ppm)}} \times 100$

PRE AND POST TEST ZERO/SPAN CHECK  
WOODSTOVE DATA SHEET #15-3

colville

Site: Myren Consulting, Woodville, WA Date: 2/17/09 Analyte: CO

Source: Kuma Ashwood Run #: EPA 2

Zero Cyl #: TC3AAM154 Conc. 00.0 % CO Cyl Press: 1540 psi

Certified by: Oxarc Date: 11/12/07

Span Cyl #: AS90457 Conc. 2.00 % CO Cyl Press: 1475 psi

Certified by: Matheson Tri Gas Date: 2/2/09

Analyzer: Make: HORIBA Model: MEXA 311GE SN: GE-30025

Range: 0 - 10.0% CO Analyzer Output: 0 - 1.0 V

Flow: 1.5 SCFH Measured by: Rotameter:  Flowmeter:

EPA Span Value = 5.0% CO

EPA Control Limits = +2.5% of 5.0% CO = + 0.125% CO

Pre Run Audit: By: A.P. Myren Time: 1255 Temp: 80 °F

Audit Results

Point #	Expected Response			Actual Response			+ Conc. Difference	Δ %
	Meter	DVM	%	Meter	DVM	%		
Zero	00.0	00.0	00.0	00.0	.001	.00563	+0.00563	+0.06
Span	2.00	1.99	2.00	1.99	.199	1.9959	-0.00411	-0.21

Comments:

Post Run Audit: By: A.P. Myren Time: 1755 Temp.: 84 °F

Audit Results

Point #	Expected Response			Actual Response			+ Conc. Difference	Δ %
	Meter	DVM	%	Meter	DVM	%		
Zero	00.0	00.0	00.0	00.0	.001	.00563	+0.0563	+0.06
Span	2.00	1.98	2.00	1.98	.198	1.9858	-0.01416	-0.71

Comments:

Conc. Difference = Act % - Exp (Std) %  
 Zero % Difference =  $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Full Scale Value}} \times 100$   
 Span % Difference =  $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Exp \% (ppm)}} \times 100$



Unit: Kuma Ashwood  
 Run: EP02  
 Date: 2/17/09  
 Technicians: ATM JRP PDG  
 WST6-Form3-Rev11/89

QUALITY CHECKS  
 WOODSTOVE DATA SHEET #16

Ambient = T/C #30: \_\_\_\_\_ °F

Thermocouple Check (at ambient): T/C #1: \_\_\_\_\_ °F; T/C #2: 70.8 °F;

T/C #3: 71.1 °F; T/C #4: 70.4 °F; T/C #5: 71.3 °F;

T/C #6: 69.2 °F; T/C #7: 70.2 °F; T/C #8: 73.4 °F;

T/C #9: 71.6 °F; T/C #10: 77.8 °F; T/C #11: 64.3 °F;

T/C #12: 69.7 °F; T/C #13: 67.6 °F; T/C #14: 61.4 °F;

T/C #15: 67.0 °F; T/C #16: 53.3 °F; T/C #17: 76.6 °F;

T/C #18: \_\_\_\_\_ °F; T/C #19: \_\_\_\_\_ °F; T/C #20: \_\_\_\_\_ °F;

T/C #21: \_\_\_\_\_ °F; T/C #22: \_\_\_\_\_ °F; T/C #23: \_\_\_\_\_ °F;

T/C #24: \_\_\_\_\_ °F; T/C #25: \_\_\_\_\_ °F; T/C #26: \_\_\_\_\_ °F;

Comments: \_\_\_\_\_

Thermocouple Readout: Pretest Zero/Span Check and Calibration:

Zero (0°F)	: <u>0.5</u> °F	Adj to: _____ °F	Post Test Check Zero (0°F):	<u>0.2</u> °F	% Difference: <u>+0.04</u>
Span (2000°F)	: <u>2000.7</u> °F	Adj to: _____ °F	Span (2000°F):	<u>2002.7</u> °F	<u>+0.11</u>

(Allowable % Difference = 1.5%. Use formulas on Woodstove Data Sheet #15 to calculate % Difference) **In Degrees Absolute.**

Thermocouple Readout Pretest Linearity Check

0°F = <u>-0.2</u> °F;	200°F = <u>201.6</u> °F;	400°F = <u>399.0</u> °F;
600°F = <u>601.3</u> °F;	800°F = <u>801.6</u> °F;	1000°F = <u>1000.8</u> °F;
1200°F = <u>1198.6</u> °F;	1400°F = <u>1399.6</u> °F;	1600°F = <u>1600.2</u> °F
1800°F = <u>1800.5</u> °F;	2000°F = <u>2000.7</u> °F	

Combustion Gas (CO<sub>2</sub>, O<sub>2</sub>, CO) Train Leak Check: Pre OK Post OK

Draft (Static) Gauge Zero Check: Pre OK Post OK

Scale Check Pre (Wt. #'s): 763.3 - 763.3 lbs = 5.0 lbs / 5.0 lbs = OK (ATM)

Post (Wt. #'s): 771.6 - 766.6 lbs = 5.0 lbs / 5.0 lbs = OK (PDG)

stack cleaned prior to the run: Yes \_\_\_\_\_ No ✓

Tunnel cleaned prior to the run: Yes \_\_\_\_\_ No ✓

DILUTION TUNNEL CALCULATIONS

1/25/09, Md=28.56, Bws=4%

6" Tunnel

EPA 1

File Name:

Manufacturer:

Model Number:

Lab Name:

Test Date:

Run Number:

Meter Box Y Factor:

Barometric pressure (in):

Gas meter temp (ave):

delta H(ave):

Gas meter initial reading:

Gas meter final reading:

Front catch (acetone) mg:

first filter catch (mg):

second filter catch (mg):

Tunnel Flow (Qsd) (dscfm)

Emission Rate(g/hr):

Emission Rate(M5H):

Avg. of Delta P Sq. Roots:

Vs (Avg.)(ft/min):

Tunnel Avg. Temperature (F):

Test time(min):

Fuel Load(lb. wet):

Wood moisture(%wet):

Burn rate(dry kg/hr):

Sample Volume (dscf)

Avg. Tunnel Static (-inch H2O):

Room Blank Catch (mg/dscf):

Emission Factor (g/kg):

Pitot Correction Factor:

front filter number

back filter number

Beaker Number:

PRELIMINARY RESULTS

FINAL RESULTS:

DATA SUMMARY

MODEL:

RUN:

DATE:

DBR:

EMISSION RATE (g/hr)(M5H)

EMISSION FACTOR (g/kg):

AVG. % PROPORTIONALITY:

MYREN CONSULTING CERTIFICATION TEST DATA

Run Time (min)	Pitot Delta P (-inch H2O)	TNL Temp (°F)	Gas Meter RDG (ft3)	Gas Meter Temp (°F)	Gas Meter Delta H (in.H2O)	Tunnel Velocity (ft/min)	PROP RATE (%)	dDGM vol std (ft3)	Tunnel Static (-inch H2O)	SQUARE ROOT DELTA P	DRY GAS METER RDG (m3)
0	0.046	126	977.0000	72	0.900	930.03			0.195	0.2145	
10	0.046	145	982.3220	75	0.900	944.98	100.7	5.039	0.190	0.2145	
20	0.045	152	987.6200	78	0.900	940.05	100.8	4.989	0.193	0.2121	
30	0.046	151	992.9500	82	0.900	949.66	98.8	4.982	0.194	0.2145	
40	0.047	143	998.2560	85	0.900	953.62	95.6	4.934	0.191	0.2168	
50	0.047	137	1003.5600	87	0.900	948.87	94.3	4.910	0.193	0.2168	
60	0.048	133	1008.8900	89	0.900	955.69	92.8	4.918	0.193	0.2191	
70	0.045	133	1014.2480	90	0.900	925.34	96.0	4.935	0.190	0.2121	
80	0.045	129	1019.6180	91	0.900	922.22	95.6	4.937	0.192	0.2121	
90	0.045	124	1025.0030	91	0.900	918.30	95.4	4.951	0.193	0.2121	
100	0.045	121	1030.3950	92	0.900	915.93	95.0	4.948	0.191	0.2121	
110	0.046	117	1035.7840	92	0.900	922.86	93.6	4.946	0.194	0.2145	
120	0.045	113	1041.1070	92	0.900	909.60	93.1	4.885	0.188	0.2121	
128	0.045	110	1045.5140	92	0.900	907.21	96.1	4.045	0.186	0.2121	
150			0.0000		0.900	0.00	0.0	0.000		0.0000	
160			0.0000		0.900	0.00	0.0	0.000		0.0000	
170			0.0000		0.900	0.00	0.0	0.000		0.0000	
180			0.0000		0.900	0.00	0.0	0.000		0.0000	
190			0.0000		0.900	0.00	0.0	0.000		0.0000	
200			0.0000		0.900	0.00	0.0	0.000		0.0000	
210			0.0000		0.900	0.00	0.0	0.000		0.0000	
220			0.0000		0.900	0.00	0.0	0.000		0.0000	
230			0.0000		0.900	0.00	0.0	0.000		0.0000	
240			0.0000		0.900	0.00	0.0	0.000		0.0000	
250			0.0000		0.900	0.00	0.0	0.000		0.0000	
260			0.0000		0.900	0.00	0.0	0.000		0.0000	
270			0.0000		0.900	0.00	0.0	0.000		0.0000	
280			0.0000		0.900	0.00	0.0	0.000		0.0000	
290			0.0000		0.900	0.00	0.0	0.000		0.0000	
300			0.0000		0.900	0.00	0.0	0.000		0.0000	
310			0.0000		0.900	0.00	0.0	0.000		0.0000	
320			0.0000		0.900	0.00	0.0	0.000		0.0000	
330			0.0000		0.900	0.00	0.0	0.000		0.0000	
340			0.0000		0.900	0.00	0.0	0.000		0.0000	
350			0.0000		0.900	0.00	0.0	0.000		0.0000	
360			0.0000		0.900	0.00	0.0	0.000		0.0000	
370			0.0000		0.900	0.00	0.0	0.000		0.0000	
380			0.0000		0.900	0.00	0.0	0.000		0.0000	

141.996

3.178

4.752

0.2143

896.795

131.000

128

13.210

16.976

2.332

63.536

0.1916

0

1.3628

0.9611

706

705

21

AUDITED

ASHWOOD

EPA 1

2/16/09

2.332

4.7518

1.3628

95.983

METHOD 5G-1 (EPA) PARTICULATE SAMPLING DATA

Rev. 2/09

DATE: 2/16/09 PAGE 1 OF 1 UNIT: KUMA Ashwood RUN: EPA 1

METER BOX: 45G-P METER Y: 1.0177 FILTER #'S: (F) 706 (R) 705

.8901 .892  
PRE TEST LEAK CHECK: 1002 CFM @ -16.1 IN HG FILTER SIZE: 110 mm

1.578/1.579  
POST TEST LEAK CHECK: 1001 CFM @ -16.1 IN HG PROBE LENGTH 21.5 IN

Pitot P <sub>g</sub>	TIME		METER READING	PITOT	TUNNEL TEMP	METER TEMP	DRY GAS METER	VAC
	CLOCK	ELAPSED	(FT <sup>3</sup> )	ΔP	(°F)	(°F)	Δh	(in Hg)
-195	1655	00	977.000	.046	126	72	0.90	0
-190	1705	10	982.322	.046	145	75	.90	0
-193	15	20	987.620	.045	152	78	.90	0
-194	25	30	992.950	.046	151	82	.90	0
-191	35	40	998.258	.047	143	85	.90	0
-193	45	50	1003.560	.047	137	87	.90	0
-193	55	60	1008.890	.048	133	89	.90	0
-190	1805	70	1014.248	.045	133	90	.90	0
-192	15	80	1019.618	.045	129	91	.90	0
-193	25	90	1025.003	.045	124	91	.90	0
-191	35	100	1030.395	.045	121	92	.90	0
-194	45	120	1035.724	.046	117	92	.90	0
-188	55	130	1041.107	.045	113	92	.90	0
-186	1903	128	1045.514	.045	110	92	.90	0
		50						
		60						
		70						
		80						
		90						

Pre Test Filter Check Weigh  
F .6944  
R .6835

End of Test Weight  
F .7139 R .6818  
.6948 .6837  
.0191 0

BP: 00 28.16  
60 28.15  
120 28.15

X = 28.153 Hg

MYREN CONSULTING, INC.

Dilution Tunnel Traverse Data with 8 Traverse Points

Unit: KUMA Ashwood

Run #: EPA 1

Date: 2/16/09

Technicians: ATM GRP POG

#12 Rev 4/2/08

T<sub>cent</sub> Pg

T<sub>trav</sub>

Δp<sub>cent</sub>

Δp

√Δp<sub>trav</sub>

Point Location

W-1	0.5'	<u>043</u>	<u>2074</u>	<u>155</u>	<u>157</u>
2	1.5'	<u>048</u>	<u>2191</u>	<u>156</u>	<u>152</u>
Center		<u>051</u>	<u>2258</u>	<u>150</u>	<u>150</u>
3	4.5	<u>053</u>	<u>2302</u>	<u>150</u>	<u>150</u>
4	5.5	<u>047</u>	<u>2098</u>	<u>149</u>	<u>148</u>
S-1	0.5	<u>047</u>	<u>2098</u>	<u>150</u>	<u>150</u>
2	1.5	<u>050</u>	<u>2236</u>	<u>150</u>	<u>150</u>
Center		<u>052</u>	<u>2200</u>	<u>150</u>	<u>150</u>
3	4.5	<u>052</u>	<u>2280</u>	<u>153</u>	<u>153</u>
4	5.5	<u>050</u>	<u>2236</u>	<u>153</u>	<u>153</u>
Totals			<u>1,9466</u>	<u>1214</u>	<u>306</u>
Average			<u>2183</u>	<u>151.75</u>	<u>214</u>

°R = (°F + 460)

Ps = BP + (-Pg/13.6) = 28.16 + (214/13.6) = 28.144

LEAK CHECKS:

Pre Test: Pg Leg: ✓ POG Velocity Head Leg: ✓ POG

Post Test: Pg Leg: OK ATM Velocity Head Leg: OK ATM

Rev 4/19/08

DILUTION TUNNEL GAS VELOCITY & VOLUMETRIC FLOW RATE CALCULATIONS

UNIT: KUMA Ashwood DATE: 2/16/09 RUN #: EPA 1 TECHNICIAN(S): ATM  
JRP

Average Gas Velocity in the Dilution Tunnel  $V_{strav}$  (EPA M2 EQN 2-9, ASTM E 2515-07 EQN 7)

$$(9) V_{strav} = (85.49) (0.99 \text{ cp}) (\frac{2.183}{\Delta P \text{ "H}_2\text{O}}) \sqrt{\frac{611.75 \text{ Ts } ^\circ\text{A}}{(10)}} = \underline{16.1183} \text{ fps}$$

$$(9A) V_s = (\frac{16.1183 \text{ fps}}{(2)}) (60) = \underline{967.098} \text{ fpm}$$

Gas Velocity in the Center of the Dilution Tunnel -  $V_{scent}$  (EPA M2 EQN 2-9, ASTM E 2515-07 EQN 7)

$$(9) V_{scent} = (85.49) (0.99 \text{ cp}) (\frac{2.269}{\Delta P \text{ "H}_2\text{O}}) \sqrt{\frac{613 \text{ Ts } ^\circ\text{A}}{(10)}} = \underline{16.7704} \text{ fps}$$

$$(9A) V_s = (\frac{16.7704 \text{ fps}}{(2)}) (60) = \underline{1006.224} \text{ fpm}$$

EPA M5G1 Section 4.2.2, ASTM E 2515-07 EQN 1 Adjustment Factor for Center of Tunnel Pitot Tube Location

$$F_p = V_{strav} / V_{scent} = \underline{16.1183} \div \underline{16.7704} = \underline{0.9611}$$

Average Stack Gas Dry Volumetric Flow Rate -  $Q_{sd}$  (EPA M2 EQN 2-10, ASTM E 2515-07 EQN 3)

$$(10) Q_{sd} = 3600 (1 - 0.04 \text{ Bws}) (\frac{16.1183 \text{ fps}}{(2)}) [(528 \text{ } ^\circ\text{A}) (\frac{28.144 \text{ Ps "Hg}}{(2)}) \text{ "Hg}] / (\frac{611.75 \text{ T}_s \text{ } ^\circ\text{A}}{(10)}) = \underline{8877.638} \text{ dscfh}$$

$$\underline{8877.638} \text{ dscfh (or dscfm)}$$

$$(10A) \underline{8877.638} \text{ dscfh} \div 60 = \underline{147.961} \text{ dscfm (or dscfm)}$$

Note: Number in { } under blank lines denotes number of decimals to be used. If a blank calls for an answer already calculated, use the number of decimals previously specified for that answer.

WOODSTOVE DATA SHEET #4-1: INITIAL FILTER WEIGHTS (TARE WEIGHTS)

Into Dessicator: Date 1-27-09 Time 1149 By PDG Front Half X Back Half X  
 Manufacturer: Pall P/N 60115 Size: 110 Lot.No.: 70726 Grade: A/E Glass

Filter #	First Wt	2009 Date	Time	By	Second Wt	Date	Time	By	Third Wt	2009 Date	Time	By
700	.6873	1-22	1331	GRP	.6877	1-23	1417	PDG				
701	.6871		1330	GRP	.6878		1419	PDG	.6877	1-26	1421	GRP
702	.6816		1329	GRP	.6825		1420	PDG	.6824	1-26	1420	GRP
703	.6761		1328	GRP	.6762		1421	PDG				
704	.6727		1327	GRP	.6732		1422	PDG				
705	.6833		1326	GRP	.6837		1423	PDG	←			
706	.6946		1325	GRP	.6948		1424	PDG	←			
707	.6773		1324	GRP	.6777		1425	PDG				
708	.6701		1323	GRP	.6702		1426	PDG				
709	.6799		1322	GRP	.6809		1427	PDG	.6806	1-26	1419	GRP
710	.6587		1321	GRP	.6590		1428	PDG				
711	.6654		1320	GRP	.6656		1429	PDG				
712	.6678		1319	GRP	.6692		1430	PDG				
713	.6864		1318	GRP	.6866		1431	PDG				
714	.6651		1318	GRP	.6655		1432	PDG				
715	.6741		1317	GRP	.6744		1433	PDG				
716	.6592		1316	GRP	.6590		1434	PDG				
717	.6531		1315	GRP	.6536		1435	PDG				
718	.6621		1314	GRP	.6623		1436	PDG				
719	.6769		1313	GRP	.6769		1437	PDG				
720	.6627		1312	GRP	.6628		1438	PDG				
721	.6567		1311	GRP	.6569		1439	PDG				
722	.6539		1310	GRP	.65340		1440	PDG				
723	.6552		1309	GRP	.6552		1441	PDG				
724	.6655		1308	GRP	.6656		1442	PDG				

Checked by A.T. Meyer Date: 1/27/09 Time 1632

QA REWEIGH

Filter #	WT	Date	Time	By
703	.6761	1/27/09	1639	AM
708	.6705		1640	AM
715	.6749	✓	1642	AM

BALANCE ROOM ENVIRONMENTAL CONDITIONS

WB	DB	%RH	Date	Time	By
57	72	38	1-22-09	1138	AM
58	75	33	1-23-09	1150	PDG
56	76	25	1-26-09	1359	GRP

50 72 31 1/27/09 1530 PDG

Post 1-22 1123 1-26  
 0.0000 0.0000 0.0000 0.0000  
 100.0000 99.9994 99.9993 99.9993

WOODSTOVE DATA SHEET #4-2:  
INITIAL BEAKER WEIGHTS (TARE WEIGHTS)

Into Dessicator: Date: 01.26.09 Time: 15:38 By: JRP

Beaker #	First Wt.	2009 Date	Time	By	Second Wt.	2009 Date	Time	By	Third Wt.	Date	Time	By
20	73.3181	1/27	1532	PDG	73.3176	1-29	1459	JRP		1/30		
21	71.0021		1534	PDG	71.0018		1458	JRP	←			
22	71.8343		1535	PDG	71.8338		1457	JRP				
23	70.7390		1536	PDG	70.7389		1455	JRP				
27	72.3310		1538	PDG	72.3307		1500	JRP				
31	69.6672		1539	PDG	69.6669		1501	JRP				
32	53.6002		1541	PDG	53.5993		1502	JRP	53.5998		1505	PDG
37	53.7267		1542	PDG	53.7262		1504	JRP				
38	53.2525		1544	PDG	53.2516		1505	JRP	53.2520		1308	PDG
39	53.1509		1545	PDG	53.1493		1506	JRP	53.1496		1311	PDG
40	53.4626		1547	PDG	53.4622		1507	JRP				
41	52.8371		1549	PDG	52.8367		1508	JRP				
42	53.8699		1550	PDG	53.8692		1509	JRP	53.8696		1302	PDG

Checked By: APM Date: 2/1/09 Time: 12:10

QA REWEIGH

Beaker #	WT	Date	Time	By
20	73.3181	2/1/09	1245	APM
31	69.6671		1217	APM
42	53.8699	X	1219	APM

BALANCE ROOM ENVIRONMENTAL CONDITIONS

WB	DB	%RH	2009 Date	Time	By
55	72	31	1/27	1530	PDG
58	77	29	1-29	1436	JRP
60	72	49	1/30	1256	PDG

1/27 0.0000 09.0000  
1-29 0.0000 09.0000  
1/30 0.0000 09.0000  
2/1 0.0000 09.0000

58 74 37 2/1 1200 APM

WOODSTOVE DATA SHEET #4-2:  
INITIAL BEAKER WEIGHTS (TARE WEIGHTS)

Blank done 12/9/07

Into Dessicator: Date: 10/12/07 Time: 0801 By: GRP

Beaker #	First Wt	Date	Time	By	Second Wt	Date	Time	By	Third Wt	Date	Time	By
25	71.8343	10/22/07	1358	GRP	71.8332	11/10/07	1938		71.8330	11-11-07	1748	Jm
26	73.2192		1400	GRP	73.2190	11/10/07	1940		73.2193	11-11-07	1746	Jm
25	72.6516		1401	GRP	72.6512	11/10/07	1944		← Blank			
26	71.7895		1403	GRP	71.7888	11/10/07	1939		71.7886	11-11-07	1747	Jm
27	72.3316		1402	GRP	72.3314	11/10/07	1945					
28	70.5979		1404	GRP	70.5975	11/10/07	1941		70.5977	11-11-07	1745	Jm
39	53.1508		1405	GRP	53.1500	11/10/07	1942					
37	53.7237	11/10/07	1945	MM	53.7238	11/11/07	1743	Jm				

Checked By: \_\_\_\_\_ Date: \_\_\_\_\_ Time: \_\_\_\_\_

QA REWEIGH

Beaker #	WT	Date	Time	By
27	72.3315	11-11	1740	Jm
25	72.6515	11-11	1741	Jm
39	53.1509	11-11	1744	Jm

BALANCE ROOM ENVIRONMENTAL CONDITIONS

WB	DB	%RH	Date	Time	By
57	68	50	10/22/07	1344	GRP
			11/10		

Post weighing  
0.0000g  
0.0000g  
0.0000g

1st  
0.0000  
0.0000g

2nd



WOODSTOVE DATA SHEET #4-3: CONSTANT FINAL WEIGHTS

FINAL BEAKER WEIGHTS

Beaker #	Into Dessic	Date	Time	By	First	Date	Time	By	Second	Date	Time	By	Third	Date	Time	By
21	✓	2-19	1312	SRP	71.0114	2/20	1027	PDG	71.0107	2/21	1530	ATM	71.0105	2/22	1230	Jm
					Power#	2/23	1415	PDG	71.0096	2/24	1003	ATM				

55 ml

FINAL FILTER WEIGHTS

Filter #	Into Dessic	Date	Time	By	First	2009 Date	Time	By	Second	Date	Time	By	Third	Date	Time	By
F 706		2/16	1920	ATM	71.33	2-17	1456	SRP	71.80	2/18	1818	ATM				
R 705		2/16	1920	ATM	68.14	2-17	1454	SRP	68.14	2/18	1819	ATM				

QA REWEIGH: FINAL WEIGHTS

Date	Beaker #	Final Wt	By
Date	Filter #	Final WT	By

SCALE ROOM ENVIRONMENTAL CONDITIONS

Weighing Session	Date	Time	By	WB	DB	%RH
2009						
1	2-17	1439	SRP	56	72	35
2	2/18	1800	ATM	55	70	36
3	2/20	1019	PDG	57	74	33
4	2/22	1822	ATM	47	59	37
5	2/23	1406	PDG	58	70	46

SCALE ROOM ENVIRONMENTAL CONDITIONS

6	2/24	0923	ATM	59	76	35
7						
8						
9						
Comments						

Acezone  
lot #  
041648

Blank  
done  
12-10/07

WST5-Form9, Pg 1, Rev 4/90  
Unit: KAMA OSHWOOD  
Run # EPA  
Date: 2/16/09

WOODSTOVE DATA SHEET #4-3: CONSTANT FINAL WEIGHTS

FINAL MAKER WEIGHTS

Beaker #	Into Dessic	2007 Date	Time	By	First	Date	Time	By	Second	Date	Time	By	Third	Date	Time	By
25	✓	12/12	1546	APP	72.6508	12/13	1342	APP	72.6511	12/14	1347	Qu				

FINAL FILTER WEIGHTS

Filter #	Into Dessic	Date	Time	By	First	Date	Time	By	Second	Date	Time	By	Third	Date	Time	By

QA REWEIGH: FINAL WEIGHTS

Date	Beaker #	Final Wt	By
Date	Filter #	Final WT	By

SCALE ROOM ENVIRONMENTAL CONDITIONS

Session	Date	Time	By	WB	DB	ZRH
1	12/13	1207	JRP	55	73	29
2	12/14	1324	JRP	57	75	31
3						
4						

SCALE ROOM ENVIRONMENTAL CONDITIONS

6						
7						
8						
9						
Comments						

WOODSTOVE DATA SHEET 4-4 SCALE QC RECORD SHEET

SCALE: SARTORIUS  
 MODEL: CP224S  
 SN: 17050374

FROM: 9/27/2007  
 THROUGH: 12/7/2007

Level	Recali	130 g	100 g	10 g	1.0 g	100 mg	20 mg	Date	Time	Tech	Wet Bulb	Dry Bulb	% RH
✓	N	129.9998	99.9997	10.0000	1.0000	0.1000	0.0199	9/27/07	1402	GRP	55	67	45
✓	Y	129.9995	99.9996	10.0001	1.0000	0.1000	0.0200	9/28/07	1335	GRP	57	69	46
✓	Y	129.9996	99.9996	9.9999	1.0000	0.1000	0.0200	10/1/07	1505	ATM	56	70	43
✓	N	129.9995	99.9996	10.0000	1.0000	0.1000	0.0199	10/2/07	1611	GRP	56	68	46
✓	N	129.9997	99.9997	9.9999	1.0000	0.1000	0.0199	10/3/07	1122	GRP	56	68	46
✓	N	129.9996	99.9996	10.0000	1.0000	0.1000	0.0199	10/4/07	1225	GRP	55	67	45
✓	Y	129.9996	99.9996	10.0000	1.0000	0.1000	0.0199	10/5/07	0750	GRP	51	62	45
✓	N	129.9997	99.9997	9.9999	1.0000	0.1000	0.0199	10/5/07	1513	GRP	56	69	43
✓	Y	129.9996	99.9996	10.0000	1.0000	0.1000	0.0200	10/9/07	1505	ATM	58	71	44
✓	N	129.9996	99.9997	10.0000	1.0000	0.1000	0.0200	10/12/07	1259	ATM	58	70	48
✓	Y	129.9995	99.9996	9.9999	1.0000	0.1000	0.0199	10/22/07	1344	GRP	57	68	50
✓	Y	129.9996	99.9997	9.9999	1.0000	0.1000	0.0199	10/29/07	1338	GRP	53	63	50
✓	N	129.9995	99.9995	10.0000	1.0000	0.1000	0.0200	10/30/07	0933	ATM	56	70	40
✓	Y	129.9996	99.9997	10.0000	1.0000	0.1000	0.0199	11/26/07	1457	GRP	55	70	36
✓	Y	129.9996	99.9996	9.9999	1.0000	0.1000	0.0199	10/31/07	1528	GRP	57	75	30
✓	Y	129.9996	99.9996	9.9999	1.0000	0.0999	0.0199	11/2/07	1235	GRP	50	67	33
✓	Y	129.9996	99.9996	10.0000	1.0000	0.1000	0.0199	11/5/07	0730	GRP	57	73	35
✓	N	129.9996	99.9997	10.0000	1.0000	0.1000	0.0200	11/9/07	1550	ATM	58	70	48
✓	Y	129.9997	99.9997	10.0000	1.0000	0.1000	0.0200	11/10/07	1865	ATM	58	71	44
✓	N	129.9997	99.9997	9.9999	1.0000	0.1000	0.0199	11/11/07	1910	ATM	55	69	39
✓	N	129.9996	99.9996	10.0000	1.0000	0.1000	0.0199	11/21/07	0822	GRP	54	67	41
✓	N	129.9998	99.9997	9.9999	1.0000	0.1000	0.0199	11/21/07	1226	ATM	58	72	41
✓	N	129.9998	99.9997	9.9999	0.9999	0.1000	0.0200	11/14/07	1710	GRP	58	73	39
✓		QC Services Audit	11/17/07										
✓	Y	129.9997	99.9997	10.0000	1.0000	0.1000	0.0200	11/15/07	1350	ATM	59	72	45
✓	N	129.9996	99.9996	9.9999	0.9999	0.1000	0.0200	11/16/07	1600	GRP	58	71	41
✓	N	129.9996	99.9996	10.0000	1.0000	0.1000	0.0199	11/19/07	1758	ATM	740	74	43
✓	Y	129.9995	99.9996	10.0000	1.0000	0.1000	0.0200	11/19/07	1143	ATM	56	70	40
✓	Y	129.9995	99.9996	10.0000	1.0000	0.1000	0.0199	11/20/07	1416	GRP	54	69	35
✓	N	129.9996	99.9996	10.0000	1.0000	0.1000	0.0200	11/27/07	1110	ATM	57	70	44
✓	N	129.9995	99.9996	10.0000	1.0000	0.1000	0.0199	12/3/07	0730	GRP	55	69	40
✓	N	129.9996	99.9996	10.0000	1.0000	0.0999	0.0200	12/16/07	1125	ATM	54	67	44
✓	Y	129.9996	99.9996	10.0000	1.0000	0.1000	0.0200	12/17/07	1348	GRP	55	69	40

SCALE: SARTORIUS  
 MODEL: CP224S  
 SN: 17050374

WOODSTOVE DATA SHEET 4-4 SCALE QC RECORD SHEET

FROM: 12/8/07  
 THROUGH: 2/3/08

Level	Recali	130 g			100 g			10 g			1.0 g			20 mg			Wet		Dry		% RH
		brated	Weights	Weight	Weight	Weight	Weight	Weight	Weight	Weight	Weight	Weight	Weight	Weight	Weight	Time	Tech	Bulb	Bulb		
✓	N	129.9996	99.9996	99.9996	10.0000	1.0000	0.1000	0.0200	12/8	12/5	ATM	57	73	35							
✓	N	129.9996	99.9996	99.9996	10.0000	1.0000	0.1000	0.0200	12/8	19/10	ATM	57	72	38							
✓	N	129.9997	99.9996	99.9996	10.0000	1.0000	0.1000	0.0199	12/9	19/35	ATM	55	72	31							
✓	Y	129.9996	99.9996	99.9996	10.0000	1.0000	0.1000	0.0200	12/10	19/53	ATM	56	72	34							
✓	N	129.9997	99.9997	99.9997	10.0000	1.0000	0.1000	0.0199	12/11	16/18	GRP	57	76	28							
✓	N	129.9997	99.9996	99.9996	10.0000	1.0000	0.1000	0.0199	12/12	5/05	GRP	56	74	30							
✓	N	129.9996	99.9996	99.9996	10.0000	1.0000	0.1000	0.0199	12/13	3/07	GRP	55	73	29							
✓	N	129.9996	99.9996	99.9996	10.0000	1.0000	0.1000	0.0199	12/14	13/21	GRP	57	75	31							
✓	N	129.9996	99.9996	99.9996	10.0000	1.0000	0.1000	0.0199	12/15	16/02	GRP	57	75	31							
✓	N	129.9998	99.9998	99.9998	10.0000	1.0000	0.1000	0.0199	12/17	08/17	GRP	55	73	29							
✓	Y	129.9996	99.9997	99.9997	10.0000	1.0000	0.1000	0.0199	12/18	08/53	GRP	58	75	34							
✓	N	129.9997	99.9997	99.9997	10.0000	1.0000	0.1000	0.0199	12/19	08/12	GRP	55	72	31							
✓	N	129.9997	99.9997	99.9997	10.0000	1.0000	0.1000	0.0199	12/20	09/16	GRP	57	71	41							
✓	Y	129.9995	99.9996	99.9996	10.0000	1.0000	0.1000	0.0199	12/21	10/35	ATM	55	70	36							
✓	Y	129.9998	99.9997	99.9997	10.0000	1.0000	0.1000	0.0200	12/22	14/34	ATM	54	66	44							
✓	N	129.9997	99.9997	99.9997	10.0000	1.0000	0.1000	0.0200	12/23	09/15	ATM	57	70	44							
✓	N	129.9996	99.9996	99.9996	10.0000	1.0000	0.1000	0.0199	12/26	12/30	ATM	57	70	44							
✓	N	129.9996	99.9996	99.9996	10.0000	1.0000	0.1000	0.0200	12/27	10/30	ATM	56	72	34							
✓	N	129.9997	99.9997	99.9997	10.0000	1.0000	0.1000	0.0200	1/8/08	13/40	GRP	54	68	38							
✓	N	129.9998	99.9997	99.9997	10.0000	1.0000	0.1000	0.0200	1/9/08	07/42	GRP	55	70	36							
✓	N	129.9997	99.9997	99.9997	10.0000	1.0000	0.1000	0.0199	1/11/08	10/40	ATM	59	73	42							
✓	N	129.9996	99.9996	99.9996	10.0000	1.0000	0.1000	0.0199	1/16/08	12/21	GRP	51	72	18							
✓	N	129.9998	99.9998	99.9998	10.0000	1.0000	0.1000	0.0199	1/17/08	12/37	GRP	56	71	37							
✓	N	129.9995	99.9996	99.9996	10.0000	1.0000	0.1000	0.0200	1/18/08	11/16	GRP	56	71	37							
✓	Y	129.9996	99.9996	99.9996	10.0000	1.0000	0.1000	0.0199	1/21/08	14/26	GRP	56	72	34							
✓	N	129.9995	99.9996	99.9996	10.0000	1.0000	0.1000	0.0199	1/22/08	15/13	GRP	56	71	37							
✓	Y	129.9996	99.9996	99.9996	10.0000	1.0000	0.1000	0.0199	1/23/08	08/05	GRP	54	69	36							
✓	Y	129.9996	99.9996	99.9996	10.0000	1.0000	0.1000	0.0200	1/24/08	07/58	GRP	54	70	33							
✓	Y	129.9996	99.9996	99.9996	10.0000	1.0000	0.1000	0.0200	1/24/08	14/50	GRP	56	71	37							
✓	N	129.9997	99.9997	99.9997	10.0000	1.0000	0.1000	0.0200	1/31/08	15/05	GRP	55	69	38							
✓	N	129.9996	99.9996	99.9996	10.0000	1.0000	0.1000	0.0199	2/1/08	10/29	GRP	54	69	36							
✓	N	129.9996	99.9996	99.9996	10.0000	1.0000	0.1000	0.0199	2/2/08	16/20	ATM	50	72	41							
✓	N	129.9996	99.9996	99.9996	10.0000	1.0000	0.1000	0.0200	2/3/08	17/10	ATM	57	70	44							

WOODSTOVE DATA SHEET 4-4 ANALYTICAL BALANCE QC RECORD SHEET SCALE: SARTORIUS  
 FROM: 12/30/08 MODEL: CP224S  
 THROUGH: 2/17/09 SN: 17050374

	Recall	140 g	100 g	10 g	1.0 g	100 mg	20 mg	Date	Time	Tech	Wet Bulb	Dry Bulb	& RH
✓	N	139.9995	99.9995	9.9999	1.0000	0.1000	0.0199	12/29/08	1430	ADM	58	72	42
✓	N	139.9995	99.9995	9.9999	1.0000	0.1000	0.0199	12/23/08	1057	GRP	60	76	38
✓	N	139.9995	99.9995	9.9999	1.0000	0.1000	0.0200	12/24/08	1019	ATM	59	72	43
✓	N	139.9994	99.9994	9.9999	1.0000	0.1000	0.0200	12/24/08	1142	ATM	59	72	45
✓	N	139.9994	99.9994	9.9999	1.0000	0.1000	0.0200	12/24/08	1050	ATM	60	75	37
✓	N	139.9994	99.9994	9.9999	1.0000	0.1000	0.0199	1/25/09	1157	PDG	58	75	34
✓	N	139.9994	99.9994	9.9999	1.0000	0.1000	0.0199	1/26/09	1845	ATM	60	75	37
✓	N	139.9995	99.9996	9.9999	1.0000	0.1000	0.0199	1/7/09	1530	GRP	58	70	48
✓	N	139.9994	99.9994	9.9999	1.0000	0.1000	0.0199	1/8/09	1356	PDG	60	72	49
✓	Yes	139.9993	99.9994	9.9999	1.0000	0.1000	0.0200	1/23/09	1053	PDG	58	72	42
✓	Yes	139.9993	99.9993	9.9999	1.0000	0.1000	0.0199	1/11/09	1128	JRP	55	72	31
✓	No	139.9994	99.9995	9.9999	1.0000	0.1000	0.0199	1/12/09	0845	PDG	59	75	38
✓	No	139.9993	99.9993	9.9999	1.0000	0.1000	0.0200	1/13/09	0825	JRP	58	74	37
✓	Yes	139.9993	99.9994	9.9999	1.0000	0.1000	0.0199	1/14/09	1212	PDG	57	72	36
✓	No	139.9993	99.9993	9.9999	1.0000	0.1000	0.0199	1/14/09	1420	GRP	59	75	37
✓	No	139.9992	99.9993	10.0000	1.0000	0.1000	0.0199	1/15/09	126	GRP	58	74	37
✓	Yes	139.9994	99.9995	9.9999	1.0000	0.1000	0.0199	1/20/09	0950	PDG	58	74	37
✓	No	139.9993	99.9994	10.0000	1.0000	0.1000	0.0199	1/20/09	1230	PDG	56	71	37
✓	No	139.9993	99.9993	9.9999	1.0000	0.1000	0.0199	1/20/09	1613	JRP	57	73	35
✓	No	139.9994	99.9994	9.9999	1.0000	0.1000	0.0200	1/22/09	1138	ATM	57	72	38
✓	No	139.9993	99.9993	9.9999	1.0000	0.1000	0.0199	1/23/09	1150	PDG	58	75	33
✓	Yes	139.9992	99.9993	10.0000	1.0000	0.1000	0.0200	1/26/09	1359	JRP	56	70	25
✓	No	139.9994	99.9995	10.0000	1.0000	0.1000	0.0199	1/27/09	1230	PDG	58	72	31
✓	No	139.9993	99.9993	10.0000	1.0000	0.1000	0.0200	1/26/09	1452	ATM	61	75	41
✓	Yes	139.9993	99.9994	10.0000	1.0000	0.1000	0.0199	1/29/09	1430	GRP	58	77	29
✓	No	139.9995	99.9995	9.9999	1.0000	0.1000	0.0199	1/30/09	1256	PDG	60	72	49
✓	Yes	139.9993	99.9994	9.9999	1.0000	0.1000	0.0199	2/17/09	1200	ATM	58	74	37
✓	No	139.9993	99.9993	9.9999	1.0000	0.1000	0.0199	2/2/09	1350	JRP	58	77	29
✓	Yes	139.9995	99.9996	9.9999	1.0000	0.1000	0.0199	2/5/09	1118	PDG	59	72	45
✓	No	139.9995	99.9995	9.9999	1.0000	0.1000	0.0199	2/6/09	1150	GRP	57	74	33
✓	No	139.9994	99.9994	10.0000	1.0000	0.1000	0.0200	2/7/09	1015	ATM	49	70	19
✓	No	139.9994	99.9994	9.9999	1.0000	0.1000	0.0199	2/16/09	1501	PDG	61	78	36
✓	No	139.9993	99.9994	9.9999	1.0000	0.1000	0.0200	2/17/09	1439	JRP	56	72	35

SCALE: SARTORIUS  
 MODEL: CP224S  
 SN: 17050374

WOODSTOVE DATA SHEET 4-4 ANALYTICAL BALANCE QC RECORD SHEET

FROM: 2/10/09  
 THROUGH:

Level	Recali	140 g	100 g	10 g	1.0 g	100 mg	20 mg	Weight	Date	Time	Tech	Wet Bulb	Dry Bulb	% RH
Y	Y	139.9993	99.9994	9.9999	1.0000	0.1000	0.0199	0.0199	2/10/09	1802	ATM	55	70	26
Y	Y	139.9993	99.9994	9.9999	1.0000	0.1000	0.0199	0.0199	2/19/09	1248	4RP	56	73	32
Y	Y	139.9993	99.9994	9.9999	0.9999	0.1000	0.0199	0.0199	2/20/09	1018	PDB	57	74	33
Y	Y	139.9993	99.9994	9.9999	1.0000	0.1000	0.0200	0.0200	2/21/09	1519	ATM	60	77	35
Y	Y	139.9993	99.9994	9.9999	1.0000	0.1000	0.0199	0.0199	2/22/09	1222	ATM	47	69	37
Y	Y	139.9994	99.9994	9.9999	0.9999	0.1000	0.0199	0.0199	2/23/09	1406	PDB	58	70	48
Y	No	139.9994	99.9994	9.9999	1.0000	0.1000	0.0200	0.0200	2/24/09	0933	ATM	59	76	35
Y	Y	139.9995	99.9995	9.9999	1.0000	0.1000	0.0199	0.0199	2/25/09	1123	PDB	60	76	38
Y	Y	139.9994	99.9994	9.9999	1.0000	0.1000	0.0199	0.0199	2-26/09	1258	JRP	55	70	36
Y	Y	139.9993	99.9993	9.9999	1.0001	0.1001	0.0200	0.0200	2/28/09	1330	ATM	57	74	33
Y	Y	139.9995	99.9995	9.9999	0.9999	0.1000	0.0199	0.0199	3/3/09	1431	PDB	59	76	35
Y	Y	139.9993	99.9995	9.9999	1.0000	0.1000	0.0199	0.0199	3/4/09	1556	4RP	56	72	40
Y	No	139.9994	99.9994	9.9999	1.0001	0.1001	0.0200	0.0200	3/5/09	1350	ATM	60	75	40
Y	No	139.9993	99.9993	9.9999	1.0000	0.1000	0.0200	0.0200	3/7/09	0850	ATM	57	71	41
Y	Y	139.9993	99.9993	10.0000	1.0001	0.1000	0.0200	0.0200	3/8/09	1323	ATM	55	70	36
Y	Y	139.9993	99.9993	9.9999	1.0000	0.1000	0.0199	0.0199	3/10/09	1122	PDB	50	75	10

Woodstove Particulate  
Catch Processing Sheet  
Woodstove Data Sheet #5  
EPA M5G-1

Unit: Kuma Ashwood  
Run: EPA 1  
Date: 2/16/09  
Technicians: ATM  
Revised 1/16/98-Data Sheet #5

Filters

Filter # (Front) 706 Beaker # 21  
Final Wt. .7130 g MI 55  
Tare Wt. .6948 g Desc. Acetone  
Net Wt. .0182 g

Final Wt. 71.0096 g + .0105  
Tare Wt. 71.0018 g +  
Net Wt. .0078 g +

Filter # (Rear) 705 Beaker # \_\_\_\_\_  
Final Wt. .6814 g MI \_\_\_\_\_  
Tare Wt. .6837 g Desc. \_\_\_\_\_  
Net Wt. -.0023 g +

Final Wt. \_\_\_\_\_ g  
Tare Wt. \_\_\_\_\_ g  
Net Wt. \_\_\_\_\_ g

Acetone Blank Calculation:

Blank Date: 12/8/07

Blank Beaker # 25  
MI 50  
Desc. Acetone

Final Wt. 72.6511 g  
Tare Wt. 72.6512 g  
Net Wt. -0.0001 g = 0.0000

0.0000 g ÷ 50 ml = 0.00000 g/ml

Blank Residue Value Calculation:

0.00000 g/ml acetone X 55 ml acetone = 0.0000 g  
Blank Residue Value

Total Particulate Catch Calculation

Filter: .0182 g  
Filter: -.0023 g  
Beakers: .0078 g -- 0.0000 g = .0078 g  
Total Catch Blank Residue Value  
Total Catch = .0234 g

Unit Kuma Harwood  
 Run # EPA 1  
 Date 2/16/99  
 Technician ATM IRP POG  
 WST6-Form1, Rev8/96

MISCELLANEOUS TEST DATA  
 WOODSTOVE DATA SHEET #8

Useable Firebox Dimensions: See QC Section Useable Volume: 2.094 ft<sup>3</sup>

Dilution Tunnel Draft (If applicable): Start .000 Stop .000 <sup>"H<sub>2</sub>O</sup>

Test Chamber Air Velocity: Start: 00.0 Stop: 00.0 Avg: 00.0 ft/min

Wet Bulb/ Start: WB: 60 °F DB: 76 °F 1.20% Amb Moisture 38 %RH

Dry Bulb Stop: WB: 59 °F DB: 75 °F 1.15% Amb Moisture 37 %RH

$\bar{X} = 1.175$  % Ambient Moisture  $\bar{X} = 37.5$  % Relative Humidity (RH)

Empty Stove Wt: 440.2 lbs.

Empty Stove Wt with Stack (Inc. Oil Seal) Wet: 763.8 lbs. Dry: 763.8 lbs.

Empty Stove Wt with Stack and Ash Ash: — lbs. Total: — lbs.

Kindling Wt. Total 4.8 lbs. Paper: 0.3 lbs. Wood: 4.5 lbs.

Pre Burn Fuel Wt. 111.430 + 12.606 + 14.212 Total: 38.248 lbs.

Total Kindling and Pre Burn Fuel Wt 43.048 lbs.

Coal Bed Wt-lbs: Range (3.3 - 2.7) 767.1 - 766.5 lbs. Actual 2.8 lbs.

766.6

Allowable Amount of Charcoal that can be removed:

Coal Bed Wt. Range  $\left( \frac{3.3}{\text{Upper Wt.}} + \frac{2.7}{\text{Lower Wt.}} \right) \times .25 = \underline{0.71 \text{ lbs}}$  lbs.

Test Fuel Wt-lbs: Ideal 14.7 lbs. Range: 16.1 - 13.2 lbs. Actual: 13.210 lbs.

Test Fuel Size (pcs.) (.75 x 1.5 x 5" Flanges) 1422 lbs 16 Pcs.

2 x 4's x 16.375 " 3 Pcs 5.844 lbs. 44.24 %

4 x 4's x 16.375 " 2 Pcs 7.366 lbs. 55.76 %

4.975 kg

Est. Dry Burn Rate (Kg/Hr.)  $\frac{13.210 - (13.210 \times \frac{4.975}{2.046}) \times \frac{60}{128}}{128} = \underline{2.3320}$  Est. Dry Burn Rate (Kg/Hr)

Est EPA Heat Output (HO<sub>E</sub>) (19,140) x 63 x 2332 = 28.120 Est Heat Output (HO<sub>E</sub>) BTU's/Hr

Comments:



Stove Operating Data  
Woodstove Test Data Sheet #9  
Cold Start - High Burn

Unit: KUMA ASHWOOD  
Run: EPA 1  
Date: 2/16/09  
Technician(s): ATM JRP POG  
Data Sheet #9 - Rev 1/98-Pg.5

Fire Started: 1330 PST

Warm up and Preburn: Primary Air: Wide open from ignition until the start of the test. At the run setting of wide open until the start of the test. High burn.

Secondary Air: No Controls, Naturally drafted

Secondary Burn/ Bypass: N/A

Charcoal Bed Preparation: Broke up, raked and leveled the coal bed prior to the addition of each warm up/pre burn fuel charge. Starting 1130 before the start of the test, broke up, raked and leveled the coal bed. In stove for 30 seconds.

Test: Door wide open during loading 0 min 50 sec, then closed.

Primary Air: Wide open from the start of the test (0:00) until the end of the test.  
High Burn.

Secondary Air: No Controls, Naturally drafted

Secondary Burn/ Bypass: N/A

Fan: ON OFF during the warm up, ON OFF High during the preburn, ON OFF at the start of the test, ON OFF for the first 5 minutes of the test, ON OFF High at 5 minutes into the test, ON OFF for the rest of the test.

Test Run Anomalies:

WOODSTOVE OPERATING DATA  
 WOODSTOVE DATA SHEET #9A-1

Wood Data: Kindling: A mix of the below grades

	Size	Mill	Grade	Species
Pre Burn	2X4	Forest Grove	# 2, Std & Btr	D. Fir, Sfc. Gnw
Test Fuel	2X4	Forest Grove	# 2, Std & Btr	D. Fir, Sfc. Gnw
	4X4	Forest Grove	No. 1	D. Fir, Sfc. Gnw

All grades WCLB Rules unless otherwise noted.

Warm up Information:

1st Warm up/Pre Burn Fuel charge (11,430 lbs) added at 13:46.  
 2nd Warm up/Pre Burn Fuel charge (12,606 lbs) added at 14:39.  
 3rd Warm up/Pre Burn Fuel charge (14,212 lbs) added at 15:40.  
 4th Warm up/Pre Burn Fuel charge (\_\_\_\_\_ lbs) added at \_\_\_\_\_.  
 5th Warm up/Pre Burn Fuel charge (\_\_\_\_\_ lbs) added at \_\_\_\_\_.  
 6th Warm up/Pre Burn Fuel charge (\_\_\_\_\_ lbs) added at \_\_\_\_\_.  
 7th Warm up/Pre Burn Fuel charge (\_\_\_\_\_ lbs) added at \_\_\_\_\_.  
 8th Warm up/Pre Burn Fuel charge (\_\_\_\_\_ lbs) added at \_\_\_\_\_.

1<sup>st</sup> Rick 4-12", 4-16" 2X4's    3<sup>rd</sup> Rick 4-12", 3-16" 2X4's  
 2<sup>nd</sup> Rick 8-16" 2X4's    Hi. Barn 3<sup>rd</sup> Rick 4-12", 5-16" 2X4's

The coals were scooped out of the stove immediately prior to adding the 3<sup>rd</sup> pre burn/warm up fuel charge. The stove lost 0.0 lbs. 2.0 lbs. of coals were put back in the stove after the scoop.

All pre burn/warm up fuel pieces were either 12 or 16 inches long. All preburn pieces/fuel charges were "ricked" in the stove. The pieces in the bottom layer in each rick contained 2 pcs that were 12 or 16 inches long and were loaded flat and perpendicular to the door. The pieces in the second layer in each rick were loaded on their side (edge) approximately parallel to the door and contained 3 or 4 pcs 16 inches long. The third layer (and fourth layer if present) was loaded flat, perpendicular to the door and contained 2 pcs 12 or 16 inches long. The majority of the pieces in each rick were in the second layer which had an approximate 0.5-1.0" space between pieces. (The loading directions indicate the direction of the longest dimension on each piece relative to the loading door opening.) Each pre burn/warm up fuel charge normally weighs within the weight range allowed for the actual test fuel charge

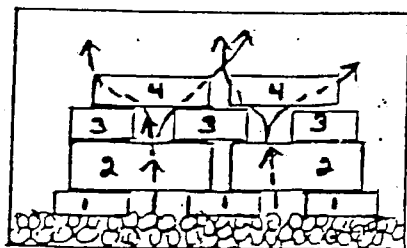
WOODSTOVE OPERATING DATA  
WOODSTOVE DATA SHEET #9A-2

Unit: Kuma Ashwood  
Run # EPA 1  
Date 2/16/09  
Technician ATM  
Page 2 of 3  
WST7-Form2-A, Rev 6/90

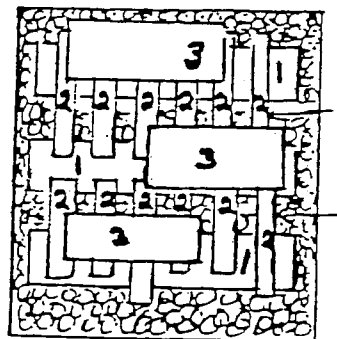
Warm up Information (cont.):

Each warm up/preburn fuel charge was ricked in exactly (as much as possible) the same manner and the weight of each rick was usually within the allowable weight range for the test fuel charge. The physical arrangement and alignment of each rick was designed to accomplish three (3) things: (1) The bottom layer was nestled firmly into the coal bed and was as close to being level with the bottom of the stove as possible, thus providing a stable loading platform for the rest of the rick, keeping it in a ricked state (as opposed to a col-lapsed or fallen down state) until the rick reached the charcoal stage and sags or collapses of its own accord. (2) It enhances the flow of primary air through the ricked preburn fuel charge, for the primary air would flow through the spaces between the pieces in the first layer and then up through the spaces between the pieces in the second, third and, if present, fourth layers. (3) It maximized, as much as possible, the surface to volume ratio of each preburn fuel charge, thereby allowing the fire immediate access to as much wood surface as possible and, thereby, insuring uniform charcoalization. All three of these enhance combustion and so get the stove as hot as possible during the warm up period, thereby maximizing the amount of heat (BTU's) stored in the stove. The actual preburn was not started until the stove surface temperatures had maximized and stabilized, thus indicating that the amount of heat stored in the stove had peaked. For this stove, the thermal storage was monitored using the Stove Top T/C surface temperature(s) and the peak value(s) obtained were 1084 of.

1026  
1084



Front View



Top View

The arrows indicate the direction of the air flow through the rick.

The primary air was adjusted to the run setting of Wide Open 12.9 lbs above the upper charcoal bed weight.

WOODSTOVE OPERATING DATA  
WOODSTOVE DATA SHEET #9A-3

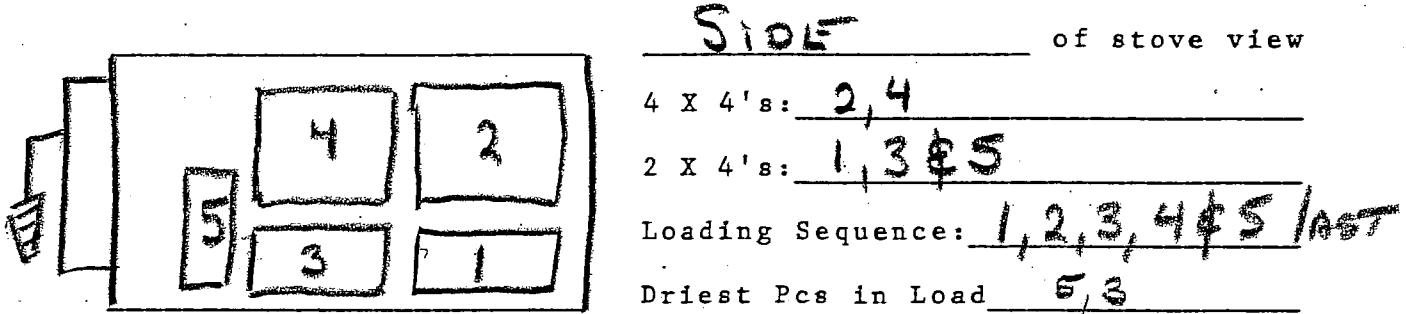
Unit Kuma Ashwood  
Run # EPA 1  
Date 2/16/09  
Technician ATM  
Page 3 of 3  
WST5-Form2-Rev11/89

Additional Comments: Test Start Sequence: ① Turned Fan Off  
② Opened Door ③ Loaded Fuel ④ Cleared coals away from air front of the LPAD ⑤ Closed door

TOTAL ELAPSED Time: 0:50  
Photo Taken @ 1:30

Test Fuel Charge Loading Information:

Test Fuel Charge and Loading Sequence Diagram



Loaded the test fuel charge on an essentially level, Medium sized, average/cool coal bed (in appearance, color and temperature for a High burn rate. Load: 0:50 Ignition: ~ 0:46

Door Closed 0:50 Vertical Column of flame (VC) up to baffle by 0:55.

2:14.9 2<sup>nd</sup> pcs had ignited.  
2:11.0 2<sup>nd</sup> forward pass front tube  
2:14.0 7.92/0.62 Gas Balance ML/L smoke  
3:02 Flames/Secondaries full width of pc 4  
3:15 " " " " pcs 4 & 5  
3:50 Front Tube igniting  
5:00 Fan ON High 11.86/.42 Light smoke.

Unit: Kuma Ashwood  
 Run: EPA  
 Date: 2/10/9  
 Technician: JAM JRP POG  
 WST1-Form7-Rev11/89

FUEL MOISTURE  
 WOODSTOVE TEST DATA SHEET #10

5kg. = 11.024 lbs. 1kg. = 2.204 lbs

Room Temperature: 65 °F Correction Factor: +0.5

NOTE: Record readings to the nearest 0.5% moisture  
 Uncor Values are corrected for temperature: Yes      No       
 Time Test Fuel Moisture Readings taken at: 1410  
 Calibration Checks: X      Y      12.0 11.8 22.0 22.2

Pc #	Dimen	Use	Top		Bottom		Side		Piece Avg Corrected
			Uncor	Cor	Uncor	Cor	Uncor	Cor	
1	3 pcs	K	8.5	8.95	9.0	9.50	8.5	8.95	9.133
2									
3									
4	2x4-8'	P	18.5	19.8	18.5	19.8	20	21.4	20.333
5			20.5	22.0	21	22.6	19.5	20.9	21.833
6			18.5	19.8	18.5	19.8	19	20.3	19.967
7			18.5	19.8	19	20.3	19	20.3	20.133
8	∇	∇	19	20.3	19	20.3	19	20.3	20.300
9									102.566
10	3"								
42 11	2x4-16/8	T	17.5	18.6	18	19.2	18.5	19.8	19.200
1.914 12			19	20.3	20	21.4	20	21.4	21.033
1.390 13	∇	∇	18	19.2	18	19.2	18	19.2	19.200
14	3"								
3.588 15	4x4-16/8	T	21	22.6	22.5	24.3	17	18.1	21.667
3.430 16	∇	∇	23	21.9	20.5	22.0	15.5	16.5	21.133
17									102.233
18									
1.422 19	SPACERS	T	19	20.3	19	20.3	20	21.4	20.167
20									OUT SPACERS

Kindling	Pretest Fuel	Test Load
9.133%	20.5132%	20.447%
8.369%	17.022%	16.976%

% Moisture - Dry Basis:  
 % Moisture - Wet Basis:  
 13.210 7.366

To obtain Wet from Dry:  $\frac{100 \times \% \text{ Dry Rdg.}}{100 + \% \text{ Dry Rdg.}} = \% \text{ Moisture, Wet Basis}$   
 Acceptable Ranges: 16-20% wet; 19-25% dry (17.5 - 22.5 on Meter [Uncor reading] at 70°F)  
 Key for Use: K= Kindling P= Pretest Fuel T= Test Fuel

1. 11.430  
 2. 12.606  
 3. 14.212

WOOD DENSITY DETERMINATION  
WOODSTOVE TEST DATA SHEET #11

Unit: Kuma Ash wood  
Run#: EPA 1  
Date: 2/16/09  
Technician: A. T. MYREN  
WST2-form11-Rev 6/90

Wood Piece: 2x4 Nominal Dimensions: 3.5" x 1.5" x 3.5"  
Depth (D): 3.860 cm  
Width (W): 0.865 cm  
Length (L): 8.1620 cm  
8.740 cm  
8.730 cm  
8.770 cm  
Length  $\bar{X}$  = 8.715 cm  
Volume: 298.218 cm<sup>3</sup>  
(D X W X L)

MOISTURE: Room Temperature: 65 °F Correction Factor: +0.5  
Uncorrected Meter Readings Corrected for temperature: Yes  No

NOTE: Record moisture meter readings to the nearest 0.5%.

	Uncor	Cor
Top:	15.5	16.5 %
Bottom:	16	17.0 %
Side:	15	15.9 %
$\bar{X}$ :		16.467 %

Avg % Moisture (Dry) 16.467 %  
Avg % Moisture (Wet) 14.139 %  
Scale: Levelled In  Out   
Zeroed: In  Out

Wet Weight: 151.0 g Dry Weight: 129.1 g

% Moisture Dried Basis: 14.503 %  
[1 - (Dry Wt ÷ Wet Wt)] X 100

Into Dryer Date 2/16/09 Time 1603 Temp 190 °F  
Out of Dryer Date 3/3/09 Time 0915 Temp 192 °F  
(Minimum Time in Dryer: 24 hrs.) Minimum Dryer Temp 100°C (212°F)

Density = 129.1 g (dry wt) ÷ 298.218 cm<sup>3</sup> (volume) = 0.4329 g/cm<sup>3</sup>

Pellet Fuel Moisture Content Determination

Tare Beaker Wt. \_\_\_\_\_ g  
Wet Wt: \_\_\_\_\_ g - \_\_\_\_\_ g = \_\_\_\_\_ g  
Gross Wet Wt. Tare Beaker Wt. Net Wet Wt.  
Dry Wt: \_\_\_\_\_ g - \_\_\_\_\_ g = \_\_\_\_\_ g  
Gross Dry Wt. Tare Beaker Wt. Net Dry Wt.

% Moisture Dried Basis: \_\_\_\_\_ %  
[1 - (Net Dry Wt ÷ Net Wet Wt.)] X 100











PRE AND POST TEST ZERO/SPAN CHECK  
WOODSTOVE DATA SHEET #15-1

Colville

Site: Myren Consulting, [redacted], WA Date: 2/16/09 Analyte: CO<sub>2</sub>

Source: Kuma Ashwood Run #: EPA 1

Zero Cyl #: TC 3AAM154 Conc. 00.0 % CO<sub>2</sub> Cyl Press: 1590 psi

Certified by: Oxarc Date: 11/12/07

Span Cyl #: AS90457 Conc. 12.5 % CO<sub>2</sub> Cyl Press: 1480 psi

Certified by: Matheson Tri Gas Date: 2/2/2009

Analyzer: Make: Horiba Model: PIR-2000 SN: 607024

Range: 0 - 25.0% CO<sub>2</sub> Analyzer Output: 0 - 1.0 v.

Flow: 1.5 SCFH Measured by: Rotameter: X Flowmeter: \_\_\_\_\_

EPA Span Value = 25.0% CO<sub>2</sub>  
EPA Control Limits = + 2.5% of 25.0% CO<sub>2</sub> = + 0.625% CO<sub>2</sub>

Pre Run Audit: By: A.P. Myren Time: 1548 Temp: 72 °F

Audit Results

Point #	Expected Response			Actual Response			+ Conc. Difference	Δ %
	Meter	DVM	%	Meter	DVM	%		
Zero	00.0	.000	00.0	00.0	.001	.07925	+0.07925	+0.32
Span	50.0	.500	12.500	49.75	.500	12.4105	-0.08953	-0.72

.238 1220

Comments:

Post Run Audit: By: A.P. Myren Time: 1956 Temp: 77 °F

Audit Results

Point #	Expected Response			Actual Response			+ Conc. Difference	Δ %
	Meter	DVM	%	Meter	DVM	%		
Zero	00.0	.000	00.0	00.0	.001	.07925	+0.07925	+0.32
Span	50.0	.500	12.500	49.75	.500	12.4105	-0.08953	-0.72

.237

Comments:

+ Conc. Difference = Act % - Exp (Std) %  
 Zero % Difference =  $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Full Scale Value}} \times 100$   
 Span % Difference =  $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Exp \% (ppm)}} \times 100$

PRE AND POST TEST ZERO/SPAN CHECK  
WOODSTOVE DATA SHEET #15-3

Colville

Site: Myren Consulting, Woodinville, WA Date: 2/16/09 Analyte: CO

Source: Kuma Ashwood Run #: EPA 1

Zero Cyl #: TC3AAM154 Conc. 00.0 % CO Cyl Press: 1590 psi

Certified by: Oxarc Date: 11/12/07

Span Cyl #: AS90457 Conc. 2.0 % CO Cyl Press: 1480 psi

Certified by: Matheson Tri Gas Date: 2/2/2009

Analyzer: Make: MORIBA Model: MEMA 311GE SN: GE-30025

Range: 0 - 10.0% CO Analyzer Output: 0 - 100 mv.

Flow: 1.5 SCFH Measured by: Rotameter: X Flowmeter:         

EPA Span Value = 5.0% CO  
EPA Control Limits = +2.5% of 5.0% CO = + 0.125% CO

Pre Run Audit: By: A.T. Myren Time: 1548 Temp: 72 °F

Point #	Expected Response			Actual Response			+ Conc. Difference	Δ %
	Meter	DVM	%	Meter	DVM	%		
Zero	00.0	00.0	00.0	0.00	.000	0.00443	-0.00443	-0.04
Span	2.00	2.00	2.00	2.00	2.01	2.0160	+0.0160	+0.80
Comments:				1.22	1.22	1.2219	-0.0381	-3.02

Post Run Audit: By: A.T. Myren Time: 1956 Temp.: 77 °F

Point #	Expected Response			Actual Response			+ Conc. Difference	Δ %
	Meter	DVM	%	Meter	DVM	%		
Zero	00.0	00.0	00.0	0.00	0.00	0.01448	-0.01448	-0.14
Span	2.00	2.00	2.00	2.00	1.99	1.9959	-0.04105	-0.21
Comments:				1.21	1.21	1.2118	-0.04815	-3.82

Conc. Difference = Act % - Exp (Std) %  
 Zero % Difference =  $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Full Scale Value}} \times 100$   
 Span % Difference =  $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Exp \% (ppm)}} \times 100$

Unit: Kama Ashwood  
 Run: EPA  
 Date: 21 109  
 Technicians: ATM JRP POG  
 WSP-Form3-Rev11/89

QUALITY CHECKS  
 WOODSTOVE DATA SHEET #16

Ambient = T/C #1: \_\_\_\_\_ °F T/C #30: \_\_\_\_\_ °F  
 Thermocouple Check (at ambient): T/C #1: \_\_\_\_\_ °F; T/C #2: 74.2 °F;  
 T/C #3: 72.4 °F; T/C #4: 68.7 °F; T/C #5: 69.5 °F;  
 T/C #6: 67.8 °F; T/C #7: 67.8 °F; T/C #8: 68.5 °F;  
 T/C #9: 68.7 °F; T/C #10: 68.4 °F; T/C #11: 67.6 °F;  
 T/C #12: 72.1 °F; T/C #13: 68.4 °F; T/C #14: 63.2 °F;  
 T/C #15: 70.0 °F; T/C #16: 64.4 °F; T/C #17: 68.3 °F;  
 T/C #18: \_\_\_\_\_ °F; T/C #19: \_\_\_\_\_ °F; T/C #20: \_\_\_\_\_ °F;  
 T/C #21: \_\_\_\_\_ °F; T/C #22: \_\_\_\_\_ °F; T/C #23: \_\_\_\_\_ °F;  
 T/C #24: \_\_\_\_\_ °F; T/C #25: \_\_\_\_\_ °F; T/C #26: \_\_\_\_\_ °F;

Comments: \_\_\_\_\_

Thermocouple Readout: Pretest Zero/Span Check and Calibration:  
 Zero (0°F) = -0.6/7 Adj to: \_\_\_\_\_ °F Post Test Check Zero (0°F): 0.5 °F % Difference +0.10  
 Span (2000°F): 2000.9 Adj to: \_\_\_\_\_ °F Span (2000°F): 2002.4 °F % Difference +0.10

(Allowable % Difference = 1.5%. Use formulas on Woodstove Data Sheet #15 to calculate % Difference) **In Degrees Absolute.**

Thermocouple Readout Pretest Linearity Check  
 0°F = -0 °F; 200°F = 201.3 °F; 400°F = 398.8 °F;  
 600°F = 601.2 °F; 800°F = 801.5 °F; 1000°F = 1000.8 °F;  
 1200°F = 1198.5 °F; 1400°F = 1399.7 °F; 1600°F = 1600.3 °F;  
 1800°F = 1800.7 °F; 2000°F = 2000.9 °F

Combustion Gas (CO<sub>2</sub>, O<sub>2</sub>, CO) Train Leak Check: Pre ok Post ok  
 Draft (Static) Gauge Zero Check: Pre ok Post ok

Scale Check Pre (Wt. #'s): 773.6 - 768.6 = 5.0 lbs / 5.0 lbs = 0/ok (ATM)  
 Post (Wt. #'s): 776.4 - 771.4 = 5.0 lbs / 5.0 lbs = 0/ok (ATM)

Stack cleaned prior to the run: Yes  No \_\_\_\_\_  
 Tunnel cleaned prior to the run: Yes  No \_\_\_\_\_ (Whole tunnel to exhaust outlet)

MYREN CONSULTING CERTIFICATION TEST DATA

DILUTION TUNNEL CALCULATIONS

1/25/09, Md=28.56, Bws=4% 6" Tunnel

File Name: EPA 3

Manufacturer: KUMA

Model Number: ASHWOOD

Lab Name: MYREN

Test Date: 2/18/09

Run Number: EPA 3

Run Box Y Factor: 1.0177

Meter pressure (in): 28.511

Gas meter temp (ave): 86

delta H(ave): 0.900

Gas meter initial reading: 159.0010

Gas meter final reading: 287.9860

Front catch (acetone) mg: 16.9489

first filter catch (mg): 10

second filter catch (mg): -15.2

Tunnel Flow (Qsd) (dscfm): 139.499

Emission Rate(g/hr): 0.946

Emission Rate(M5H): 1.738

Avg. of Delta P Sq. Roots: 0.2023

Vs (Avg.)(ft/min): 817.298

Tunnel Avg. Temperature (F): 95.269

Test time(min): 245

Fuel Load(lb. wet): 13.308

Wood moisture(%wet): 16.602

Burn rate(dry kg/hr): 1.233

Sample Volume (dscf): 121.255

Avg. Tunnel Static (-inch H2O): 0.1614

Room Blank Catch (mg/dscf): 0

Emission Factor (g/kg): 0.7670

Pitot Correction Factor: 0.9634

front filter number: 710

back filter number: 709

Beaker Number: 23

PRELIMINARY RESULTS

FINAL RESULTS:

DATA SUMMARY

MODEL: ASHWOOD

RUN: EPA 3

DATE: 2/18/09

DBR: 1.233

EMISSION RATE (g/hr)(M5H): 1.7376

EMISSION FACTOR (g/kg): 0.7670

AVG. % PROPORTIONALITY: 95.974

Run Time (min)	Pitot Deltap (-inch H2O)	TNL Temp (°F)	Gas Meter RDG (ft3)	Gas Meter Temp (°F)	Gas Meter Delta H (in.H2O)	Tunnel Velocity (ft/min)	PROP RATE (%)	dDGM vol std (ft3)	Tunnel Static (-inch H2O)	Square Root Delta P	Dry Gas Meter RDG (m3)
0	0.041	94	159.0010	69	0.900	848.31			0.160	0.2025	
10	0.039	105	164.2640	72	0.900	835.52	104.7	5.075	0.152	0.1975	
20	0.040	101	169.4730	75	0.900	843.17	100.8	4.995	0.153	0.2000	
30	0.039	102	174.7030	78	0.900	833.30	101.5	4.987	0.150	0.1975	
40	0.041	102	179.9190	81	0.900	854.41	97.6	4.946	0.163	0.2025	
50	0.042	101	185.1430	83	0.900	864.00	95.8	4.936	0.167	0.2049	
60	0.041	99	190.3670	85	0.900	852.13	96.1	4.917	0.165	0.2025	
70	0.041	99	195.5990	86	0.900	852.13	95.9	4.916	0.164	0.2025	
80	0.042	99	200.8430	87	0.900	862.46	94.6	4.918	0.165	0.2049	
90	0.041	98	206.1000	87	0.900	851.37	95.9	4.930	0.165	0.2025	
100	0.042	98	211.3730	88	0.900	861.69	94.7	4.936	0.166	0.2049	
110	0.042	95	216.6410	88	0.900	859.37	94.3	4.932	0.165	0.2049	
120	0.041	93	221.9120	88	0.900	847.54	95.4	4.935	0.160	0.2025	
130	0.041	91	227.1940	88	0.900	846.01	95.4	4.945	0.162	0.2025	
140	0.041	91	232.4740	89	0.900	846.01	95.0	4.934	0.161	0.2025	
150	0.041	90	237.7560	88	0.900	845.24	95.3	4.945	0.160	0.2025	
160	0.041	91	243.0370	89	0.900	846.01	95.0	4.935	0.162	0.2025	
170	0.041	92	248.3280	89	0.900	846.78	95.3	4.944	0.163	0.2025	
180	0.041	92	253.6110	89	0.900	846.78	95.1	4.937	0.163	0.2025	
190	0.041	92	258.9020	90	0.900	846.78	94.9	4.935	0.164	0.2025	
200	0.041	91	264.1860	90	0.900	846.01	94.7	4.929	0.161	0.2025	
210	0.041	91	269.4770	90	0.900	846.01	94.9	4.935	0.160	0.2025	
220	0.041	92	274.7560	90	0.900	846.78	94.7	4.924	0.162	0.2025	
230	0.041	92	280.0500	90	0.900	846.78	95.0	4.938	0.163	0.2025	
240	0.041	93	285.3390	90	0.900	847.54	95.0	4.933	0.161	0.2025	
245	0.041	93	287.8960	90	0.900	847.54	91.8	2.385	0.160	0.2025	
270			0.0000			0.00	0.0	0.000		0.0000	
280			0.0000			0.00	0.0	0.000		0.0000	
290			0.0000			0.00	0.0	0.000		0.0000	
300			0.0000			0.00	0.0	0.000		0.0000	
310			0.0000			0.00	0.0	0.000		0.0000	
320			0.0000			0.00	0.0	0.000		0.0000	
330			0.0000			0.00	0.0	0.000		0.0000	
340			0.0000			0.00	0.0	0.000		0.0000	
350			0.0000			0.00	0.0	0.000		0.0000	
360			0.0000			0.00	0.0	0.000		0.0000	
370			0.0000			0.00	0.0	0.000		0.0000	
380			0.0000			0.00	0.0	0.000		0.0000	

METHOD 5G-1 (EPA) PARTICULATE SAMPLING DATA

Rev. 2/09

DATE: 2/18/09 PAGE 1 OF 2 UNIT: Kuma Ashwood RUN: EPA 3

METER BOX: 45G-P METER Y: 1.0177 FILTER #'S: (F) 710 (R) 709

750/752  
PRE TEST LEAK CHECK: .002 CFM @ -15.6 IN HG FILTER SIZE: 110 mm

1054/1059  
POST TEST LEAK CHECK: 1005 CFM @ -15.1 IN HG PROBE LENGTH 21.0 IN

TIME		METER READING (FT <sup>3</sup> )	PITOT		TUNNEL TEMP (°F)	METER TEMP (°F)	GAS METER Δh	VAC (in Hg)
CLOCK	ELAPSED		ΔP	Pg				
1155	00	159.001	.041	-160	94	69	.90	0
1205	10	164.264	.039	-152	105	72	.90	0
15	20	169.473	.040	-153	101	75	.90	0
25	30	174.703	.039	-150	102	78	.90	0
35	40	179.919	.041	-163	102	81	.90	0
45	50	185.143	.042	-167	101	83	.90	0
55	60	190.367	.041	-165	99	85	.90	0
1305	70	195.599	.041	-164	99	86	.90	0
15	80	200.843	.042	-165	99	87	.90	0
25	90	206.100	.041	-165	98	87	.90	0
35	100	211.373	.042	-166	96	88	.90	0
45	10	216.641	.042	-165	95	88	.90	0
55	120	221.912	.041	-160	93	88	.90	0
1405	30	227.194	.041	-162	91	88	.90	0
15	40	232.474	.041	-161	91	89	.90	0
25	50	237.756	.041	-160	90	88	.90	0
35	60	243.037	.041	-162	91	89	.90	0
45	70	248.328	.041	-163	92	89	.90	0
55	180	253.611	.041	-163	92	89	.90	0
1505	90	258.902	.041	-164	92	90	.90	0

BP

00	28.51	255	28.915
60	28.505		
120	28.51		
180	28.51		
240	28.515	AVG. =	28.511

Pre Test Filter  
Check Weighing  
F .6594  
R .6809

End of Test Weight  
F .6699 R .6656  
.6590 .6806  
.0109 0

METHOD 5G - 1 (EPA) PARTICULATE SAMPLING DATA

Rev. 2/09

DATE: 2/16/09 PAGE 2 OF 2 UNIT: Kumar Ashwood RUN: EPA 3

METER BOX: 45G-P METER Y: 1.0177 FILTER #'S: (F) 710 (R) 709

PRE TEST LEAK CHECK: <sup>1.750/1.752</sup> 1.002 CFM @ -15.16 IN HG FILTER SIZE: 110 mm

POST TEST LEAK CHECK: <sup>1.054/1.059</sup> 1.005 CFM @ -15.11 IN HG PROBE LENGTH 21.0 IN

TIME		METER READING (FT <sup>3</sup> )	PITOT		TUNNEL TEMP (°F)	METER TEMP (°F)	GAS METER Δh	VAC (in Hg)
CLOCK	ELAPSED		ΔP	Pg				
1515	200	264.186	1041	-1161	91	90	190	0
25	10	269.477	1041	-1160	91	90	190	0
35	20	274.756	1041	-1162	92	90	190	0
45	30	280.050	1041	-1163	92	90	190	0
55	240	285.339	1041	-1161	93	90	190	0
1600	50245	282.986	1041	-1160	93	90	190	0
	60							
	70							
	80							
	90							
	00							
	10							
	20							
	30							
	40							
	50							
	60							
	70							
	80							
	90							

BP  
00 28.51    255 28.515  
160 28.505    \_\_\_\_\_  
170 28.51    \_\_\_\_\_  
180 28.51    \_\_\_\_\_  
240 28.515    AVG. = 28.510

Pre Test Filter  
 Check Weighing  
 F 1.6594  
 R 1.6809

End of Test Weight  
 F 1.6590    R 1.6806



MYREN CONSULTING, INC.

Dilution Tunnel Traverse Data with 8 Traverse Points

Unit: KUMA Ashwood  
 Run #: EPA 3  
 Date: 2/18/09

Technicians:

Rev 4/2/08

Pg

T<sub>cent</sub>

T<sub>trav</sub>

√ΔP<sub>cent</sub>

ΔP

√ΔP<sub>trav</sub>

Point Location

W-1	0.5"	.1033	.1817	.1041	.2025	104	104
2	1.5	.1039	.1975			105	104
Center	Center						104
3	4.5	.1040	.2000			104	101
4	5.5	.1038	.1949			103	101
S-1	0.5	.1037	.1924			101	101
2	1.5	.1039	.1975			101	101
Center	Center						101
3	4.5	.1039	.1975	.1040	.2000	101	101
4	5.5	.1036	.1897			100	101
Totals			1.5512		.4025	819	205
Average			.1939		.20125	102.375	102.5
						562.4	562.5
							101

°R = (°F + 460)

Ps = BP + (-Pg/13.6) = 20.51 + (-1505/13.6) = 20.498 "Hg

LEAK CHECKS:

Pre Test: Pg Leg: ✓ 4RP Velocity Head Leg: ✓ 9RP

Post Test: Pg Leg: ✓ 4RP Velocity Head Leg: ✓ 9RP

Rev 4/19/08

DILUTION TUNNEL GAS VELOCITY & VOLUMETRIC FLOW RATE CALCULATIONS

UNIT: KUMA Ashwood DATE: 2/18/09 RUN #: EPA 3 TECHNICIAN(S): ATM JRP  
POG

Average Gas Velocity in the Dilution Tunnel  $V_{strav}$  (EPA M2 EQN 2-9, ASTM E 2515-07 EQN 7)

$$(9) V_{strav} = (85.49) (\frac{0.99 \text{ cp}}{1.939}) \times \sqrt{\Delta P} \text{ "H}_2\text{O} = \frac{562.4}{(0)} \text{ Ts } ^\circ\text{A} = \underline{13,641.58} \text{ fps}$$

$$(9A) V_s = (\frac{13,641.58 \text{ fps}}{(60)}) = \underline{018.495} \text{ fpm}$$

Gas Velocity in the Center of the Dilution Tunnel -  $V_{scent}$  (EPA M2 EQN 2-9, ASTM E 2515-07 EQN 7)

$$(9) V_{scent} = (85.49) (\frac{0.99 \text{ cp}}{20125}) \times \sqrt{\Delta P} \text{ "H}_2\text{O} = \frac{562.5}{(0)} \text{ Ts } ^\circ\text{A} = \underline{14,159.94} \text{ fps}$$

$$(9A) V_s = (\frac{14,159.94 \text{ fps}}{(60)}) = \underline{049.596} \text{ fpm}$$

EPA M5G1 Section 4.2.2, ASTM E 2515-07 EQN 1 Adjustment Factor for Center of Tunnel Pitot Tube Location

$$F_p = V_{strav} / V_{scent} = \underline{13,641.58} \div \underline{14,159.94} = \underline{0.9634}$$

Average Stack Gas Dry Volumetric Flow Rate -  $Q_{sd}$  (EPA M2 EQN 2-10, ASTM E 2515-07 EQN 3)

$$(10) Q_{sd} = 3600 (1 - 0.04 \text{ Hws}) (\frac{13,641.6 \text{ fps}}{(528 \text{ } ^\circ\text{A})}) (\frac{28,498 \text{ Ps "Hg}}{(562.4 \text{ Ts } ^\circ\text{A})}) (\frac{29.92 \text{ "Hg}}{(0)}) = \underline{8275.624} \text{ dscfhr (or dscfm)}$$

$$(10A) \frac{8275.624 \text{ dscfhr} \div 60}{(1)} = \underline{137.927} \text{ dscfm (or dscfm)}$$

Note: Number in { } under blank lines denotes number of decimals to be used. If a blank calls for an answer already calculated, use the number of decimals previously specified for that answer.

WOODSTOVE DATA SHEET #4-1: INITIAL FILTER WEIGHTS (TARE WEIGHTS)

Into Dessicator: Date 1-20-09 Time 1149 By PDG Front Half X Back Half X

Manufacturer: Pall P/N. 60115 Size: 110 Lot.No.: 70726 Grade: A/E Glass

Filter #	First Wt	2009 Date	Time	By	Second Wt	Date	Time	By	Third Wt	2009 Date	Time	By
700	.6873	1-22	1331	GRP	.6877	1-23	1417	PDG				
701	.6871		1330	GRP	.6878		1419	PDG	.6877	1-26	1421	GRP
702	.6876		1329	GRP	.6825		1420	PDG	.6824	1-26	1420	GRP
703	.6761		1328	GRP	.6762		1421	PDG				
704	.6727		1327	GRP	.6732		1422	PDG				
705	.6833		1326	GRP	.6837		1423	PDG				
706	.6946		1325	GRP	.6948		1424	PDG				
707	.6773		1324	GRP	.6777		1425	PDG				
708	.6701		1323	GRP	.6702		1426	PDG				
709	.6799		1322	GRP	.6809		1427	PDG	.6806	1-26	1419	GRP
710	.6587		1321	GRP	.6590		1428	PDG				
711	.6654		1320	GRP	.6656		1429	PDG				
712	.6678		1319	GRP	.6692		1430	PDG				
713	.6864		1318	GRP	.6866		1431	PDG				
714	.6651		1318	GRP	.6655		1432	PDG				
715	.6741		1317	GRP	.6744		1433	PDG				
716	.6592		1316	GRP	.6590		1434	PDG				
717	.6531		1315	GRP	.6536		1435	PDG				
718	.6621		1314	GRP	.6623		1436	PDG				
719	.6769		1313	GRP	.6769		1437	PDG				
720	.6627		1312	GRP	.6628		1438	PDG				
721	.6567		1311	GRP	.6569		1439	PDG				
722	.6539		1310	GRP	.65340		1440	PDG				
723	.6552		1309	GRP	.6552		1441	PDG				
724	.6655		1308	GRP	.6656		1442	PDG				

Checked by A.T. Myer Date: 1/27/09 Time 1632

QA REWEIGH

BALANCE ROOM ENVIRONMENTAL CONDITIONS

Filter #	WT	Date	Time	By
703	.6761	1/27/09	1639	ATM
708	.6795		1640	ATM
715	.6799		1642	ATM

WB	DB	%RH	Date	Time	By
57	72	38	1-22-09	1138	ATM
58	25	33	1/24/09	1150	PDG
56	76	25	1-26-09	1359	GRP
58	72	31	1/27/09	1530	PDG

Post 1-22 1423 1-26  
 0.0000 0.0000 0.0000  
 100.0000 99.9994 99.9993 99.9993

WOODSTOVE DATA SHEET #4-2:  
INITIAL BEAKER WEIGHTS (TARE WEIGHTS)

Into Dessicator: Date: 01.26.09 Time: 15:38 By: QRP

Beaker #	First Wt.	2009 Date	Time	By	Second Wt.	2009 Date	Time	By	Third Wt.	Date	Time	By
20	73.3181	1-27	1532	PDG	73.3176	1-29	1459	QRP		1/30		
21	71.0021		1534	PDG	71.0018		1458	QRP				
22	71.8343		1535	PDG	71.8338		1457	QRP				
23	70.7390		1536	PDG	70.7389		1455	QRP				
27	72.3310		1538	PDG	72.3307		1500	QRP				
31	69.6672		1539	PDG	69.6669		1501	QRP				
32	53.6002		1541	PDG	53.5993		1502	QRP	53.5998		1305	PDG
37	53.7267		1542	PDG	53.7262		1504	QRP				
38	53.2525		1544	PDG	53.2516		1505	QRP	53.2520		1308	PDG
39	53.1509		1545	PDG	53.1493		1506	QRP	53.1496		1311	PDG
40	53.4626		1547	PDG	53.4622		1507	QRP				
41	52.8371		1549	PDG	52.8367		1508	QRP				
42	53.8699		1550	PDG	53.8692		1509	QRP	53.8696		1302	PDG

Checked By: APM Date: 2/1/09 Time: 12:10

QA REWEIGH

Beaker #	WT	Date	Time	By
20	73.3181	2/1/09	1215	ATM
31	69.6671		1217	ATM
42	53.8699		1219	ATM

BALANCE ROOM ENVIRONMENTAL CONDITIONS

WB	DB	%RH	2009 Date	Time	By
55	72	31	1/27	1530	PDG
58	77	29	1-29	1436	QRP
60	72	49	1/30	1258	PDG

1/27 1.29 1530 2/1 0.0000 0.0000 0.0000 0.0000  
09.6666 70.0000 69.6666 53.8666

POST

WOODSTOVE DATA SHEET #4-2:  
INITIAL BEAKER WEIGHTS (TARE WEIGHTS)

Blank done 12/10/07

Into Dessicator: Date: 10/12/07 Time: 0801 By: GRP

Beaker #	First Wt	Date	Time	By	Second Wt	Date	Time	By	Third Wt	Date	Time	By
22	71.8343	10/22/07	1358	GRP	71.8332	11/10/07	1938		71.8330	11-11-07	1748	Jm
24	73.2192		1400	GRP	73.2190	11/10/07	1940		73.2193	11-11-07	1746	Jm
25	72.6516		1401	GRP	72.6512	11/10/07	1944		Blank			
26	71.7895		1403	GRP	71.7888	11/10/07	1939		71.7896	11-11-07	1747	Jm
27	72.3316		1402	GRP	72.3314	11/10/07	1945					
28	70.5977		1404	GRP	70.5975	11/10/07	1941		70.5977	11-11-07	1745	Jm
39	53.1508		1405	GRP	53.1500	11/10/07	1942					
37	53.7237	11/10/07	1945	ATM	53.7238	11/11/07	1743	Jm				

Checked By: \_\_\_\_\_ Date: \_\_\_\_\_ Time: \_\_\_\_\_

QA REWEIGH

Beaker #	WT	Date	Time	By
27	72.3315	11-11	1740	Jm
25	72.6515	11-11	1741	Jm
39	53.1509	11-11	1744	Jm

BALANCE ROOM ENVIRONMENTAL CONDITIONS

WB	DB	%RH	Date	Time	By
57	68	50	10/22/07	1344	GRP
			11/10		

Post weighing LSD 0.0000g  
 0.0000g  
 0.0000g

WOODSTOVE DATA SHEET #4-3: GC CANT FINAL WEIGHTS

60 ml.

FINAL BEAKER WEIGHTS

Beaker #	Into Dessic	Date	Time	By	First	Date	Time	By	Second	Date	Time	By	Third	Date	Time	By
23	70.7582	2/21	1542	ATM	70.7578	2/22	1237	Jim	70.7566	2/23	1408	PDG	70.7553	2/24	1010	ATM
					Fourth											
					70.7559	2/25	1132	PDG	70.7558	2/26	1329	ARP				

2009

FINAL FILTER WEIGHTS

Filter #	Into Dessic	Date	Time	By	First	Date	Time	By	Second	Date	Time	By	Third	Date	Time	By
F 710	.6699	2/18	1850	ATM	.6691	2/19	1321	ARP	(.6690)	2/20	1046	PDG				
R 709	.6656	2/18	1850	ATM	.6654	2/19	1325	ARP	(.6654)	2/20	1030	PDG				

QA REWEIGH: FINAL WEIGHTS

Date	Beaker #	Final Wt	By
Date	Filter #	Final WT	By

SCALE ROOM ENVIRONMENTAL CONDITIONS

Weighing Session	Date	Time	By	WB	DB	%RH
2009						
1	2-19	1218	ARP	56	73	32
2	2/20	1018	PDG	57	74	33
3	2/22	1222	ATM	47	59	37
4	2/23	1406	PDG	58	20	48
5	2/24	0953	ATM	59	75	35

SCALE ROOM ENVIRONMENTAL CONDITIONS

6	2/25	1123	PDG	60	24	38
7	2/26	1258	JRP	55	70	36
8						
9						
Comments						

Ac done  
lot #  
041648

Blank  
done  
12/10/07

WOODSTOVE DATA SHEET #4-3: CONSTANT FINAL WEIGHTS

TRUS 776512

WST5-Form 9, Pg. 1, Rev. 4/90  
Unit Kumukahi Ashwood  
Run # 4328-3  
Date: 2/10/09

**FINAL BEAKER WEIGHTS**

Beaker #	Into Dessic	2007		Time	By	First	Date	Time	By	Second	Date	Time	By	Third	Date	Time	By	
		Date	Date															
25	L	12/12	12/12	1546	JRP	72.6508	12/13	1342	JRP	92.6511	12/14	1347	JRP					

**FINAL FILTER WEIGHTS**

Filter #	Into Dessic			Time	By	First	Date	Time	By	Second	Date	Time	By	Third	Date	Time	By	
		Date	Date															

**QA BEWZICH: FINAL WEIGHTS**

Date	Beaker #	Final Wt	By

**SCALE ROOM ENVIRONMENTAL CONDITIONS**

Weighing Session	Date	Time	By	WB	DR	ZRH
1	12/13	1207	JRP	55	73	29
2	12/14	1321	JRP	57	75	31
3						
4						

**SCALE ROOM ENVIRONMENTAL CONDITIONS**

Comments						
6						
7						
8						
9						

SCALE: SARTORIUS  
 MODEL: CP224S  
 SN: 17050374

WOODSTOVE DATA SHEET 4-4 SCALE QC RECORD SHEET

FROM: 9/27/2007  
 THROUGH: 12/7/2007

Level	Recali	130 g	100 g	10 g	1.0 g	100 mg	20 mg	Date	Time	Tech	Wet Bulb	Dry Bulb	% RH
✓	N	129.9998	99.9998	10.0000	1.0000	0.1000	0.0199	9/27/07	1402	GRP	55	67	45
✓	Y	129.9995	99.9996	10.0001	1.0000	0.1000	0.0200	9/28/07	1335	GRP	57	69	46
✓	Y	129.9996	99.9996	9.9999	1.0000	0.1000	0.0200	10/1/07	1505	ATM	58	70	48
✓	N	129.9995	99.9996	10.0000	1.0001	0.1000	0.0199	10/2/07	1611	GRP	56	68	46
✓	N	129.9997	99.9997	9.9999	1.0001	0.1000	0.0199	10/3/07	1122	GRP	56	68	46
✓	N	129.9996	99.9996	10.0000	1.0000	0.0999	0.0199	10/4/07	0925	GRP	55	67	45
✓	Y	129.9996	99.9996	10.0000	1.0000	0.1000	0.0199	10/5/07	0750	GRP	51	62	45
✓	Y	129.9997	99.9997	9.9999	1.0000	0.1000	0.0199	10/5/07	1313	GRP	56	69	43
✓	Y	129.9996	99.9996	10.0000	1.0001	0.1001	0.0200	10/9/07	1505	ATM	38	41	44
✓	N	129.9996	99.9997	10.0000	1.0001	0.1001	0.0200	10/12/07	1259	ATM	50	70	48
✓	Y	129.9995	99.9996	9.9999	1.0000	0.1000	0.0199	10/22/07	1344	GRP	57	68	50
✓	Y	129.9996	99.9997	9.9999	1.0000	0.1000	0.0199	10/29/07	1338	GRP	53	63	50
✓	N	129.9995	99.9995	10.0000	1.0000	0.1000	0.0200	10/31/07	0933	ATM	56	70	40
✓	Y	129.9996	99.9997	10.0000	1.0000	0.1000	0.0199	10/31/07	1457	GRP	55	70	36
✓	Y	129.9996	99.9996	9.9999	1.0000	0.1000	0.0199	10/31/07	1528	GRP	57	75	30
✓	Y	129.9996	99.9996	9.9999	1.0000	0.0999	0.0199	11/2/07	1238	GRP	50	67	33
✓	Y	129.9996	99.9996	10.0000	1.0001	0.1000	0.0199	11/5/07	0730	GRP	57	73	35
✓	Y	129.9996	99.9997	10.0000	1.0000	0.1001	0.0201	11/9/07	1550	ATM	58	70	48
✓	N	129.9996	99.9997	10.0000	1.0000	0.1000	0.0200	11/10/07	1885	ATM	58	71	44
✓	Y	129.9997	99.9997	9.9999	1.0000	0.1000	0.0199	11/11/07	1810	ATM	55	69	39
✓	N	129.9997	99.9996	9.9999	1.0000	0.1000	0.0199	11/21/07	0822	GRP	54	67	41
✓	N	129.9996	99.9996	10.0000	1.0000	0.1000	0.0199	11/23/07	1226	ATM	58	72	41
✓	N	129.9998	99.9997	9.9999	0.9999	0.1000	0.0200	11/14/07	1710	GRP	58	73	39
✓	Y	QC Services Audit 11/17/07											
✓	Y	129.9997	99.9997	10.0000	1.0000	0.1000	0.0200	11/15/04	1350	ATM	59	72	45
✓	N	129.9996	99.9996	9.9999	0.9999	0.1000	0.0200	11/16/07	1600	GRP	58	71	41
✓	N	129.9996	99.9996	10.0000	1.0000	0.1000	0.0199	11/19/07	1358	ATM	740	74	43
✓	Y	129.9996	99.9997	10.0000	1.0000	0.1000	0.0200	11/19/07	1143	ATM	56	70	40
✓	Y	129.9995	99.9996	10.0000	1.0000	0.1000	0.0199	11/20/07	1416	GRP	54	69	35
✓	N	129.9996	99.9996	10.0000	1.0000	0.1000	0.0200	11/21/07	1110	ATM	57	70	44
✓	N	129.9995	99.9996	10.0000	1.0000	0.1000	0.0199	12/3/07	0730	GRP	55	69	40
✓	N	129.9996	99.9996	10.0000	1.0000	0.0999	0.0200	12/6/07	1125	ATM	54	67	44
✓	Y	129.9996	99.9996	10.0000	1.0000	0.1000	0.0200	12/17/07	1348	GRP	55	69	40



SCALE: SARTORIUS  
 MODEL: CP224S  
 SN: 17050374

WOODSTOVE DATA SHEET 4-4 SCALE QC RECORD SHEET

FROM: 12/2/04  
 THROUGH: 2/3/08

Level	brated	130 g	100 g	10 g	1.0 g	100 mg	20 mg	Date	Time	Tech	Wet Bulb	Dry Bulb	% RH
✓	N	129.9996	99.9996	10.0000	1.0000	0.1000	0.0200	12/8	12:15	ATM	57	73	35
✓	N	129.9996	99.9996	10.0000	1.0000	0.1001	0.0200	12/8	19:10	ATM	57	72	38
✓	N	129.9997	99.9996	10.0000	1.0000	0.1000	0.0199	12/9	19:35	ATM	55	72	31
✓	Y	129.9996	99.9996	10.0000	1.0000	0.1000	0.0200	12/10	19:53	ATM	56	72	34
✓	N	129.9997	99.9997	10.0000	1.0000	0.1000	0.0199	12/11	16:18	GRP	57	76	28
✓	N	129.9997	99.9996	10.0000	1.0000	0.0999	0.0199	12/12	5:05	GRP	56	74	30
✓	N	129.9997	99.9996	9.9999	0.9999	0.1000	0.0199	12/13	3:07	GRP	55	73	29
✓	N	129.9996	99.9996	9.9999	0.9999	0.1000	0.0199	12/14	13:21	GRP	57	75	31
✓	N	129.9996	99.9996	9.9999	1.0001	0.1000	0.0199	12/15	16:02	GRP	57	75	31
✓	Y	129.9997	99.9997	9.9999	1.0000	0.1000	0.0199	12/17	08:17	GRP	55	73	29
✓	N	129.9998	99.9998	9.9999	1.0000	0.1000	0.0199	12/18	08:53	GRP	58	75	34
✓	N	129.9997	99.9997	10.0000	1.0000	0.1000	0.0199	12/19	08:12	GRP	55	72	31
✓	Y	129.9997	99.9997	10.0000	1.0001	0.0999	0.0199	12/20	09:16	GRP	57	71	41
✓	Y	129.9998	99.9997	10.0000	1.0000	0.1000	0.0199	12/21	10:85	ATM	55	70	36
✓	N	129.9997	99.9996	10.0000	1.0000	0.1000	0.0200	12/22	14:54	ATM	54	66	44
✓	N	129.9996	99.9998	10.0000	1.0000	0.1000	0.0200	12/23	09:15	ATM	57	70	44
✓	N	129.9996	99.9996	9.9999	1.0000	0.1000	0.0199	12/26	12:30	ATM	57	70	44
✓	N	129.9997	99.9997	10.0000	1.0000	0.1000	0.0200	12/27	10:30	ATM	56	72	41
✓	N	129.9998	99.9997	9.9999	1.0000	0.1000	0.0200	1/8/08	13:40	GRP	54	68	38
✓	N	129.9997	99.9997	10.0000	1.0001	0.1000	0.0200	1/9/08	07:42	GRP	55	70	36
✓	N	129.9998	99.9998	10.0000	1.0000	0.1000	0.0199	1/11/08	10:40	ATM	59	73	42
✓	Y	129.9996	99.9997	10.0000	1.0000	0.1000	0.0199	1/16/08	12:21	GRP	51	72	18
✓	N	129.9999	99.9998	10.0000	1.0000	0.1000	0.0199	1/17/08	12:37	GRP	56	71	37
✓	N	129.9998	99.9998	10.0000	1.0000	0.0999	0.0200	1/18/08	11:16	GRP	56	71	37
✓	Y	129.9995	99.9996	9.9999	1.0001	0.1000	0.0199	1/21/08	14:26	GRP	56	72	34
✓	N	129.9995	99.9996	10.0000	1.0001	0.1000	0.0199	1/24/08	15:13	GRP	56	71	37
✓	Y	129.9996	99.9996	9.9999	1.0000	0.1000	0.0199	1/23/08	08:05	GRP	54	69	36
✓	Y	129.9996	99.9996	10.0000	1.0000	0.1000	0.0200	1/24/08	07:58	GRP	54	70	33
✓	N	129.9998	99.9997	10.0000	1.0000	0.1000	0.0199	1/24/08	14:50	GRP	56	71	37
✓	N	129.9997	99.9996	10.0000	1.0000	0.1000	0.0200	1/31/08	15:05	GRP	55	69	38
✓	N	129.9997	99.9996	10.0000	1.0000	0.1000	0.0199	2/1/08	10:49	GRP	54	69	36
✓	N	129.9996	99.9996	9.9999	1.0000	0.1000	0.0199	2/20/08	16:20	ATM	56	72	41
✓	N	129.9996	99.9996	10.0000	1.0000	0.1000	0.0200	2/3/08	17:10	ATM	57	70	44

WOODSTOVE DATA SHEET 4-4 ANALYTICAL BALANCE QC RECORD SHEET

SCALE: SARTORIUS

FROM: 12/20/08

MODEL: CP222AS

THROUGH: 2/17/09

SN: 17050374

Level	Recall		140 g		100 g		10 g		1.0 g		100 mg		20 mg		Wet		Dry	
	brated	Weights	Weight	Weight	Weight	Weight	Weight	Weight	Weight	Weight	Weight	Weight	Weight	Weight	Weight	Tech	Bulb	Bulb
✓	N	139.9993	99.9993	9.9993	9.9999	1.0000	0.1000	0.0199	0.0199	1420	ARM	58	72	42				
✓	N	139.9995	99.9995	9.9995	9.9999	1.0000	0.1000	0.0199	0.0199	1057	GRP	60	76	38				
✓	N	139.9994	99.9994	9.9994	9.9999	1.0000	0.1000	0.0200	0.0200	1019	ATM	59	72	43				
✓	N	139.9994	99.9994	9.9994	9.9999	1.0000	0.1000	0.0200	0.0200	1142	ARM	59	72	45				
✓	N	139.9994	99.9994	9.9994	9.9999	1.0000	0.1000	0.0200	0.0200	1050	ARM	60	73	37				
✓	N	139.9994	99.9994	9.9994	9.9999	1.0000	0.1000	0.0199	0.0199	1157	PDG	58	75	34				
✓	N	139.9994	99.9994	9.9994	9.9999	1.0000	0.1000	0.0199	0.0199	1045	ATM	60	75	37				
✓	N	139.9995	99.9995	9.9995	9.9999	1.0000	0.1000	0.0199	0.0199	1530	GRP	58	70	48				
✓	N	139.9994	99.9994	9.9994	9.9999	1.0000	0.1000	0.0199	0.0199	1356	PDG	60	72	49				
✓	Yes	139.9993	99.9993	9.9993	9.9999	1.0000	0.1000	0.0200	0.0200	1023	PDG	58	72	42				
✓	Yes	139.9993	99.9993	9.9993	9.9999	1.0000	0.1000	0.0199	0.0199	1128	JRP	55	72	31				
✓	Yes	139.9994	99.9994	9.9994	9.9999	1.0000	0.1000	0.0199	0.0199	0845	PDG	59	75	38				
✓	NO	139.9993	99.9993	9.9993	9.9999	1.0000	0.1000	0.0200	0.0200	0825	JRP	58	74	37				
✓	Yes	139.9994	99.9994	9.9994	9.9999	1.0000	0.1000	0.0199	0.0199	1212	PDG	57	72	38				
✓	NO	139.9992	99.9992	9.9992	9.9999	1.0000	0.1000	0.0199	0.0199	1420	GRP	59	75	37				
✓	NO	139.9994	99.9994	9.9994	9.9999	1.0000	0.1000	0.0199	0.0199	1126	GRP	57	74	37				
✓	Yes	139.9993	99.9993	9.9993	9.9999	1.0000	0.1000	0.0199	0.0199	0950	PDG	58	74	34				
✓	Yes	139.9993	99.9993	9.9993	9.9999	1.0000	0.1000	0.0199	0.0199	1230	PDG	56	71	37				
✓	NO	139.9993	99.9993	9.9993	9.9999	1.0000	0.1000	0.0199	0.0199	1613	JRP	57	73	35				
✓	NO	139.9994	99.9994	9.9994	9.9999	1.0000	0.1000	0.0200	0.0200	1130	ATM	57	72	38				
✓	NO	139.9993	99.9993	9.9993	9.9999	1.0000	0.1000	0.0199	0.0199	1150	PDG	58	75	33				
✓	YES	139.9992	99.9992	9.9992	9.9999	1.0000	0.1000	0.0200	0.0200	1359	JRP	56	70	25				
✓	NO	139.9994	99.9994	9.9994	9.9999	1.0000	0.1000	0.0200	0.0200	1530	PDG	57	72	31				
✓	NO	139.9993	99.9993	9.9993	9.9999	1.0000	0.1000	0.0200	0.0200	1452	ATM	61	75	41				
✓	YES	139.9993	99.9993	9.9993	9.9999	1.0000	0.1000	0.0199	0.0199	1130	GRP	58	77	29				
✓	NO	139.9995	99.9995	9.9995	9.9999	1.0000	0.1000	0.0199	0.0199	1256	PDG	60	72	49				
✓	Yes	139.9993	99.9993	9.9993	9.9999	1.0000	0.1000	0.0199	0.0199	1200	ATM	59	74	37				
✓	NO	139.9993	99.9993	9.9993	9.9999	1.0000	0.1000	0.0199	0.0199	1350	GRP	58	77	29				
✓	Yes	139.9995	99.9995	9.9995	9.9999	1.0000	0.1000	0.0199	0.0199	1118	PDG	59	72	45				
✓	NO	139.9995	99.9995	9.9995	9.9999	1.0000	0.1000	0.0199	0.0199	1150	GRP	57	74	33				
✓	NO	139.9994	99.9994	9.9994	9.9999	1.0000	0.1000	0.0200	0.0200	1015	ATM	49	70	19				
✓	NO	139.9994	99.9994	9.9994	9.9999	1.0000	0.1000	0.0199	0.0199	1501	PDG	61	78	36				
✓	NO	139.9993	99.9993	9.9993	9.9999	1.0000	0.1000	0.0200	0.0200	1439	JRP	56	72	35				

SCALE: SARTORIUS  
 MODEL: CP224S  
 SN: 17050374

WOODSTOVE DATA SHEET 4-4 ANALYTICAL BALANCE QC RECORD SHEET

FROM: 2/10/09  
 THROUGH:

Level	Recali	140 g	100 g	10 g	1.0 g	100 mg	20 mg	Date	Time	Tech	Wet Bulb	Dry Bulb	& RH
brated	Weights	Weight	Weight	Weight	Weight	Weight	Weight				Bulb	Bulb	
Y	139.9993	99.9993	9.9999	1.0000	0.1000	0.0199	0.0199	2/10/09	1600	ATM	55	70	26
Y	139.9993	99.9994	9.9999	1.0000	0.1000	0.0199	0.0199	2/19/09	1248	JRP	56	73	32
Y	139.9993	99.9994	9.9999	0.9999	0.1000	0.0199	0.0199	2/20/09	1018	PDG	57	74	33
Y	139.9993	99.9994	10.0000	1.0000	0.1000	0.0200	0.0200	2/21/09	1519	ATM	60	77	35
Y	139.9993	99.9993	9.9999	1.0000	0.1000	0.0199	0.0199	2/22/09	1222	ATM	47	59	37
Y	139.9994	99.9994	9.9999	0.9999	0.1000	0.0199	0.0199	2/23/09	1406	PDG	58	70	48
Y	139.9994	99.9997	9.9999	1.0000	0.1000	0.0200	0.0200	2/24/09	0953	ATM	59	76	35
Y	139.9995	99.9995	9.9999	1.0000	0.1000	0.0199	0.0199	2/25/09	123	PDG	60	76	38
Y	139.9994	99.9994	9.9999	1.0000	0.1000	0.0199	0.0199	2/26/09	1258	JRP	55	70	36
Y	139.9993	99.9993	9.9999	1.0001	0.1001	0.0200	0.0200	2/29/09	1320	ATM	57	74	33
Y	139.9995	99.9995	9.9999	0.9999	0.1000	0.0199	0.0199	3/3/09	1431	PDG	59	76	35
Y	139.9993	99.9995	9.9999	1.0000	0.1000	0.0199	0.0199	3/4/09	1556	JRP	56	70	40
Y	139.9994	99.9994	9.9999	1.0001	0.1001	0.0200	0.0200	3/5/09	1350	ATM	60	73	40
Y	139.9993	99.9993	9.9999	1.0000	0.1000	0.0200	0.0200	3/7/09	0850	ATM	57	71	41
Y	139.9993	99.9993	10.0000	1.0001	0.1000	0.0200	0.0200	3/8/09	1323	ATM	55	70	36
Y	139.9993	99.9993	9.9999	1.0000	0.1000	0.0199	0.0199	3/10/09	1212	PDG	80	75	10

Woodstove Particulate  
Catch Processing Sheet  
Woodstove Data Sheet #5  
EPA M5G-1

Unit: Kuma Ashwood  
Run: EPA 3  
Date: 2/18/09  
Technicians: ATM  
Revised 1/16/98-Data Sheet #5

Filters

Filter # (Front) 710 Beaker # 23  
Final Wt. .6690 g MI 60  
Tare Wt. .6590 g Desc. Acetone  
Net Wt. .0100 g

Final Wt. 70.7558 g 70.7553  
Tare Wt. 70.7389 g  
Net Wt. .0169 g 16.4

Filter # (Rear) 709 Beaker # \_\_\_\_\_  
Final Wt. .6654 g MI \_\_\_\_\_  
Tare Wt. .6806 g Desc. \_\_\_\_\_  
Net Wt. -.0152 g

Final Wt. \_\_\_\_\_ g  
Tare Wt. \_\_\_\_\_ g  
Net Wt. \_\_\_\_\_ g

Acetone Blank Calculation:

Blank Date: 12/8/07

Blank Beaker # 25 Final Wt. 72.6511 g  
MI 50 Tare Wt. 72.6512 g  
Desc. Acetone Net Wt. -0.0001 g = 0.0000  
0.0000 g ÷ 50 ml = 0.00000 g/ml

Blank Residue Value Calculation:

0.00000 g/ml acetone X 60 ml acetone = 0.0000 g  
Blank Residue Value

Total Particulate Catch Calculation

Filter: .0100 g  
Filter: -.0152 g  
Beakers: .0169 g - 0.0000 g = .0169 g  
Total Catch Blank Residue Value  
Total Catch = .0117 g

Unit Kuma Ashwood  
 Run # EPA 3  
 Date 2/18/09  
 Technician ATM JRP PDG  
 WST6-Form1, Rev8/96

MISCELLANEOUS TEST DATA  
 WOODSTOVE DATA SHEET #8

Useable Firebox Dimensions: See QC Section Useable Volume: 2.094 ft<sup>3</sup>

Dilution Tunnel Draft (If applicable): Start .000 Stop .000 "H<sub>2</sub>O

Test Chamber Air Velocity: Start: 00.0 Stop: 000 Avg: 00.0 ft/min

Wet Bulb/ Start: WB: 59 °F DB: 70 °F 0.85 % Amb Moisture 52 %RH

Dry Bulb Stop: WB: 60 °F DB: 71 °F 0.90 % Amb Moisture 52 %RH

$\bar{X} = 0.875$  % Ambient Moisture  $\bar{X} = 52.0$  % Relative Humidity (RH)

Empty Stove Wt: 440.2 lbs.

Empty Stove Wt with Stack (Inc. Oil Seal) Wet: 763.9 lbs. Dry: 763.8 lbs. 765.6

Empty Stove Wt with Stack and Ash Ash: — lbs. Total: — lbs.

Kindling Wt. Total 4.9 lbs. Paper: .3 lbs. Wood: 4.6 lbs.

Pre Burn Fuel Wt. 10.360 + 12.574 + 10.676 Total: 33.610 lbs. ✓

Total Kindling and Pre Burn Fuel Wt 38.510 lbs. ✓

Coal Bed Wt-lbs: Range (3.3 - 2.7) 767.1 - 766.5 lbs. Actual 766.7 lbs. 2.9

Allowable Amount of Charcoal that can be removed:

Coal Bed Wt. Range  $\left( \frac{3.3}{\text{Upper Wt.}} + \frac{2.7}{\text{Lower Wt.}} / 2 \right) \times .25 = 0.75$  lbs. 0.7 ✓

Test Fuel Wt-lbs: Ideal 14.7 lbs. Range: 16.1 - 13.2 lbs. Actual: 13.308 lbs.

Test Fuel Size (pcs.) (.75 x 1.5 x 5" Flanges) 1,378 lbs 16 Pcs.

2 x 4's x 16.375" 3 Pcs 5.956 lbs. 44.76 %

4 x 4's x 16.375" 2 Pcs 7.352 lbs. 55.24 %

5.0343 kg ✓

Est. Dry Burn Rate (Kg/Hr.)  $\frac{13.308 - (13.308 \times .16602)}{2.2046} \times \frac{60}{245} = 1.233$  Est. Dry Burn Rate (Kg/Hr)

Est EPA Heat Output (H<sub>O<sub>E</sub></sub>) (19,140) x  $\frac{63}{100} \times 1.233 = 14,866$  Est Heat Output (H<sub>O<sub>E</sub></sub>) BTU's/Hr

Comments:

Stove Operating Data  
Woodstove Test Data Sheet #9  
Cold Start

Unit: KUMA Ashwood  
Run: EPA 3  
Date: 2/18/09  
Technician(s): ATM JRP R06  
Data Sheet #9 - Rev 1/98-Pg.1

Fire Started: 08:08

*2.561 (thru rods)*  
Warm up and Preburn: Primary Air: Wide open from ignition until the start of preburn when the primary air control(s) was (were) adjusted to the run setting of .553". At the run setting until the start of the test.

Secondary Air: No Controls. Naturally Drafted

Secondary Burn/Bypass: N/A

Charcoal Bed Preparation: Broke up, raked and leveled the coal bed prior to the addition of each warm up/pre burn fuel charge. Starting 1:30 before the start of the test, broke up, raked and leveled the coal bed. In stove for 32 seconds.

Test: Door wide open during loading 0 min 58 sec, then closed.

Primary Air: Wide open from the start of the test (0:00) until 4:45. Adjusted to the run setting of .553" open between 4:45 and 5:00. At the run setting of .553" open at 5:00 into the run.

Secondary Air:  
No Controls. Naturally Drafted.

Secondary Burn/Bypass: N/A

Fan: OFF. Fan Confirmation Test

Test Run Anomalies: None. Great Run.

WOODSTOVE OPERATING DATA  
 WOODSTOVE DATA SHEET #9A-1

Wood Data: Kindling: A mix of the below grades

	Size	Mill	Grade	Species
Pre Burn	2X4	Forest Grove	# 2, Std & BTR	D. Fir, Sfc. Gnw
Test Fuel	2X4	Forest Grove	# 2, Std & BTR	D. Fir, Sfc, Gnw
	4X4	Forest Grove	No. 1	D. Fir, Sfc, Gnw

All grades WCLB Rules unless otherwise noted.

Warm up Information:

1st Warm up/Pre Burn Fuel charge (10.360 lbs) added at 0824.  
 2nd Warm up/Pre Burn Fuel charge (12.574 lbs) added at 0917.  
 3rd Warm up/Pre Burn Fuel charge (10.676 lbs) added at 1023.  
 4th Warm up/Pre Burn Fuel charge (\_\_\_\_\_ lbs) added at \_\_\_\_\_.  
 5th Warm up/Pre Burn Fuel charge (\_\_\_\_\_ lbs) added at \_\_\_\_\_.  
 6th Warm up/Pre Burn Fuel charge (\_\_\_\_\_ lbs) added at \_\_\_\_\_.  
 7th Warm up/Pre Burn Fuel charge (\_\_\_\_\_ lbs) added at \_\_\_\_\_.  
 8th Warm up/Pre Burn Fuel charge (\_\_\_\_\_ lbs) added at \_\_\_\_\_.

1<sup>st</sup> Rick 4-12" 4-16" 2X4's      3<sup>rd</sup> Rick 4-12", 3-16" 2X4's  
 2<sup>nd</sup> Rick 8-16" 2X4's

The coals were scooped out of the stove immediately prior to adding the 3<sup>rd</sup> pre burn/warm up fuel charge. The stove lost 0.1 lbs. 2.0 lbs. of coals were put back in the stove after the scoop.

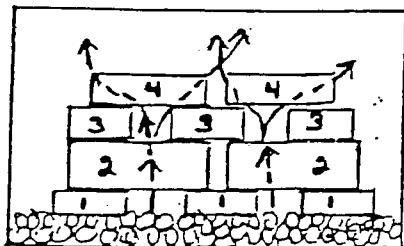
All pre burn/warm up fuel pieces were either 12 or 16 inches long. All preburn pieces/fuel charges were "ricked" in the stove. The pieces in the bottom layer in each rick contained 2 pcs that were 12 or 16 inches long and were loaded flat and perpendicular to the door. The pieces in the second layer in each rick were loaded on their side (edge) approximately parallel to the door and contained 3 or 4 pcs 16 inches long. The third layer (and fourth layer if present) was loaded flat, perpendicular to the door and contained 2 pcs 12 or 16 inches long. The majority of the pieces in each rick were in the second layer which had an approximate 0.5-1.0" space between pieces. (The loading directions indicate the direction of the longest dimension on each piece relative to the loading door opening.) Each pre burn/warm up fuel charge normally weighs within the weight range allowed for the actual test fuel charge.

WOODSTOVE OPERATING DATA  
WOODSTOVE DATA SHEET #9A-2

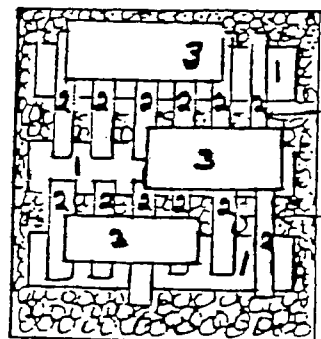
Unit: Kuma Ashwood  
Run # EPA 3  
Date 2/18/09  
Technician ATM  
Page 2 of         
WST7-Form2-A, Rev 6/90

Warm up Information (cont.):

Each warm up/preburn fuel charge was ricked in exactly (as much as possible) the same manner and the weight of each rick was usually within the allowable weight range for the test fuel charge. The physical arrangement and alignment of each rick was designed to accomplish three (3) things: (1) The bottom layer was nestled firmly into the coal bed and was as close to being level with the bottom of the stove as possible, thus providing a stable loading platform for the rest of the rick, keeping it in a ricked state (as opposed to a col-lapsed or fallen down state) until the rick reached the charcoal stage and sags or collapses of its own accord. (2) It enhances the flow of primary air through the ricked preburn fuel charge, for the primary air would flow through the spaces between the pieces in the first layer and then up through the spaces between the pieces in the second, third and, if present, fourth layers. (3) It maximized, as much as possible, the surface to volume ratio of each preburn fuel charge, thereby allowing the fire immediate access to as much wood surface as possible and, thereby, insuring uniform charcoalization. All three of these enhance combustion and so get the stove as hot as possible during the warm up period, thereby maximizing the amount of heat (BTU's) stored in the stove. The actual preburn was not started until the stove surface temperatures had maximized and stabilized, thus indicating that the amount of heat stored in the stove had peaked. For this stove, the thermal storage was monitored using the Stove Top T/C surface temperature(s) and the peak value(s) 991 obtained were 1088 °F. 1088



Front View



Top View

The arrows indicate the direction of the air flow through the rick.

The primary air was adjusted to the run setting of 0.553" open 4.7 lbs above the upper charcoal bed weight.

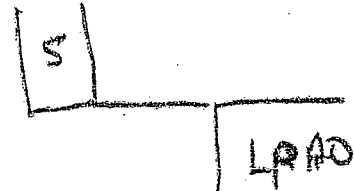


WOODSTOVE OPERATING DATA  
WOODSTOVE DATA SHEET #9A-3

Unit Kuma Ashwood  
Run # EPA 3  
Date 2/18/09  
Technician ATM  
Page 3 of       
WST5-Form2-Rev11/89

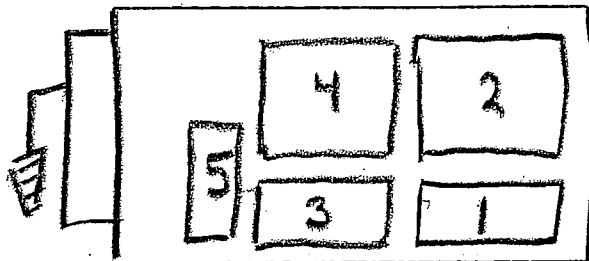
Additional Comments:      Test Start Sequence: ① Adjusted Primary Air Control to Wide Open. ② Opened Door. ③ Loaded fuel. ④ Cleared coals away from in front of the LPAD. ⑤ Closed Door.

TOTAL ELAPSED Time: 0:58  
Photo @ 1:30



Test Fuel Charge Loading Information:

Test Fuel Charge and Loading Sequence Diagram



SIDE of stove view

4 X 4's: 2, 4  
2 X 4's: 1, 3 & 5  
Loading Sequence: 1, 2, 3, 4 & 5 last  
Driest Pcs in Load 5, 3

Loaded the test fuel charge on an essentially level, Medium sized, average to hot coal bed (in appearance, color and temperature for a Med Low (1.0-1.25) burn rate. Load: 0:58 Ignition: 0:50  
on Left end of 5  
1:00 VC ↑ baffle  
1:30 Secondaries igniting  
2:30 Great Start  
4:45 - 5:00 PAC adjusted to the run setting.  
5:00 Maintained a hot pocket of coals under and behind p.c. 5 with a VC up to the baffle, + Secondaries full width of 5. 11.3/51 (%CO<sub>2</sub>/%CO)  
5:46 Secondaries centering (decreasing)  
7:50      "      increasing

Unit: Kuma Ashwood  
 Run: EPA 3  
 Date: 2/18/09  
 Technician: ATM JRP PDG  
 WST1-Form7-Rev11/89

FUEL MOISTURE  
 WOODSTOVE TEST DATA SHEET #10

5 kg. = 11.024 lbs. 1 kg. = 2.204 lbs

Room Temperature: 61.5 °F Correction Factor: +1.0

NOTE: Record readings to the nearest 0.5% moisture  
 Uncor Values are corrected for temperature: Yes   
 Time Test Fuel Moisture Readings taken at: 8:39 No  
 Calibration Checks: X 12.0 Y 11.6 22.0 22.1

Pc #	Dimen	Use	Top		Bottom		Side		Piece Avg Corrected
			Uncor	Cor	Uncor	Cor	Uncor	Cor	
1	3000	K	9	9.5	9	9.5	8.5	8.95	9.317
2									
3									
4	2x4-8'	P	18.5	19.8	20.5	20	18	19.2	20.333
5			18	19.2	22	23.7	21	22.6	21.833
6			20.5	21.4	21.5	23.1	22	23.7	22.733
7			22	23.7	19.5	20.9	20	21.4	22.000
8	V	V	19.5	20.9	20	21.4	20	21.4	21.233
9									108.132
10									
11									
12	2x4-16 1/2'	T	20	21.4	19.5	20.9	19.5	20.9	21.067
13			18	19.2	18	19.2	18	19.2	19.200
14	V	V	18	19.2	18	19.2	18	19.2	19.200
15									
16	4x4-16 1/2'	T	19	20.3	18.5	19.8	20.5	22.0	20.700
17	V	V	18	19.2	17.5	18.6	19.0	20.3	19.367
18									99.534
19									
20	SPACERS	T	18	19.2	19	20.3	19	20.3	19.933

2.040  
 1.522  
 3.534  
 3.484  
 1.378

Kindling	Pretest Fuel	Test Load
9.317%	21.6264%	19.9068%
8.523%	17.781%	16.602%

% Moisture - Dry Basis:  
 % Moisture - Wet Basis:  
 13.308  
 7.352

To obtain Wet from Dry:  $\frac{100 \times \% \text{ Dry Rdg.}}{100 + \% \text{ Dry Rdg.}} = \% \text{ Moisture, Wet Basis}$   
 10.360

Acceptable Ranges: 16-20% wet; 19-25% dry  
 (17.5 - 22.5 on Meter [Uncor reading] at 70°F)  
 2 12.574  
 3 10.676

Key for Use: K= Kindling P= Pretest Fuel T= Test Fuel

WOOD DENSITY DETERMINATION  
WOODSTOVE TEST DATA SHEET #11

Unit: Kuma Ash wood  
Run#: EPA 3  
Date: 2/18/09  
Technician: A.T. Myren  
WST2-form11-Rev 6/90

Wood Piece: 2x4 Nominal Dimensions: 3.5" x 3.5" x 1.5"  
Depth (D): 3.795 cm  
Width (W): 8.765 cm  
Length (L): 8.780 cm  
8.745 cm  
8.769 cm  
8.775 cm  
Length  $\bar{X}$  = 8.76725 cm  
Volume: 291.627 cm<sup>3</sup>  
(D X W X L)

MOISTURE: Room Temperature: 61.5 °F Correction Factor: +1.0  
Uncorrected Meter Readings Corrected for temperature: Yes  No

NOTE: Record moisture meter readings to the nearest 0.5%

	Uncor	Cor	%
Top:	19	20.3	%
Bottom:	19	20.3	%
Side:	18	19.2	%
$\bar{X}$ :		19.983	%

Avg % Moisture (Dry) 19.983 %  
Avg % Moisture (Wet) 16.620 %  
Scale: Leveled In  Out   
Zeroed: In  Out

Wet Weight: 126.7 g Dry Weight: 109.3 g

% Moisture Dried Basis: 13.733 %  
[1 - (Dry Wt ÷ Wet Wt)] X 100

Into Dryer Date 2/18/09 Time 1517 Temp 190 °F  
Out of Dryer Date 3/2/09 Time 0915 Temp 192 °F  
(Minimum Time in Dryer: 24 hrs.) Minimum Dryer Temp 100°C (212°F)

Density = 109.3 g (dry wt) ÷ 291.627 cm<sup>3</sup> (volume) = 0.3748 g/cm<sup>3</sup>

Pellet Fuel Moisture Content Determination

Tare Beaker Wt. \_\_\_\_\_ g  
Wet Wt: \_\_\_\_\_ g - \_\_\_\_\_ g = \_\_\_\_\_ g  
Gross Wet Wt. Tare Beaker Wt. Net Wet Wt.  
Dry Wt: \_\_\_\_\_ g - \_\_\_\_\_ g = \_\_\_\_\_ g  
Gross Dry Wt. Tare Beaker Wt. Net Dry Wt.

% Moisture Dried Basis: \_\_\_\_\_ %  
[1 - (Net Dry Wt ÷ Net Wet Wt.)] X 100

Pre Burn Test wt.  
4.7 lbs. @ 771.8 lbs.  
Test Start wt. Range WST2-Form 16  
7671 - 7665 lbs.

PRE BURN DATA  
RECORD SHEET #13  
WST2-Form 16

BAFD Pressure  
28.5

Unit: Kuma Ashwood  
Run: EPA 3  
Page: 1 of 1

Date: 2-18-09

Technician(s): AJM JRP

Minute Time	Scale Weight	Burn Rate	Stack	Stove Top	Left Side	Back	Right Side	Bottom	Firebox	2nd Burn	Room Temp	Static	Comments
0	771.8	0	625	1052	630	511	621	416	979	1394	76	-077	RAIC FWD 0.30mm (45m)
5	771.0	18	471	965	629	504	620	415	956	1377	77	-067	Primary Air Set at 55.1 PA
10	770.3	17	425	940	625	486	617	415	977	1385	76	-063	Secondary Air Set at fixed
15	769.6	17	411	918	624	475	615	414	1002	1401	76	-062	Fan: OFF - ECT
20	768.9	17	402	912	629	464	615	412	1024	1426	76	-062	TUNNEL ON AT: 1105
25	768.3	16	389	906	633	456	614	409	1038	1401	77	-061	Buckets Iced
30	767.9	14	362	896	631	460	615	406	996	1368	77	-056	ANALYZERS SPANNED
35	767.7	12	331	890	623	478	614	403	994	1346	77	-051	Pumps turned on at: 1144
40	767.5	12	311	745	604	495	612	400	980	1321	77	-049	58516 AT 1147
45	767.3	12	295	699	604	500	606	396	960	1199	77	-046	57312 - 12.14
50	767.2	11	296	647	593	469	594	396	933	1162	76	-046	Check WAB: 5614 - 11.8
55	767.1	11	270	602	573	473	576	394	881	995	86	-042	543.8 - 17.6
60	767.0	11	263	587	556	434	561	394	850	964	76	-041	52516 - 19.2
65	766.9	11	255	563	539	440	573	392	826	949	76	-040	Probe IN TUNNEL
70	766.8	11	251	542	524	422	529	391	806	915	75	-039	TUNNEL APV 510.4 - 15
75	766.7	11	246	526	511	405	514	389	791	940	76	-038	49514 - 15
80													48116 - 13.1
85													469.0 - 12.6
90													
													455.5 - 46.5

Hot Box ON

\* Packed Rod. @ 410mm





Myren Consulting Inc Data Sheet P3 of 5 Unit Kelma Ashwood Date 2 / 18 / 09 Run FPA3  
 Test En 76617 AT 4694 Barometric Pressure 28.5 InHg Gas Flows @ 1.5" Technician(s) ATM GRF DDG

Time E/T min	Scale Wt.	Lbs. Left	Burn Rate	CO <sub>2</sub> v.	CO <sub>2</sub> %	O <sub>2</sub> v.	O <sub>2</sub> %	CO v.	CO %	Gas Bal	Opacity & Notes	Calc Wet B	Dry B		Stack	
													Wet B #1	Dry B #2	Temp #3	Static Press
120	768.8	2.1	.1	358	8.90	11.44	11.1	111	8.0		clear				242	7041
125	768.7	2.0	.1	363	9.02	11.36	10.4	104	8.7						253	7039
130	768.6	1.9	.1	354	8.90	11.49	12.1	121	7.3						247	7038
135	768.5	1.8	.1	337	8.38	11.85	13.4	134	6.3						241	7038
140	768.4	1.7	.1	330	8.21	11.99	14.0	140	5.9						238	7036
145	768.3	1.6	.1	321	7.99	12.15	15.2	152	5.3						233	7035
150	768.2	1.5	.1	311	7.74	12.35	16.3	163	4.7						229	7034
155	768.1	1.4	.1	305	7.59	12.45	17.1	171	4.4						226	7034
160	768.0	1.3	.1	297	7.39	12.65	17.6	176	4.3						224	7033
165	767.9	1.2	.1	284	7.07	12.89	18.7	187	3.8						221	7032
170	767.9	1.2	0	284	7.07	12.86	19.3	193	3.7						217	7031
175	767.8	1.1	.1	281	7.00	12.93	19.5	195	3.6						211	7030
Tot																

Time E/T	Top #4	Left #5	Back #6	Right #7	Bottom #8	Firebox #9	2 <sup>nd</sup> burn #10	Amb. #11	Tnl. #12	C Gas HBox #13	C Gas Impgr #14	Part. Filt. #15	Part. Cond. #16	Cent. 2nd #17	Tube 1 #18	Tube 2 #19	Tube 3 #20
125	577	535	440	519	315	889	1012	76	92	225	36	70	36	1036			
130	558	529	440	513	315	887	991	76	91	225	36	70	36	1013			
135	525	522	436	504	315	876	981	75	91	223	36	70	36	965			
140	523	517	433	500	316	850	965	75	91	223	36	70	36	972			
145	506	511	428	494	316	829	944	75	90	222	36	76	36	956			
150	495	505	424	480	316	821	931	76	90	222	36	76	36	941			
155	486	499	421	461	316	807	910	76	91	222	36	76	36	926		AT	4AT
160	475	493	416	474	317	794	896	76	91	221	36	79	36	907		440.6	-28.4
165	465	488	411	466	317	761	864	76	91	221	36	79	36	891		429.4	-39.6
170	455	482	405	463	317	760	851	77	92	222	36	80	36	876			
175	445	477	400	456	314	757	841	76	91	222	35	79	37	865		418.4	-50.6
Tot																	

11209





Myren Consulting Inc Data Sheet P5 of 5 Unit Kume A wood Date 2/1/09 Run PA  
 Test Enc. Wt 766.7 AT 469.0 Barometric Pressure 28.52 "hg Gas Flows @ 1.5" Technician(s) ATM GAK PDB

Time -ET- min	Scale Wt.	Lbs. -Left-	Burn Rate	CO <sub>2</sub> v. %	CO <sub>2</sub> -%	O <sub>2</sub> v. %	O <sub>2</sub> -%	CO v. %	CO -%	Gas Bal	Opacity & Notes	Calc Wet B	Wet B #1	Dry B #2	Stack	
															Temp #3	Static Press
240	246.9	11	0	124	6.01	13.88	2.02	2.02	3.0						196	-826
245	246.7	0	1	24	6.01	13.94	1.85	1.85	3.2						195	2025
250															<del>391</del>	<del>6051</del>
255															<del>1350</del>	<del>81041</del>
260															<del>271</del>	<del>6041</del>
265																
270																
275																
280																
285																
290																
295																
Tot																

Total  
AVG ÷ 50

Time -ET- min	Top #4	Left #5	Back #6	Right #7	Bottom #8	Firebox #9	2 <sup>nd</sup> burn #10	Amb. #11	Tal. #12	C Gas H Box #13	C Gas Impgr #14	Part. Filt. #15	Part. Cond. #16	Tube 1 #17	Tube 2 #18	Tube 3 #19	H <sub>2</sub> O H box #20	
																		240
245	389	426	387	403	304	649	747	79	93	223	36	83	38	786		802.2	-6618	
250																		
255																		
260																		
265																		
270																		
275																		
280																		
285																		
290																		
295																		
Tot																		

Total  
AVG ÷ 50

Delta  
Stack  
SI-OP  
ΔAT

53093  
11062

469.0  
882.2  
-86.0

PRE AND POST TEST ZERO/SPAN CHECK  
WOODSTOVE DATA SHEET #15-1

Colville

Site: Myren Consulting, , WA Date: 2/18/09 Analyte: CO<sub>2</sub>

Source: Kuma Ashwood Run #: EPA 3

Zero Cyl #: TC 3AAM154 Conc. 00.0 % CO<sub>2</sub> Cyl Press: 1510 psi

Certified by: Oxarc Date: 11/12/07

Span Cyl #: AS 90457 Conc. 12.5 % CO<sub>2</sub> Cyl Press: 1490 psi

Certified by: Matheson Tri Gas Date: 2/2/09

Analyzer: Make: Horiba Model: PIR-2000 SN: 607024

Range: 0 - 25.0% CO<sub>2</sub> Analyzer Output: 0 - 1.0 v.

Flow: 1.5 SCFH Measured by: Rotameter: X Flowmeter:           

EPA Span Value = 25.0% CO<sub>2</sub>  
EPA Control Limits = + 2.5% of 25.0% CO<sub>2</sub> = + 0.625% CO<sub>2</sub>

Pre Run Audit: By: A.T. Myren Time: 1105 Temp: 75 °F

Audit Results

Point #	Expected Response			Actual Response			+ Conc. Difference	Δ %
	Meter	DVM	%	Meter	DVM	%		
Zero	00.0	.000	00.0	00.0	.000	.05453	+0.05453	+0.22
Span	50.0	.500	12.5	49.75	.499	12.3858	-0.1142	-0.91

Comments:

Post Run Audit: By: A.T. Myren Time: 1656 Temp: 77 °F

Audit Results

Point #	Expected Response			Actual Response			+ Conc. Difference	Δ %
	Meter	DVM	%	Meter	DVM	%		
Zero	00.0	.000	00.0	00.0	.000	.05453	+0.05453	+0.22
Span	50.0	.500	12.5	50.5	.506	12.5587	+0.0587	+0.46

Comments:

+ Conc. Difference = Act % - Exp (Std) %  
 Zero % Difference =  $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Full Scale Value}} \times 100$   
 Span % Difference =  $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Exp \% (ppm)}} \times 100$

PRE AND POST TEST ZERO/SPAN CHECK  
WOODSTOVE DATA SHEET #15-3

colville

Site: Myren Consulting, Woodinville, WA Date: 2/18/09 Analyte: CO

Source: Kuma Ashwood Run #: EPA 3

Zero Cyl #: TC3AAM 154 Conc. 00.0 % CO Cyl Press: 1510 psi

Certified by: Oxarc Date: 11/12/07

Span Cyl #: AS 904 57 Conc. 2.00 % CO Cyl Press: 1490 psi

Certified by: Matheson Tri Gas Date: 2/2/09

Analyzer: Make: HORIBA Model: 311GE SN: GE-30025

Range: 0 - 10.0% CO Analyzer Output: 0 - 1.0 V

Flow: 1.5 SCFH Measured by: Rotameter: X Flowmeter:     

EPA Span Value = 5.0% CO  
EPA Control Limits = +2.5% of 5.0% CO = + 0.125% CO

Pre Run Audit: By: A.T. Myren Time: 1105 Temp: 75 °F

Audit Results

Point #	Expected Response			Actual Response			+ Conc. Difference	Δ %
	Meter	DVM	%	Meter	DVM	%		
Zero	00.0	00.0	00.0	0.00	.000	-0.00443	-0.00443	-0.04
Span	2.00	.200	2.00	2.00	.200	2.00595	+0.00595	+0.30

Comments:

Post Run Audit: By: A.T. Myren Time: 1656 Temp.: 77 °F

Audit Results

Point #	Expected Response			Actual Response			+ Conc. Difference	Δ %
	Meter	DVM	%	Meter	DVM	%		
Zero	00.0	00.0	00.0	0.00	.000	-0.00443	-0.00443	-0.04
Span	2.00	.200	2.00	1.99	.199	1.9959	-0.0041	-0.21

Comments:

Conc. Difference = Act % - Exp (Std) %  
 Zero % Difference =  $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Full Scale Value}} \times 100$   
 Span % Difference =  $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Exp \% (ppm)}} \times 100$

Unit: Kuma Ashwood  
 Run: EPA 3  
 Date: 2/18/89  
 Technicians: ATM JRP PDG  
 WS Form 3-Rev 11/89

QUALITY CHECKS  
 WOODSTOVE DATA SHEET #16

Ambient = Tr: \_\_\_\_\_ °F T/C#30: \_\_\_\_\_ °F  
 Thermocouple Check (at ambient): T/C#1: \_\_\_\_\_ °F; T/C#2: 66.2 °F;  
 T/C #3: 63.7 °F; T/C #4: 63.3 °F; T/C #5: 62.4 °F;  
 T/C #6: 63.0 °F; T/C #7: 62.8 °F; T/C #8: 68.7 °F;  
 T/C #9: 74.8 °F; T/C #10: 60.7 °F; T/C #11: 61.5 °F;  
 T/C #12: 63.2 °F; T/C #13: 63.4 °F; T/C #14: 59.2 °F;  
 T/C #15: 62.9 °F; T/C #16: 53.5 °F; T/C #17: 74.2 °F;  
 T/C #18: \_\_\_\_\_ °F; T/C #19: \_\_\_\_\_ °F; T/C #20: \_\_\_\_\_ °F;  
 T/C #21: \_\_\_\_\_ °F; T/C #22: \_\_\_\_\_ °F; T/C #23: \_\_\_\_\_ °F;  
 T/C #24: \_\_\_\_\_ °F; T/C #25: \_\_\_\_\_ °F; T/C #26: \_\_\_\_\_ °F;

Comments: \_\_\_\_\_

Thermocouple Readout: Pretest Zero/Span Check and Calibration:  
 Zero (0°F) : 0.2 °F Adj to: \_\_\_\_\_ °F Post Test Check Zero (0°F): 0.6 °F % Difference +0.13  
 Span (2000°F): 2000.3 °F Adj to: \_\_\_\_\_ °F Span (2000°F): 2001.6 °F % Difference +0.07

(Allowable % Difference = 1.5%. Use formulas on Woodstove Data Sheet #15 to calculate % Difference) **In Degrees Absolute.**

Thermocouple Readout Pretest Linearity Check  
 0°F = 0.2 °F; 200°F = 202.1 °F; 400°F = 399.4 °F;  
 600°F = 601.6 °F; 800°F = 801.8 °F; 1000°F = 1001.0 °F;  
 1200°F = 1198.8 °F; 1400°F = 1399.6 °F; 1600°F = 1600.2 °F;  
 1800°F = 1800.3 °F; 2000°F = 2000.3 °F

Combustion Gas (CO<sub>2</sub>, O<sub>2</sub>, CO) Train Leak Check: Pre PDG Post PDG  
 Draft (Static) Gauge Zero Check: Pre ATM Post PDG

Scale Check Pre (Wt, #'s): 770.4 - 765.4 = 5.0 lbs / 50 lbs = 0% ATM  
 Post (Wt, #'s): 770.7 - 765.7 = 5.0 lbs / 50 lbs = 0% PDG

stack cleaned prior to the run: Yes \_\_\_\_\_ No ✓  
 Tunnel cleaned prior to the run: Yes \_\_\_\_\_ No ✓

MYREN CONSULTING CERTIFICATION TEST DATA

DILUTION TUNNEL CALCULATIONS

1/25/09, Md=28.56, Bws=4% 6" Tunnel

File Name:	EPA 5	Run Time (min)	PITOT DELTAP (- INCH H2O)	TNL TEMP (°F)	GAS METER RDG (ft3)	GAS METER TEMP (°F)	GAS DELTA H (in.H2O)	TUNNEL VELOCITY (ft/min)	PROP RATE (%)	dGDM vol std (ft3)	Tunnel Static (- Inch H2O)	SQUARE ROOT DELTA P	DRY GAS METER RDG (m3)
Manufacturer:	KUMA	0	0.041	96	457.4020	70	0.900	849.23			0.154	0.2025	
Model Number:	ASHWOOD	10	0.040	103	462.6680	73	0.900	844.07	104.1	5.076	0.151	0.2000	
Lab Name:	MYREN	20	0.040	97	467.9480	76	0.900	839.57	102.7	5.061	0.152	0.2000	
Test Date:	2/20/09	30	0.039	98	473.1950	79	0.900	829.75	102.3	5.001	0.152	0.1975	
Run Number:	EPA 5	40	0.040	102	478.4560	82	0.900	843.32	100.5	4.987	0.151	0.2000	
Meter Box Y Factor:	1.0177	50	0.040	101	483.7080	85	0.900	842.57	99.1	4.951	0.150	0.2000	
Barometric pressure (in):	28.551	60	0.040	101	488.9600	87	0.900	842.57	98.4	4.933	0.150	0.2000	
Gas meter temp (ave):	89	70	0.040	102	494.2340	88	0.900	843.32	98.5	4.944	0.150	0.2000	
delta H(avg):	0.900	80	0.040	101	499.5030	89	0.900	842.57	98.0	4.931	0.150	0.2000	
Gas meter initial reading:	457.4020	90	0.040	100	504.7830	90	0.900	841.82	97.8	4.932	0.150	0.2000	
Gas meter final reading:	602.7820	100	0.040	98	510.0520	90	0.900	840.32	97.4	4.922	0.151	0.2000	
Front catch (acetone) mg:	5.8	110	0.040	96	515.3330	91	0.900	838.81	97.1	4.924	0.151	0.2000	
first filter catch (mg):	66.7	120	0.040	95	520.6160	91	0.900	838.06	97.0	4.926	0.151	0.2000	
second filter catch (mg):	0.6	130	0.039	95	525.9140	91	0.900	827.51	96.8	4.940	0.151	0.1975	
Tunnel Flow (Qsd) (dscfm)	140.186	140	0.040	94	531.2110	92	0.900	837.30	96.8	4.930	0.150	0.2000	
Emission Rate(g/hr):	4.519	150	0.040	93	536.5000	92	0.900	836.54	96.6	4.922	0.150	0.2000	
Emission Rate(M5H) :	6.365	160	0.040	93	541.8020	92	0.900	836.54	96.9	4.935	0.151	0.2000	
Avg. of Delta P Sq. Roots:	0.2000	170	0.040	92	547.1140	92	0.900	835.79	96.9	4.944	0.152	0.2000	
Vs (Avg.)(ft/min):	822.400	180	0.040	94	552.4120	92	0.900	837.30	96.9	4.931	0.151	0.2000	
Tunnel Avg. Temperature (F):	96.793	190	0.039	95	557.7130	93	0.900	827.51	97.9	4.925	0.151	0.1975	
Test time(min):	275	200	0.040	95	563.0180	93	0.900	838.06	96.7	4.928	0.151	0.2000	
Fuel Load(lb. wet):	13.332	210	0.040	95	568.3250	93	0.900	838.06	96.8	4.930	0.152	0.2000	
Wood moisture(%wet):	16.449	220	0.040	96	573.6280	94	0.900	838.81	96.4	4.918	0.152	0.2000	
Burn rate(dry kg/hr):	1.102	230	0.039	98	578.9160	94	0.900	829.75	97.6	4.904	0.151	0.1975	
Sample Volume (discf)	136.052	240	0.040	97	584.2140	94	0.900	839.56	96.4	4.913	0.151	0.2000	
Avg. Tunnel Static (-inch H2O):	0.1510	250	0.040	97	589.5280	95	0.900	839.56	96.4	4.919	0.151	0.2000	
Room Blank Catch (mg/dscf):	0	260	0.039	95	594.8420	94	0.900	827.51	97.8	4.928	0.151	0.1975	
Emission Factor (g/kg):	4.0995	270	0.039	94	600.1330	94	0.900	826.77	97.3	4.907	0.150	0.1975	
Pitot Correction Factor:	0.97975	275	0.040	94	602.7820	94	0.900	837.30	96.2	2.457	0.151	0.2000	
front filter number	714				0.0000			0.00	0.0	0.000		0.0000	
back filter number	713				0.0000			0.00	0.0	0.000		0.0000	
Beaker Number:	25				0.0000			0.00	0.0	0.000		0.0000	
PRELIMINARY RESULTS					0.0000			0.00	0.0	0.000		0.0000	
FINAL RESULTS:	AUDITED	300			0.0000			0.00	0.0	0.000		0.0000	
DATA SUMMARY		310			0.0000			0.00	0.0	0.000		0.0000	
MODEL:	ASHWOOD	320			0.0000			0.00	0.0	0.000		0.0000	
RUN:	EPA 5	330			0.0000			0.00	0.0	0.000		0.0000	
DATE:	2/20/09	340			0.0000			0.00	0.0	0.000		0.0000	
DBR:	1.102	350			0.0000			0.00	0.0	0.000		0.0000	
EMISSION RATE (g/hr)(M5H)	6.3647	360			0.0000			0.00	0.0	0.000		0.0000	
EMISSION FACTOR (g/kg):	4.0995	370			0.0000			0.00	0.0	0.000		0.0000	
AVG. % PROPORTIONALITY:	98.033	380			0.0000			0.00	0.0	0.000		0.0000	

METHOD 5G

PARTICULATE SAMPLING DATA

Rev. 2/09

DATE: 2/20/09 PAGE 1 OF 2 UNIT: Kumar Ashwood RUN: EPA 5

METER BOX: 45G-P METER Y: 1.0177 FILTER #'S: (F) 714 (R) 713

.208/.208  
PRE TEST LEAK CHECK: .000 CFM @ -15.5 IN HG FILTER SIZE: 110 mm

.846/.846  
POST TEST LEAK CHECK: .000 CFM @ -15.2 IN HG PROBE LENGTH 21.0 IN

TIME		METER READING (FT <sup>3</sup> )	PITOT		TUNNEL TEMP (°F)	METER TEMP (°F)	GAS METER Δh	VAC (in Hg)
CLOCK	ELAPSED		ΔP	Pg				
1030	00	457.402	.041	-154	96	70	0.90	0.0
	40	462.668	.040	-151	103	73	.90	0
	50	467.948	.040	-152	97	76	.90	0
1100	30	473.195	.039	-152	98	79	.90	0
	40	478.456	.040	-151	102	82	.90	0
	50	483.708	.040	-150	101	85	.90	0
	60	488.960	.040	-150	101	87	.90	0
	70	494.234	.040	-150	102	88	.90	0
	80	499.503	.040	-150	101	89	.90	0
1200	90	504.783	.040	-150	100	90	.90	0
	100	510.052	.040	-151	98	90	.90	0
	110	515.333	.040	-151	96	91	.90	0
	120	520.616	.040	-151	95	91	.90	0
	130	525.914	.039	-151	95	91	.90	0
	140	531.211	.040	-151	94	92	.90	0
1300	150	536.500	.040	-150	93	92	.90	0
	160	541.802	.040	-151	93	92	.90	0
	170	547.114	.040	-152	92	92	.90	0
	180	552.412	.040	-151	94	92	.90	0
	190	557.713	.039	-151	95	93	.90	0

BP

00 28.57  
 60 28.57  
 120 28.55  
 180 28.55  
 240 28.54 AVG. = 28.55  
 275 28.52

Pre Test Filter  
 Check Weighing  
 F .6660  
 R .6870

End of Test Weight  
 F .7330 R .6874  
.6655 .6866  
.0675

METHOD 5G

PARTICULATE SAMPLING DATA

Rev. 2/09

DATE: 2/20/09 PAGE 2 OF 2 UNIT: Kuma Ashwood RUN: EPA 5

METER BOX: 456-P METER Y: 1.0177 FILTER #'S: (F) 714 (R) 713

PRE TEST LEAK CHECK: .000 CFM @ -15.5 IN HG FILTER SIZE: 110 mm

POST TEST LEAK CHECK: .000 CFM @ -15.2 IN HG PROBE LENGTH 21.0 IN

TIME		METER READING (FT <sup>3</sup> )	PITOT		TUNNEL TEMP (°F)	METER TEMP (°F)	GAS METER Δh	VAC (in Hg)
CLOCK	ELAPSED		ΔP	Pg				
1350	200	563.018	.040	-151	95	93	.90	0
1400	210	568.325	.040	-152	95	93	.90	0
10	220	573.628	.040	-152	96	94	.90	0
20	230	578.916	.039	-151	98	94	.90	0
30	240	584.214	.040	-151	97	94	.90	0
40	250	589.528	.040	-151	97	95	.90	0
50	260	594.842	.039	-151	95	94	.90	0
1500	270	600.133	.039	-150	94	94	.90	0
1505	<del>270</del> 275	602.782	.040	-151	94	94	.90	0
	90							
	00							
	10							
	20							
	30							
	40							
	50							
	60							
	70							
	80							
	90							

75 min

BP  
00 28.57  
60 28.57  
120 28.555  
180 28.55  
240 28.54    AVG. = 28.551  
275 28.52

Pre Test Filter  
 Check Weighing  
 F = .6660  
 R = .6870

End of Test Weight  
 F .6655    R .6866

MYREN CONSULTING, INC.

Dilution Tunnel Traverse Data with 8 Traverse Points

Unit: KUMMA Ashwood  
 Run #: EPA 5  
 Date: 2/20/09  
 Technicians: ATM PDG JRP  
 12 Rev 4/2/08

12 Pg

Point	Location	$\Delta p$	$\sqrt{\Delta p_{trav}}$	$\Delta p$	$\sqrt{\Delta p_{cent}}$	$T_{trav}$	$T_{cent}$	Pg
W-1	0.5"	<u>.038</u>	<u>.1949</u>			<u>101</u>		
2	1.5"	<u>.041</u>	<u>.2025</u>	<u>.041</u>	<u>.2025</u>	<u>101</u>		<u>160</u>
Center	Center							
3	4.5	<u>.040</u>	<u>.2000</u>			<u>101</u>		
4	5.5	<u>.039</u>	<u>.1975</u>			<u>101</u>		
S-1	0.5	<u>.036</u>	<u>.1897</u>			<u>99</u>		
2	1.5	<u>.041</u>	<u>.2025</u>			<u>99</u>		<u>158</u>
Center	Center							
3	4.5	<u>.041</u>	<u>.2025</u>			<u>99</u>		
4	5.5	<u>.039</u>	<u>.1975</u>			<u>99</u>		
Totals			<u>1.5071</u>		<u>.4050</u>	<u>800</u>	<u>200</u>	<u>1219</u>
Average			<u>.1984</u>		<u>.2025</u>	<u>100</u>	<u>100</u>	<u>1595</u>
		$^{\circ}R = (^{\circ}F + 460)$				<u>560</u>	<u>560</u>	

Ps = BP + (-Pg/13.6) = 28.57 + (-1595/13.6) = 20.558

LEAK CHECKS:  
 Pre Test: Pg Leg: OK Velocity Head Leg: OK  
 Post Test: Pg Leg: OK Velocity Head Leg: OK



DILUTION TUNNEL GAS VELOCITY & VOLUMETRIC FLOW RATE CALCULATIONS

Rev 4/19/08

UNIT: Kumar Ashwood DATE: 2/20/09 RUN #: EPA 5 TECHNICIAN(S): AM JRP  
PAG

Average Gas Velocity in the Dilution Tunnel  $V_{strav}$  (EPA M2 EQN 2-9, ASTM E 2515-07 EQN 7)

$$(9) V_{strav} = (85.49) (0.99 \text{ cp}) (\frac{1904}{\sqrt{\Delta P}} \sqrt{\Delta P}) \sqrt{\Delta P} \frac{Ts}{Ps} = 13,913.72 \text{ fps}$$

$$(9A) V_s = (\frac{13,913.72}{60}) \text{ fpm} = 231.823 \text{ fpm}$$

Gas Velocity in the Center of the Dilution Tunnel -  $V_{scent}$  (EPA M2 EQN 2-9, ASTM E 2515-07 EQN 7)

$$(9) V_{scent} = (85.49) (0.99 \text{ cp}) (\frac{2025}{\sqrt{\Delta P}} \sqrt{\Delta P}) \sqrt{\Delta P} \frac{Ts}{Ps} = 14,201.25 \text{ fps}$$

$$(9A) V_s = (\frac{14,201.25}{60}) \text{ fpm} = 236.675 \text{ fpm}$$

EPA M5G1 Section 4.2.2, ASTM E 2515-07 EQN 1 Adjustment Factor for Center of Tunnel Pitot Tube Location

$$F_p = V_{strav} / V_{scent} = 13,913.72 \div 14,201.25 = 0.97975$$

Average Stack Gas Dry Volumetric Flow Rate -  $Q_{sd}$  (EPA M2 EQN 2-10, ASTM E 2515-07 EQN 3)

$$(10) Q_{sd} = 3600 (1 - 0.04 Bws) (\frac{13,913.72}{3600}) (1.963 \text{ ft}^2) [(528 \text{ } ^\circ\text{A}) (\frac{28.558 \text{ Ps } ^\circ\text{Hg}}{560 \text{ Ts } ^\circ\text{A}}) (29.92 \text{ } ^\circ\text{Hg})] = 9494.726 \text{ dscfh}$$

$$(10A) \frac{9494.726}{60} \text{ dscfm} = 158.244 \text{ dscfm}$$

Note: Number in { } under blank lines denotes number of decimals to be used. If a blank calls for an answer already calculated, use the number of decimals previously specified for that answer.

WOODSTOVE DATA SHEET #4-1: INITIAL FILTER WEIGHTS (TARE WEIGHTS)

Into Dessicator: Date 1-20-09 Time 1149 By PDG Front Half X Back Half X

Manufacturer: Pall P/N. 60115 Size: 110 Lot.No.: 70726 Grade: A/E Glass

Filter #	First Wt	2009 Date	Time	By	Second Wt	Date	Time	By	Third Wt	2009 Date	Time	By
700	.6873	1-22	1331	GRP	.6877	1-23	1417	PDG				
701	.6871		1330	GRP	.6878		1419	PDG	.6877	1-26	1421	GRP
702	.6876		1329	GRP	.6825		1420	PDG	.6824	1-26	1420	GRP
703	.6761		1328	GRP	.6762		1421	PDG				
704	.6727		1327	GRP	.6732		1422	PDG				
705	.6833		1326	GRP	.6837		1423	PDG				
706	.6946		1325	GRP	.6948		1424	PDG				
707	.6773		1324	GRP	.6777		1425	PDG				
708	.6701		1323	GRP	.6702		1426	PDG				
709	.6799		1322	GRP	.6809		1427	PDG	.6806	1-26	1419	GRP
710	.6587		1321	GRP	.6590		1428	PDG				
711	.6654		1320	GRP	.6656		1429	PDG				
712	.6688		1319	GRP	.6692		1430	PDG				
713	.6864		1318	GRP	.6866		1431	PDG				
714	.6651		1318	GRP	.6655		1432	PDG				
715	.6741		1317	GRP	.6744		1433	PDG				
716	.6592		1316	GRP	.6590		1434	PDG				
717	.6531		1315	GRP	.6536		1435	PDG				
718	.6621		1314	GRP	.6623		1436	PDG				
719	.6769		1313	GRP	.6769		1437	PDG				
720	.6627		1312	GRP	.6628		1438	PDG				
721	.6567		1311	GRP	.6569		1439	PDG				
722	.6539		1310	GRP	.65340		1440	PDG				
723	.6552		1309	GRP	.6552		1441	PDG				
724	.6655		1308	GRP	.6656		1442	PDG				

Checked by A.T. Myer Date: 1/27/09 Time 1632

QA REWEIGH

BALANCE ROOM ENVIRONMENTAL CONDITIONS

Filter #	WT	Date	Time	By
703	.6761	1/27/09	1639	AMM
708	.6705		1640	AMM
715	.6799		1642	AMM

WB	DB	%RH	Date	Time	By
57	72	38	1-22-09	1138	ATM
58	25	33	1-23-09	1150	PDG
56	76	25	1-26-09	1359	GRP
58	72	31	1/27/09	1530	PDG

Post 1-22 1-23 1-26  
 0.0000 0.0000 0.0000  
 100.0000 99.9994 99.9993

WOODSTOVE DATA SHEET #4-2:  
INITIAL BEAKER WEIGHTS (TARE WEIGHTS)

Into Dessicator: Date: 9.04.08 Time: 13:33 By: JRP

Beaker #	First Wt	2008 Date	Time	By	Second Wt	2009 Date	Time	By	Third Wt	2009 Date	Time	By
24	73.2197	12/17	1628	JRP	73.2186	1/20	1000	PDG	73.2188	1/20	1635	JRP
25	72.6520		1625	JRP	72.6512		1002	PDG	72.6514		1635	JRP
26	71.7887		1631	JRP	71.7881		1007	PDG	71.7877		1626	JRP
28	70.5985		1627	JRP	70.5976		1003	PDG	70.5977		1632	JRP
29	71.5207		1635	JRP	71.5191		1008	PDG	71.5193		1637	JRP
30	70.7867		1629	JRP	70.7855		1005	PDG	70.7856		1627	JRP
33	53.1490		1632	JRP	53.1483		1012	PDG	53.1486		1633	JRP
34	53.2618		1636	JRP	53.2609		1014	PDG	53.2609		1628	JRP
35	53.2826		1637	JRP	53.2817		1016	PDG	53.2815		1629	JRP
36	53.5752		1638	JRP	53.5742		1010	PDG	53.5744		1634	JRP
42												
43	53.2325		1633	JRP	53.2315		1011	PDG	53.2319		1631	JRP

Checked By: A.P. Myam Date: 1/23/09 Time: 1145

QA REWEIGH

Beaker #	WT	Date	Time	By
35	53.2820	1/23/09	1146	APM
26	71.7882	1/23/09	1147	APM
43	53.2323	1/23/09	1149	APM

BALANCE ROOM ENVIRONMENTAL CONDITIONS

WB	DB	%RH	Date	Time	By
52	70	25	12/17/08	1619	JRP
58	74	37	1/20/09	0950	PDG
57	73	33	1/20/09	1613	JRP
57	72	38	1/23/09	1138	APM

WOODSTOVE DATA SHEET #4-2:  
INITIAL BEAKER WEIGHTS (TARE WEIGHTS)

Blanks done 12/9/07

Into Dessicator: Date: 10/12/07 Time: 0801 By: GRP

Beaker #	First Wt	Date	Time	By	Second Wt	Date	Time	By	Third Wt	Date	Time	By
22	71.8343	10/22/07	1358	GRP	71.8332	11/10/07	1938		71.8330	11-11-07	1748	Jm
24	73.2192		1400	GRP	73.2190	11/10/07	1940		73.2193	11-11-07	1746	Jm
25	72.6516		1401	GRP	72.6512	11/10/07	1944		Blank			
26	71.7895		1403	GRP	71.7888	11/10/07	1939		71.7886	11-11-07	1747	Jm
27	72.3316		1402	GRP	72.3314	11/10/07	1945					
28	70.5979		1404	GRP	70.5975	11/10/07	1941		70.5977	11-11-07	1745	Jm
39	53.1508		1405	GRP	53.1500	11/10/07	1942					
37	53.7237	11/10/07	1945	Jm	53.7238	11/11/07	1743	Jm				

Checked By: \_\_\_\_\_ Date: \_\_\_\_\_ Time: \_\_\_\_\_

QA REWEIGH

Beaker #	WT	Date	Time	By
27	72.3315	11-11	1740	Jm
25	72.6515	11-11	1741	Jm
39	53.1509	11-11	1744	Jm

BALANCE ROOM ENVIRONMENTAL CONDITIONS

WB	DB	%RH	Date	Time	By
57	68	50	10/22/07	1344	GRP
			11/10		

Post weighing  
0.0000g  
in room for  
LSD  
0.0000  
00000h  
2nd

WOODSTOVE DATA SHEET #4-3: COULANT FINAL WEIGHTS

FINAL BEAKER WEIGHTS

Beaker #	Into Dessic Date	Time	By	First	Date	Time	By	Second	Date	Time	By	Third	Date	Time	By
25	2/23/2009	0925	PM	72.6562	7/24	1007	AM	72.6570	2/28	1029	PM	72.6572	2/26	1331	JRP

FINAL FILTER WEIGHTS

Filter #	Into Dessic Date	Time	By	First	Date	Time	By	Second	Date	Time	By	Third	Date	Time	By
F 714	2/20/2009	1945	AM	7322	2/21	1546	AM	7325	2/22	1240	JRP	7331	2/23	1424	PM
				7324	2/24	1012	AM	7322	2/25	1134	PM				
R 713	2/20/2009	1945	AM	6870	2/21	1535	AM	6874	2/22	1238	JRP	6873	2/23	1420	PM
				6872	2/24	1012	AM								

SCALE ROOM ENVIRONMENTAL CONDITIONS

Session	Date	Time	By	WB	DB	%RH
6	2/26/2009	JRP	55	70	36	
7						
8						
9						
Comments						

SCALE ROOM ENVIRONMENTAL CONDITIONS

Session	Date	Time	By	WB	DB	%RH
1	2/21/2009	1519	AM	60	77	35
2	2/22/2009	1322	AM	47	59	37
3	2/23/2009	1406	PM	58	20	46
4	2/24/2009	0953	AM	59	46	35
5	2/25/2009	1123	PM	60	20	38

QA REWEIGH: FINAL WEIGHTS

Date	Beaker #	Final Wt	By
Date	Filter #	Final WT	By

Acuone  
best #  
041648

WOODSTOVE DATA SHEET #4-3: CONSTANT FINAL WEIGHTS  
TALS 776812

Blank  
done  
12-19-07

HST5-Form 9, Pg. 1, Rev. 4/90  
Unit: KUMR  
Run # 5  
Date: 2-19-09

FINAL BEAKER WEIGHTS

Beaker #	Into Dessic	2007 Date	Time	By	First	Date	Time	By	Second	Date	Time	By	Third	Date	Time	By
35	✓	12/12	1546	JRP	72.6508	12/13	1342	JRP	72.6511	12/14	1347	JRP				

FINAL FILTER WEIGHTS

Filter #	Into Dessic	Date	Time	By	First	Date	Time	By	Second	Date	Time	By	Third	Date	Time	By

QA BENVLICH: FINAL WEIGHTS

Date	Beaker #	Final Wt	By
Date	Filter #	Final Wt	By

SCALE ROOM ENVIRONMENTAL CONDITIONS

Weighing Session	Date	Time	By	WB	DB	ZRH
1	12/13	1307	JRP	55	73	29
2	12/14	1331	JRP	57	75	31

SCALE ROOM ENVIRONMENTAL CONDITIONS

	6	7	8	9	Comments

WOODSTOVE DATA SHEET 4-4 SCALE QC RECORD SHEET

SCALE: SARTORIUS  
 MODEL: CP224S  
 SN: 17050374

FROM: 9/27/2007  
 THROUGH: 12/7/2007

Level	Recali	130 g	100 g	10 g	1.0 g	100 mg	20 mg	Date	Time	Tech	Wet Bulb	Dry Bulb	% RH
✓	N	129.9998	99.9998	10.0000	1.0000	0.1000	0.0199	9/27/07	1402	GRP	55	67	45
✓	Y	129.9995	99.9996	10.0001	1.0000	0.1000	0.0200	9/28/07	1335	GRP	57	69	46
✓	Y	129.9996	99.9996	9.9999	1.0000	0.1000	0.0200	10/1/07	1505	ATM	58	70	48
✓	N	129.9995	99.9996	10.0000	1.0000	0.1000	0.0199	10/2/07	1611	GRP	56	68	46
✓	N	129.9997	99.9997	9.9999	1.0001	0.1000	0.0199	10/3/07	1122	GRP	56	68	46
✓	N	129.9996	99.9996	10.0000	1.0000	0.1000	0.0199	10/4/07	1235	GRP	55	67	45
✓	Y	129.9996	99.9996	10.0000	1.0000	0.1000	0.0199	10/5/07	0750	GRP	51	62	45
✓	N	129.9997	99.9997	9.9999	1.0000	0.1000	0.0199	10/5/07	1513	GRP	56	69	43
✓	Y	129.9996	99.9996	10.0000	1.0001	0.1001	0.0200	10/9/07	1505	ATM	58	71	44
✓	N	129.9996	99.9997	10.0000	1.0001	0.1001	0.0200	10/12/07	1259	ATM	58	70	48
✓	Y	129.9995	99.9996	9.9999	1.0000	0.1000	0.0199	10/22/07	1344	GRP	57	68	50
✓	Y	129.9996	99.9997	9.9999	1.0000	0.1000	0.0199	10/29/07	1338	GRP	53	63	50
✓	N	129.9995	99.9995	10.0000	1.0000	0.1000	0.0200	10/31/07	0933	ATM	56	70	40
✓	Y	129.9996	99.9997	10.0000	1.0000	0.1000	0.0199	10/31/07	1457	GRP	55	70	36
✓	Y	129.9996	99.9996	9.9999	1.0000	0.1000	0.0199	10/31/07	1528	GRP	57	75	30
✓	Y	129.9996	99.9996	9.9999	1.0000	0.0999	0.0199	11/2/07	1238	GRP	58	67	33
✓	Y	129.9996	99.9996	10.0000	1.0001	0.1000	0.0199	11/5/07	0730	GRP	57	73	35
✓	Y	129.9996	99.9997	10.0000	1.0000	0.1001	0.0201	11/9/07	1550	ATM	58	70	48
✓	N	129.9996	99.9997	10.0000	1.0000	0.1000	0.0200	11/10/07	1885	ATM	58	71	44
✓	Y	129.9997	99.9997	9.9999	1.0000	0.1000	0.0199	11/11/07	1810	ATM	55	69	39
✓	N	129.9997	99.9996	9.9999	1.0000	0.1000	0.0199	11/12/07	0822	GRP	54	67	41
✓	N	129.9996	99.9996	10.0000	1.0000	0.1000	0.0199	11/26/07	1226	ATM	58	72	41
✓	N	129.9998	99.9997	9.9999	0.9999	0.1000	0.0200	11/14/07	1710	GRP	58	73	39
✓	QC	Services Audit 11/11/07											
✓	Y	129.9997	99.9997	10.0000	1.0000	0.1000	0.0200	11/15/04	1350	ATM	59	72	45
✓	N	129.9996	99.9996	9.9999	0.9999	0.1000	0.0200	11/16/07	1600	GRP	58	71	41
✓	N	129.9996	99.9996	10.0000	1.0000	0.1000	0.0199	11/19/07	1758	ATM	740	74	43
✓	Y	129.9995	99.9996	10.0000	1.0000	0.1001	0.0200	11/20/07	1416	GRP	56	70	40
✓	Y	129.9996	99.9996	10.0000	1.0000	0.1000	0.0199	11/21/07	1110	ATM	54	69	35
✓	N	129.9995	99.9996	10.0000	1.0000	0.1000	0.0200	12/3/07	0730	GRP	57	70	40
✓	Y	129.9996	99.9996	10.0000	1.0000	0.0999	0.0200	12/16/07	1125	ATM	54	67	44
✓	Y	129.9996	99.9996	10.0000	1.0000	0.1000	0.0200	12/17/07	1348	GRP	55	69	40

SCALE: SARTORIUS  
 MODEL: CP224S  
 SN: 17050374

WOODSTOVE DATA SHEET 4-4 SCALE QC RECORD SHEET

FROM: 12/8/07  
 THROUGH: 2/3/08

Level	Recali	130 g	100 g	10 g	1.0 g	100 mg	20 mg	Date	Time	Tech	Wet Bulb	Dry Bulb	% RH
brated,	Weights	Weight	Weight	Weight	Weight	Weight	Weight				Bulb	Bulb	
✓	N	129.9996	99.9996	10.0000	1.0000	0.1000	0.0200	12/8	12:15	ATM	57	73	35
✓	N	129.9996	99.9996	10.0000	1.0000	0.1000	0.0200	12/8	19:10	ATM	57	72	38
✓	N	129.9997	99.9996	10.0000	1.0000	0.1000	0.0199	12/9	19:35	ATM	55	72	31
✓	Y	129.9996	99.9996	10.0000	1.0000	0.1000	0.0200	12/10	19:53	ATM	56	72	34
✓	N	129.9997	99.9997	10.0000	1.0000	0.1000	0.0199	12/11	16:18	GRP	57	76	28
✓	N	129.9997	99.9996	10.0000	1.0000	0.0999	0.0199	12/12	5:05	GRP	56	74	30
✓	N	129.9997	99.9996	9.9999	0.9999	0.1000	0.0199	12/13	3:07	GRP	55	73	29
✓	N	129.9996	99.9996	9.9999	0.9999	0.1000	0.0199	12/14	13:21	GRP	57	75	31
✓	N	129.9996	99.9996	9.9999	1.0000	0.1000	0.0199	12/15	16:02	GRP	57	75	31
✓	N	129.9998	99.9998	9.9999	1.0001	0.1000	0.0199	12/17	08:17	GRP	55	73	29
✓	Y	129.9996	99.9997	9.9999	1.0000	0.1000	0.0199	12/18	08:53	GRP	58	75	34
✓	N	129.9997	99.9997	10.0000	1.0000	0.1000	0.0199	12/19	08:12	GRP	55	72	31
✓	N	129.9997	99.9997	10.0000	1.0000	0.1000	0.0199	12/20	09:16	GRP	57	71	41
✓	Y	129.9995	99.9995	10.0000	1.0001	0.1000	0.0199	12/21	10:25	ATM	55	70	36
✓	Y	129.9997	99.9996	10.0000	1.0000	0.1000	0.0200	12/22	14:34	ATM	54	66	44
✓	N	129.9996	99.9996	10.0000	1.0000	0.1000	0.0200	12/23	09:15	ATM	57	70	44
✓	N	129.9996	99.9996	9.9999	1.0000	0.1000	0.0199	12/26	12:30	ATM	54	70	44
✓	N	129.9996	99.9997	10.0000	1.0000	0.1000	0.0200	12/27	10:30	ATM	56	72	34
✓	N	129.9997	99.9997	9.9999	1.0000	0.1000	0.0200	12/28	13:42	GRP	54	68	38
✓	N	129.9998	99.9997	9.9999	1.0001	0.1000	0.0200	12/28	07:42	GRP	55	70	36
✓	N	129.9997	99.9997	10.0000	1.0000	0.1000	0.0199	1/11/08	10:40	ATM	59	73	42
✓	Y	129.9996	99.9997	10.0000	1.0000	0.1000	0.0199	1/16/08	12:21	GRP	51	72	18
✓	N	129.9999	99.9998	10.0000	1.0000	0.1000	0.0199	1/17/08	12:37	GRP	56	71	37
✓	N	129.9998	99.9998	10.0000	1.0000	0.0999	0.0200	1/18/08	11:16	GRP	56	71	37
✓	Y	129.9995	99.9996	9.9999	1.0001	0.1000	0.0199	1/21/08	14:26	GRP	56	72	34
✓	N	129.9995	99.9996	10.0000	1.0001	0.1000	0.0199	1/22/08	15:13	GRP	56	71	37
✓	Y	129.9996	99.9996	9.9999	1.0000	0.1000	0.0199	1/23/08	08:05	GRP	54	69	36
✓	Y	129.9996	99.9996	10.0000	1.0000	0.1000	0.0200	1/24/08	07:58	GRP	54	70	33
✓	N	129.9998	99.9997	10.0000	1.0000	0.1000	0.0199	1/24/08	14:50	GRP	56	71	37
✓	N	129.9997	99.9996	10.0000	1.0000	0.1000	0.0200	1/31/08	15:05	GRP	55	69	38
✓	N	129.9996	99.9996	10.0000	1.0000	0.1000	0.0199	2/1/08	10:29	GRP	54	69	36
✓	N	129.9996	99.9996	9.9999	1.0000	0.1000	0.0199	2/2/08	16:20	ATM	56	72	41
✓	N	129.9996	99.9996	10.0000	1.0000	0.1000	0.0200	2/3/08	17:10	ATM	57	70	44



SCALE: SARTORIUS  
 MODEL: CP2224S  
 SN: 17050374

WOODSTOVE DATA SHEET 4-4 ANALYTICAL BALANCE QC RECORD SHEET

FROM: 12/30/08  
 THROUGH: 2/17/09

Level	Recali	140 g	100 g	10 g	1.0 g	100 mg	20 mg	Date	Time	Tech	Wet Bulb	Dry Bulb	& RH
✓	N	139.9995	99.9995	9.9999	1.0000	0.1000	0.0199	12/29/08	1430	ADM	58	72	42
✓	N	139.9995	99.9995	9.9999	1.0000	0.1000	0.0199	12/23/08	1057	GRP	60	76	38
✓	N	139.9994	99.9994	9.9999	1.0000	0.1000	0.0200	12/24/08	1019	ATM	59	72	43
✓	N	139.9994	99.9994	9.9999	1.0000	0.1000	0.0200	12/24/08	1142	ADM	57	72	45
✓	N	139.9994	99.9994	9.9999	1.0000	0.1000	0.0200	12/23/08	1050	ADM	60	73	37
✓	N	139.9994	99.9994	9.9999	1.0000	0.1000	0.0199	1/6/09	1157	PDG	58	75	34
✓	N	139.9994	99.9994	9.9999	1.0000	0.1000	0.0199	1/6/09	1845	ADM	60	75	37
✓	N	139.9995	99.9996	9.9999	1.0000	0.1000	0.0199	1/7/09	1530	GRP	58	70	48
✓	N	139.9994	99.9994	9.9999	1.0000	0.1000	0.0199	1/8/09	1356	PDG	60	72	49
✓	Yes	139.9995	99.9994	9.9999	1.0000	0.1000	0.0200	1/09/09	1053	PDG	58	72	42
✓	Yes	139.9993	99.9993	9.9999	1.0000	0.1000	0.0199	1/11/09	1128	JRP	55	72	31
✓	Yes	139.9994	99.9995	9.9999	1.0000	0.1000	0.0199	1/12/09	0845	PDG	59	75	38
✓	NO	139.9993	99.9993	9.9999	1.0000	0.1000	0.0200	1/13/09	0825	JRP	58	74	37
✓	Yes	139.9993	99.9994	9.9999	1.0000	0.1000	0.0199	1/14/09	1212	PDG	57	72	36
✓	NO	139.9992	99.9993	9.9999	1.0000	0.1000	0.0199	1/14/09	1420	GRP	59	75	37
✓	Yes	139.9994	99.9995	9.9999	1.0000	0.1000	0.0199	1/15/09	126	GRP	58	74	37
✓	Yes	139.9993	99.9994	9.9999	1.0000	0.1000	0.0199	1/20/09	0950	PDG	58	74	37
✓	NO	139.9993	99.9993	9.9999	1.0000	0.1000	0.0199	1/20/09	1230	PDG	56	71	34
✓	NO	139.9994	99.9994	9.9999	1.0000	0.1000	0.0200	1/20/09	1613	JRP	57	73	35
✓	NO	139.9993	99.9993	9.9999	1.0000	0.1000	0.0200	1/22/09	1138	ADM	57	72	38
✓	NO	139.9993	99.9993	9.9999	1.0000	0.1000	0.0199	1/23/09	1150	PDG	58	75	35
✓	YES	139.9992	99.9993	10.0000	1.0000	0.1000	0.0200	1/26/09	1359	JRP	56	76	35
✓	NO	139.9994	99.9995	10.0000	1.0000	0.1000	0.0199	1/27/09	1520	PDG	57	72	31
✓	NO	139.9993	99.9993	10.0000	1.0000	0.1000	0.0200	1/26/09	1452	ADM	61	75	41
✓	YES	139.9993	99.9994	10.0000	1.0000	0.1000	0.0199	1/29/09	1430	GRP	58	77	29
✓	NO	139.9995	99.9995	9.9999	1.0000	0.1000	0.0199	1/30/09	1256	PDG	60	72	49
✓	NO	139.9993	99.9994	9.9999	1.0000	0.1000	0.0199	2/1/09	1200	ADM	58	74	37
✓	NO	139.9993	99.9993	9.9999	1.0000	0.1000	0.0199	2/2/09	1350	GRP	58	77	29
✓	Yes	139.9995	99.9996	9.9999	1.0000	0.1000	0.0199	2/5/09	1118	PDG	59	72	45
✓	NO	139.9995	99.9995	9.9999	1.0000	0.1000	0.0199	2/6/09	1150	GRP	57	74	33
✓	NO	139.9994	99.9994	10.0000	1.0000	0.1000	0.0200	2/7/09	1015	ADM	49	70	19
✓	NO	139.9994	99.9994	9.9999	1.0000	0.1000	0.0199	2/16/09	1501	PDG	61	78	26
✓	NO	139.9993	99.9994	9.9999	1.0000	0.1000	0.0200	2/17/09	1439	JRP	56	78	35

SCALE: SARTORIUS  
 MODEL: CP224S  
 SN: 17050374

WOODSTOVE DATA SHEET 4-4 ANALYTICAL BALANCE QC RECORD SHEET

FROM: 2/10/09  
 THROUGH:

Level	Recali	140 g	100 g	10 g	1.0 g	100 mg	20 mg	Weight	Weight	Date	Time	Tech	Wet Bulb	Dry Bulb	& RH
Y	Y	139.9993	99.9994	9.9999	1.0000	0.1000	0.0199	0.0199	0.0199	2/10/09	1800	ATM	55	70	36
Y	Y	139.9993	99.9994	9.9999	1.0000	0.1000	0.0199	0.0199	0.0199	2/10/09	1848	JRP	56	73	32
Y	Y	139.9993	99.9994	9.9999	0.9999	0.1000	0.0199	0.0199	0.0199	2/20/09	1018	POD	57	74	33
Y	Y	139.9993	99.9994	10.0000	1.0000	0.1000	0.0200	0.0200	0.0200	2/21/09	1519	ATM	60	77	35
Y	Y	139.9993	99.9994	9.9999	1.0000	0.1000	0.0199	0.0199	0.0199	2/22/09	1222	ATM	47	59	37
Y	Y	139.9994	99.9994	9.9999	0.9999	0.1000	0.0199	0.0199	0.0199	2/23/09	1406	POD	58	70	48
Y	No	139.9994	99.9994	9.9999	1.0000	0.1000	0.0200	0.0200	0.0200	2/24/09	0953	ATM	59	76	35
Y	Yes	139.9995	99.9995	9.9999	1.0000	0.1000	0.0199	0.0199	0.0199	2/25/09	123	POD	60	76	38
Y	Yes	139.9994	99.9994	9.9999	1.0000	0.1000	0.0199	0.0199	0.0199	2-26/09	1258	JRP	55	70	36
Y	Yes	139.9993	99.9993	9.9999	1.0001	0.1001	0.0200	0.0200	0.0200	2/20/09	1330	ATM	57	74	33
Y	Yes	139.9995	99.9995	9.9999	0.9999	0.1000	0.0199	0.0199	0.0199	3/3/09	1431	POD	59	76	35
Y	NO	139.9993	99.9995	9.9999	1.0000	0.1000	0.0199	0.0199	0.0199	3/4/09	1556	JRP	56	70	40
Y	NO	139.9994	99.9994	9.9999	1.0001	0.1001	0.0200	0.0200	0.0200	3/5/09	1350	ATM	60	75	30
Y	NO	139.9993	99.9993	9.9999	1.0000	0.1000	0.0200	0.0200	0.0200	3/7/09	0850	ATM	57	71	41
Y	Yes	139.9993	99.9993	10.0000	1.0001	0.1000	0.0200	0.0200	0.0200	3/8/09	1323	ATM	55	70	36
Y	Yes	139.9993	99.9993	9.9999	1.0000	0.1000	0.0199	0.0199	0.0199	3/10/09	1212	POD	50	75	40

Woodstove Particulate  
Catch Processing Sheet  
Woodstove Data Sheet #5  
EPA M5G-1

Unit: Kuma Ashwood  
Run: EPA 5  
Date: 2/20/09  
Technicians: ATM  
Revised 1/16/98-Data Sheet #5

Filters

Filter # (Front) 714 Beaker # 25  
Final Wt. .7322 g MI 50  
Tare Wt. .6655 g Desc. Acetone  
Net Wt. .0667 g  
66.9

Final Wt. 72.6572 g 72.6562  
Tare Wt. 72.6514 g  
Net Wt. .0058 g .0048

Filter # (Rear) 713 Beaker # \_\_\_\_\_  
Final Wt. .6872 g MI \_\_\_\_\_  
Tare Wt. .6866 g Desc. \_\_\_\_\_  
Net Wt. .0006 g

Final Wt. \_\_\_\_\_ g  
Tare Wt. \_\_\_\_\_ g  
Net Wt. \_\_\_\_\_ g

Acetone Blank Calculation:

Blank Date: 12/8/07

Blank Beaker # 25 Final Wt. 72.6511 g  
MI 50 Tare Wt. 72.6512 g  
Desc. Acetone Net Wt. -0.0001 g = 0.0000  
0.0000 g ÷ 50 ml = 0.00000 g/ml

Blank Residue Value Calculation:

0.00000 g/ml acetone X 50 ml acetone = 0.0000 g  
Blank Residue Value

Total Particulate Catch Calculation

Filter: .0667 g  
Filter: .0006 g  
Beakers: .0058 g -- 0.0000 g = .0058 g  
Total Catch Blank Residue Value  
Total Catch = .0731 g

Unit Kama Ashwood  
 Run # EPA  
 Date 2/20/09  
 Technician ATM IRP PJD  
 WST6-Form1, Rev8/96

MISCELLANEOUS TEST DATA  
 WOODSTOVE DATA SHEET #8

Useable Firebox Dimensions: See QC Section Useable Volume: 2.094 ft<sup>3</sup>

Dilution Tunnel Draft (If applicable): Start .000 Stop .000 "H<sub>2</sub>O

Test Chamber Air Velocity: Start: 00.0 Stop: 00.0 Avg: 00.0 ft/min

Wet Bulb/ Start: WB: 58 °F DB: 74 °F 1.10% Amb Moisture 36 %RH

Dry Bulb Stop: WB: 60 °F DB: 78 °F 1.10% Amb Moisture 33 %RH

$\bar{X} = 1.10$  % Ambient Moisture  $\bar{X} = 34.5$  % Relative Humidity (RH)

Empty Stove Wt: 440.2 lbs.

Empty Stove Wt with Stack (Inc. Oil Seal) Wet: 763.8 lbs. Dry: 763.8 lbs.

Empty Stove Wt with Stack and Ash Ash: — lbs. Total: — lbs.

Kindling Wt. Total 5.3 lbs. Paper: .4 lbs. Wood: 4.9 lbs.

Pre Burn Fuel Wt. 10.688 + 14.070 + 10.658 Total: 35.416 lbs.

Total Kindling and Pre Burn Fuel Wt 40.716 lbs.

Coal Bed Wt-lbs: Range (3.3 - 2.7) 767.1 - 766.8 lbs. Actual: 3.0 lbs.  
766.8

Allowable Amount of Charcoal that can be removed:

Coal Bed Wt. Range  $\left( \frac{3.3}{\text{Upper Wt.}} + \frac{2.7}{\text{Lower Wt.}} / 2 \right) \times .25 = \underline{0.7}$  lbs.

Test Fuel Wt-lbs: Ideal 14.7 lbs. Range: 11.1 - 13.3 lbs. Actual: 13.332 lbs.

Test Fuel Size (pcs.) (.75 x 1.5" x 5" Flanges) 1.600 lbs 16 Pcs.

2 x 4's x 16.0 " 3 Pcs 5.966 lbs. 44.75 %

4 x 4's x 16.0 " 2 Pcs 7.366 lbs. 55.25 %

5.0526 kg.

Est. Dry Burn Rate (Kg/Hr.)  $\frac{13.332 - (13.332 \times .16449)}{2.2046} \times \frac{60}{275} = \underline{1.1024}$  Est. Dry Burn Rate (Kg/Hr)

Est EPA Heat Output (HO<sub>E</sub>) (19,140) x  $\frac{63}{100} \times 1.1024 = \underline{13,293}$  Est Heat Output (HO<sub>E</sub>) BTU's/Hr

Comments: 245 mins = 1.2374 kg/hr.

Stove Operating Data  
Woodstove Test Data Sheet #9  
Cold Start

Unit: Kuma Ashwood  
Run: EPA 5  
Date: 2/20/09  
Technician(s): AT Myren  
Data Sheet #9-Rev 1/98-Pg.2

Fire Started: 06:50

Warm up and Preburn: Primary Air: Wide open from ignition until the start of preburn when the primary air control(s) was (were) adjusted to the run setting of .428" orifice. At the run setting until the start of the test. 2 5/32 thru rod

Secondary Air: No Controls, Naturally Drafted

Secondary Burn Bypass: N/A

Charcoal Bed Preparation: Broke up, raked and leveled the coal bed prior to the addition of each warm up/pre burn fuel charge. Starting 1:30 before the start of the test, broke up, raked and leveled the coal bed. In stove for 32 seconds.

Test: Door wide open during loading 1 min 15 sec, then closed

Primary Air: Wide open from the start of the test (0:00) until 4:45. Adjusted to the run setting of .428" between 4:45 and 5:00. At the run setting of .428" open at 5:00 into the run.

Secondary Air: No Controls, Naturally Drafted.

Secondary Burn Bypass: N/A

Fan: ON/OFF during the warm up, ON/OFF Low during the preburn, ON/OFF at the start of test, ON/OFF for the first 30 minutes of test, ON/OFF Low at 30 minutes into test, ON/OFF for the rest of test.

Test Run Anomalies: This run went "south" right after 5:00. Got a good 1<sup>st</sup> 5 but then there was not enough to keep 2<sup>nd</sup>s going. Overran start

WOODSTOVE OPERATING DATA  
 WOODSTOVE DATA SHEET #9A-1

Wood Data: Kindling: A mix of the below grades

	Size	Mill	Grade	Species
Pre Burn	2X4	Forest Grove	# 2, STD # BTR	D. Fir, Sfc. GRN
Test Fuel	2X4	Forest Grove	# 2, STD # BTR	D. Fir, Sfc, GRN
	4X4	Forest Grove	No. 1	D. Fir, Sfc, GRN

All grades WCLB Rules unless otherwise noted.

Warm up Information:

1st Warm up/Pre Burn Fuel charge (10.688 lbs) added at 0712.  
 2nd Warm up/Pre Burn Fuel charge (14.070 lbs) added at 0755.  
 3rd Warm up/Pre Burn Fuel charge (10.658 lbs) added at 0852.  
 4th Warm up/Pre Burn Fuel charge (\_\_\_\_\_ lbs) added at \_\_\_\_\_.  
 5th Warm up/Pre Burn Fuel charge (\_\_\_\_\_ lbs) added at \_\_\_\_\_.  
 6th Warm up/Pre Burn Fuel charge (\_\_\_\_\_ lbs) added at \_\_\_\_\_.  
 7th Warm up/Pre Burn Fuel charge (\_\_\_\_\_ lbs) added at \_\_\_\_\_.  
 8th Warm up/Pre Burn Fuel charge (\_\_\_\_\_ lbs) added at \_\_\_\_\_.

1<sup>st</sup> Rick 4-12" 4-16" 2X4's      3<sup>rd</sup> Rick 4-12", 3-16" 2X4's  
 2<sup>nd</sup> Rick 8-16" 2X4's

The coals were scooped out of the stove immediately prior to adding the 3<sup>rd</sup> pre burn/warm up fuel charge. The stove lost 0 lbs. 2.0 lbs. of coals were put back in the stove after the scoop.

All pre burn/warm up fuel pieces were either 12 or 16 inches long. All preburn pieces/fuel charges were "ricked" in the stove. The pieces in the bottom layer in each rick contained 2 pcs that were 12 or 16 inches long and were loaded flat and perpendicular to the door. The pieces in the second layer in each rick were loaded on their side (edge) approximately parallel to the door and contained 3 or 4 pcs 16 inches long. The third layer (and fourth layer if present) was loaded flat, perpendicular to the door and contained 2 pcs 12 or 16 inches long. The majority of the pieces in each rick were in the second layer which had an approximate 0.5-1.0" space between pieces. (The loading directions indicate the direction of the longest dimension on each piece relative to the loading door opening.) Each pre burn/warm up fuel charge normally weighs within the weight range allowed for the actual test fuel charge.

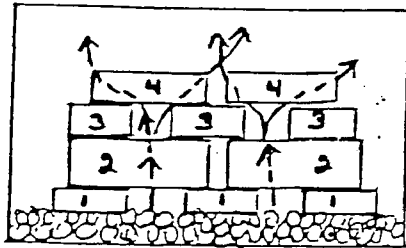
WOODSTOVE OPERATING DATA  
WOODSTOVE DATA SHEET #9A-2

Unit: Kuma Ashwood  
Run # EPA 5  
Date 2/20/09  
Technician ATM  
Page 2 of 4  
WST7-Form2-A, Rev 6/90

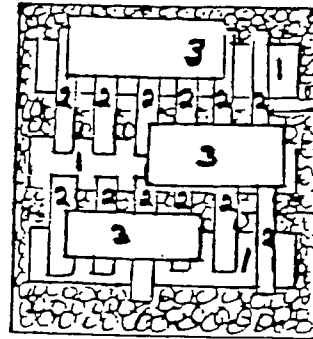
Warm up Information (cont.):

Each warm up/preburn fuel charge was ricked in exactly (as much as possible) the same manner and the weight of each rick was usually within the allowable weight range for the test fuel charge. The physical arrangement and alignment of each rick was designed to accomplish three (3) things: (1) The bottom layer was nestled firmly into the coal bed and was as close to being level with the bottom of the stove as possible, thus providing a stable loading platform for the rest of the rick, keeping it in a ricked state (as opposed to a col-lapsed or fallen down state) until the rick reached the charcoal stage and sags or collapses of its own accord. (2) It enhances the flow of primary air through the ricked preburn fuel charge, for the primary air would flow through the spaces between the pieces in the first layer and then up through the spaces between the pieces in the second, third and, if present, fourth layers. (3) It maximized, as much as possible, the surface to volume ratio of each preburn fuel charge, thereby allowing the fire immediate access to as much wood surface as possible and, thereby, insuring uniform charcoalization. All three of these enhance combustion and so get the stove as hot as possible during the warm up period, thereby maximizing the amount of heat (BTU's) stored in the stove. The actual preburn was not started until the stove surface temperatures had maximized and stabilized, thus indicating that the amount of heat stored in the stove had peaked. For this stove, the thermal storage was monitored using the Stove Top T/C surface temperature(s) and the peak value(s) obtained were 1000 °F.

898  
1000



Front View



Top View

The arrows indicate the direction of the air flow through the rick.

The primary air was adjusted to the run setting of .428" OPEN 3.5 lbs above the upper charcoal bed weight.

(2.436" on thr. Rod.)

Additional Comments:

Test Start Sequence:

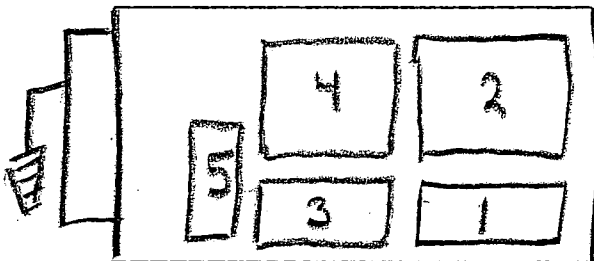
① Turned Fan off  
② Adjusted Primary Air Control to Wide Open  
③ Opened door  
④ Loaded fuel  
⑤ cleared coals away from the LPAO  
⑥ Closed door.

TOTAL ELAPSED Time: 1:15

Photo @ 1:45

Test Fuel Charge Loading Information:

Test Fuel Charge and Loading Sequence Diagram



510L

of stove view

4 X 4's: 2, 4

2 X 4's: 1, 3 & 5

Loading Sequence: 1, 2, 3, 4 & 5 last

Driest Pcs in Load 5, 3

Loaded the test fuel charge on an essentially level, Medium sized, Aug to Cool coal bed (in appearance, color and temperature for a Med Low (1.0-1.25) burn rate. Load: 1:15 Ignition: 1:10  
1:16 Vertical column of flame up to baffles (VC)  
1:45 Photo

2:50 6:15 / 1.02 (% CO<sub>2</sub> / % CO) M = Med Smoke

(3:46) Gas Balance 8.47 / 1.84 Front Tube igniting  
Secondaries the full width of 4 & 5. R/ML

4:45 - 5:00 Primary Air Control Adjusted to the run setting  
5:00 Flames decreasing. Maintained a hot pocket of coals underneath and behind pc 5. The back of the front tube was orange (hot) & Secondaries

5:30 Secondaries decreasing

6:11 Secondaries at top of VC and just behind it,  
6:45 " still decreasing 5.73 / 1.24 M



WOODSTOVE OPERATING DATA  
 WOODSTOVE DATA SHEET #9A-4

Additional Comments: 7:11 VC still decreasing  
 8:03 VC up to baffle w/ secondaries flashing @ top of VC  
 10:35 VC still increasing a bit right of center  
 11:10 VC decreasing - down to top of pc 5  
 14:11 VC up maybe just a little bit  
 14:45 Secondary flashes in VC  
 15:30 5.48 / 1.29 VC flickers right of center again, m/mh  
 16:21 VC flickers increasing in height  
 16:50 secondary flashes above pc 4 left of center  
 17:17 flames under center bottom front edge of 4 occ.  
 18:19 steady (rumbling) secondaries above pc 4,  
 VC height decreasing (Primary Secondary Flip Flop)  
 20:42 VC flickers increasing in height  
 21:35 secondaries just about went out 7.92 / 1.67  
 22:27 flames on center top edge of 5  
 25:20 7.73 / 1.52  
 26:03 secondaries forward part front tube on h side.  
 (29:03) Gas Balance 13:03 / 1.29  
 30:00 Fan On  
 (31:00) Out of balance, Strickitis, Lots of yellow  
 flames in VC and up the front of pc 5 occasionally.  
 This was not a good start.

Unit: Kuma Ashwood  
 Run: EPA 5  
 Date: 2/20/09  
 Technician: AVM JPO PUG  
 WST1-Form7-Rev11/89

FUEL MOISTURE  
 WOODSTOVE TEST DATA SHEET #10

5kg. = 11.024 lbs. 1kg. = 2.204 lbs

Room Temperature: 60.4 °F

Correction Factor: +1.0

NOTE: Record readings to the nearest 0.5% moisture  
 Uncor Values are corrected for temperature: Yes  No   
 Time Test Fuel Moisture Readings taken at: \_\_\_\_\_  
 Calibration Checks: X  Y  12.0 11.7 22.0 22.0

Pc #	Dimen	Use	Top		Bottom		Side		Piece Avg Corrected
			Uncor	Cor	Uncor	Cor	Uncor	Cor	
1	3' pcs	K	8.5	8.95	7.5	7.85	8.5	8.95	8.583
2									
3									
4	2x4-8'	P	19.0	20.3	19.5	20.9	20	21.4	20.867
5			22	23.7	22.5	24.3	21	22.6	23.533
6			19	20.3	19	20.3	18.5	19.8	20.133
7			19	20.3	19.5	20.9	19.5	20.9	20.700
8	✓	✓	18	19.2	18	19.2	18.5	19.8	19.400
9									(104.633)
10	"								
11	2x4-16	T	18	19.2	18.5	19.8	19	20.3	19.767
12			19.5	20.9	20	21.4	19	20.3	20.867
13	✓	✓	18	19.2	18	19.2	18	19.2	19.200
14	"								
15	4x4-16	T	18	19.2	18	19.2	18.5	18.8	19.400
16	✓	✓	18	19.2	18	19.2	18	19.2	19.200
17									(98.434)
18									
19	SPAWERS	T	19	20.3	19	20.3	18	19.2	19.933
20									(out) Specials

1.3  
1.906  
1.496  
3.476  
3.548

1.600

	Kindling	Pretest Fuel	Test Load
% Moisture - Dry Basis:	8.583%	20.9266%	19.6868%
% Moisture - Wet Basis:	7.905%	17.305%	16.449%

To obtain Wet from Dry:  $\frac{100 \times \% \text{ Dry Rdg.}}{100 + \% \text{ Dry Rdg.}} = \% \text{ Moisture, Wet Basis}$   
 Acceptable Ranges: 16-20% wet; 19-25% dry  
 (17.5 - 22.5 on Meter [Uncor reading] at 70°F)  
 Key for Use: K= Kindling P= Pretest Fuel T= Test Fuel

13.332  
7.366 dry  
1 10.688  
2 14.070  
3 10.658

WOOD DENSITY DETERMINATION  
WOODSTOVE TEST DATA SHEET #11

Unit: Kuma Ash wood  
Run#: EPA 5  
Date: 21 20 109  
Technician: A.T. Myren  
WST2-form11-Rev 6/90

Wood Piece: 4x4 Nominal Dimensions: 3.5 x 3.5 x 5 1/16"  
Depth (D): 8.860 cm  
Width (W): 8.875 cm  
Length (L): 14.515 cm  
14.615 cm  
14.910 cm  
14.470 cm  
Length  $\bar{X}$  = 14.6275 cm  
Volume: 1150.197 cm<sup>3</sup>  
(D X W X L)

MOISTURE: Room Temperature: 60.4 °F Correction Factor: 11.0  
Uncorrected Meter Readings Corrected for temperature: Yes  No

NOTE: Record moisture meter readings to the nearest 0.5%

	Uncor	Cor	%
Top:	15.5	16.5	%
Bottom:	17	18.1	%
Side:	15	15.9	%
$\bar{X}$ :		16.833	%

Avg % Moisture (Dry) 16.833 %

Aug % Moisture (Wet) 14.408 %

Scale: Levelled In  Out

Zeroed: In  Out

Wet Weight: 566.8 g Dry Weight: 484.6 g

% Moisture Dried Basis: 14.502 %  
[1 - (Dry Wt ÷ Wet Wt)] X 100

Into Dryer Date 2/20/09 Time 0845 Temp 200 °F  
Out of Dryer Date 3/3/09 Time 0915 Temp 192 °F  
(Minimum Time in Dryer: 24 hrs.) Minimum Dryer Temp 100°C (212°F)

Density = 484.6 g ÷ 1150.197 cm<sup>3</sup> = 0.4213 g/cm<sup>3</sup>  
(dry wt) (volume)

Pellet Fuel Moisture Content Determination

Tare Beaker Wt. \_\_\_\_\_ g

Wet Wt: \_\_\_\_\_ g - \_\_\_\_\_ g = \_\_\_\_\_ g

Gross Wet Wt. Tare Beaker Wt. Net Wet Wt.

Dry Wt: \_\_\_\_\_ g - \_\_\_\_\_ g = \_\_\_\_\_ g

Gross Dry Wt. Tare Beaker Wt. Net Dry Wt.

% Moisture Dried Basis: \_\_\_\_\_ %  
[1 - (Net Dry Wt ÷ Net Wet Wt.)] X 100

Pre Burn  
3.5 lbs. 790.6 lbs.  
Tear Sheet wt. Range 767.1 - 766.5 lbs.

PRE BURN DATA  
RECORD SHEET #13  
Range WST2-Form 16

BAFO: 28.57 MB  
PRESSURE

Unit: KUMHO Ashwood Date: 2.20.09  
Run: EPAS Technician(s): ATM JRP  
Page: 1 of 1

Hot Box On ✓

T/C#-3 4 5 6 7 8 9 10 11

Minute	Scale Weight	Burn Rate	Stack	Stove Top	Left Side	Back	Right Side	Bottom	Firebox	2nd Burn	Room Temp	Static	Comments
0	790.6	0	599	690	597	380	572	374	1037	1389	79	-075	ROKED FWD @ 36 min
5	769.9	.7	456	819	604	383	582	385	1004	1394	79	-066	Primary Air Set at 488" CRG
10	769.3	.6	419	918	607	389	584	390	990	1404	79	-065	Secondary Air Set at
15	768.7	.6	386	878	609	393	583	392	999	1408	78	-062	Fan: Low @ Start down
20	768.3	.4	365	851	608	395	583	391	984	1401	79	-059	TUNNEL ON AT: 26 mi/h.
25	767.9	.4	333	787	606	403	583	389	991	1384	79	-056	Buckets Iced ✓
30	767.7	.2	310	734	601	418	580	386	988	1237	78	-050	ANALYZERS SPANNED ✓
35	767.5	.2	286	669	590	438	572	383	960	1123	77	-047	Pumps turned on at: 56 mi/h
40	767.3	.2	289	628	575	433	561	381	945	1100	77	-048	530.4 AT AT
45	767.2	.1	264	602	553	424	543	380	899	987	77	-045	515.6 - 4.8
50	767.2	0	253	570	537	417	527	379	860	961	77	-043	Check WB/DB: 500.4 - 15.2
55	767.1	.1	244	535	517	408	509	378	833	929	77	-040	486.0 - 14.4
60	767.0	.1	236	510	502	398	493	376	804	869	77	-039	469.4 - 16.6
65	766.9	.1	231	485	487	388	478	374	784	849	76	-037	ROBE IN TUNNEL ✓
70	766.8	.1	226	469	476	381	465	370	769	837	76	-036	TUNNEL AP 455.8 - 13.1
75													442.4 - 13.1
80													432.2 - 10
85													
90													
													RAISE FWD FLAMES OUT
													STAY AT 430 ISH











Myren Consulting Inc Data Sheet P5 of 5 Unit Kuma A wood Date 2/20/09 Run PA5  
 Test EA 766.8 AT 432.2 Barometric Pressure 28.5 Technician(s) ATM JRP PDC

Time	ET min	Scale Wt.	Lbs. Left	Burn Rate	CO <sub>2</sub> v.	CO <sub>2</sub> %	O <sub>2</sub> v.	O <sub>2</sub> %	CO v.	CO %	Gas Bal	Opacity & Notes	Calc Wet B	Wet B #1	Dry B #2	Stack		
																Temp #3	Static Press	
240	1430	767.3	.5	.1	252	6.28		13.39	2.46	2.46	2.6						181	-025
245	35	767.3	.5	0	250	6.24		13.44	2.47	2.46	2.5						180	-025
250	40	767.2	.4	.1	251	6.26		13.40	2.48	2.48	2.5						179	-024
255	45	767.1	.3	.1	266	6.63		13.40	1.75	1.75	3.8						178	-024
260	50	767.1	.3	0	266	6.63		13.37	1.80	1.80	3.7						178	-024
265	55	767.0	.2	.1	269	6.70		13.19	2.01	2.01	3.3						178	-024
270	1500	766.9	.1	.1	270	6.73		13.11	2.14	2.13	3.2						178	-024
275	05	766.8	0	.1	266	6.63		13.17	2.20	2.20	3.0						178	-024
280																		
285																		
290																		
295																		
Tot																		

Total  
 Avg ÷ 56  
 1430  
 1334  
 2074  
 238

Time	EA	Top #4	Left #5	Back #6	Right #7	Bottom #8	Firebox #9	2 <sup>nd</sup> burn #10	Amb. #11	Tnl. #12	C Gas HBox #13	C Gas Injpr #14	Part. Filt. #15	Part. Cond. #16	Tube 1 #17	Tube 2 #18	Haber #19	Hoffbox #20
245	35	352	401	352	386	289	634	713	82	97	221	35	88	38	756			
250	40	350	399	350	384	289	625	710	81	97	221	35	88	37	764			
255	45	348	397	348	382	287	624	739	82	96	220	35	87	38	796			
260	50	347	395	347	380	287	622	742	82	95	220	35	86	37	799			
265	55	347	393	346	379	286	620	743	81	95	219	35	86	38	808			
270	1500	347	391	346	378	284	617	738	81	94	218	35	85	37	790			
275	05	346	389	345	378	283	613	734	81	94	218	35	85	38	787			
280		349	389	345	378	283	613	734	81	94	218	35	85	38	787			
285		349	389	345	378	283	613	734	81	94	218	35	85	38	787			
290		349	389	345	378	283	613	734	81	94	218	35	85	38	787			
295		349	389	345	378	283	613	734	81	94	218	35	85	38	787			
Tot																		

DUDA  
 Start 432.2  
 Stop 346.2  
 DAT - 840

PRE AND POST TEST ZERO/SPAN CHECK  
WOODSTOVE DATA SHEET #15-1

Colville

Site: Myren Consulting, [REDACTED], WA Date: 2/20/09 Analyte: CO<sub>2</sub>

Source: Kuma Ashwood Run #: EPA 5

Zero Cyl #: TC 3AAM154 Conc. 00.0 % CO<sub>2</sub> Cyl Press: 1470 psi

Certified by: Oxlow Date: 11/12/07

Span Cyl #: AS 90457 Conc. 12.5 % CO<sub>2</sub> Cyl Press: 1450 psi

Certified by: Matheson Tri Gas Date: 2/2/09

Analyzer: Make: Horiba Model: PIR-2000 SN: 607024

Range: 0 - 25.0% CO<sub>2</sub> Analyzer Output: 0 - 1.0 v.

Flow: 1.5 SCFH Measured by: Rotameter: X Flowmeter:         

EPA Span Value = 25.0% CO<sub>2</sub>

EPA Control Limits = + 2.5% of 25.0% CO<sub>2</sub> = + 0.625% CO<sub>2</sub>

Pre Run Audit: By: A.P. Myren Time: 928 Temp: 78 °F

Audit Results

Point #	Expected Response			Actual Response			+ Conc. Difference	Δ %
	Meter	DVM	%	Meter	DVM	%		
Zero	00.0	.000	00.0	00.0	.000	00.0	+0.05453	+0.22
Span	80.0	1.500	12.5	49.75	.499	12.38575	-0.11425	-0.91

Comments:

Post Run Audit: By: A.P. Myren Time: 1600 Temp: 80 °F

Audit Results

Point #	Expected Response			Actual Response			+ Conc. Difference	Δ %
	Meter	DVM	%	Meter	DVM	%		
Zero	00.0	.000	00.0	00.0	.000	00.0	+0.07925	+0.32
Span	80.0	1.500	12.5	49.5	.499	12.38575	-0.11425	-0.91

Comments:

+ Conc. Difference = Act % - Exp (Std) %  
 Zero % Difference =  $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Full Scale Value}} \times 100$   
 Span % Difference =  $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Exp \% (ppm)}} \times 100$

PRE AND POST TEST ZERO/SPAN CHECK  
WOODSTOVE DATA SHEET #15-3

Colville

Site: Myren Consulting, Woodville, WA Date: 2/20/09 Analyte: CO

Source: Kumar Ashwood Run #: EPA 5

Zero Cyl #: TC3AAM154 Conc. 00.0 % CO Cyl Press: 1500 psi

Certified by: Oxarc Date: 11/12/07

Span Cyl #: \_\_\_\_\_ Conc. 2.00 % CO Cyl Press: 1450 psi

Certified by: Matheson Tri Gas Date: \_\_\_\_\_

Analyzer: Make: HORIBA Model: MEXA 311GE SN: GE-30075

Range: 0 - 10.0% CO Analyzer Output: 0 - 10 ✓

Flow: 1.5 SCFH Measured by: Rotameter: X Flowmeter: \_\_\_\_\_

EPA Span Value = 5.0% CO  
EPA Control Limits = +2.5% of 5.0% CO = + 0.125% CO

Pre Run Audit: By: A.T. Myren Time: 9:28 Temp: 78 °F

Point #	Expected Response			Actual Response			+ Conc. Difference	Δ %
	Meter	DVM	%	Meter	DVM	%		
Zero	00.0	00.0	00.0	00.0	000	00.043	-0.00443	-0.04
Span	2.00	2.00	2.00	2.00	1.99	1.9959	-0.00411	-0.21

Comments: \_\_\_\_\_

Post Run Audit: By: A.T. Myren Time: 16:00 Temp.: 80 °F

Point #	Expected Response			Actual Response			+ Conc. Difference	Δ %
	Meter	DVM	%	Meter	DVM	%		
Zero	00.0	00.0	00.0	0.00	000	-0.0043	-0.00443	-0.04
Span	2.00	2.00	2.00	1.95	1.95	19.5569	-0.04431	-2.22

Comments: \_\_\_\_\_

+ Conc. Difference = Act % - Exp (Std) %  
 Zero % Difference =  $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Full Scale Value}} \times 100$   
 Span % Difference =  $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Exp \% (ppm)}} \times 100$

Unit: Kuma Ashwood  
 Run: EPA 5  
 Date: 21 20 199  
 Technicians: HTM JRP PDG  
 WS: 5-Form3-Rev11/89

QUALITY CHECKS  
 WOODSTOVE DATA SHEET #16

Ambient = Tr: \_\_\_\_\_ °F T/C#30: \_\_\_\_\_ °F  
 Thermocouple Check (at ambient): T/C#1: — °F; T/C#2: 65.8 °F;  
 T/C #3: 80.7 °F; T/C #4: 93.8 °F; T/C #5: 100.8 °F;  
 T/C #6: 90.8 °F; T/C #7: 94.0 °F; T/C #8: 105.6 °F;  
 T/C #9: 105.8 °F; T/C #10: 105.2 °F; T/C #11: 60.4 °F;  
 T/C #12: 64.8 °F; T/C #13: 65.4 °F; T/C #14: 60.1 °F;  
 T/C #15: 64.7 °F; T/C #16: 55.9 °F; T/C #17: 95.8 °F;  
 T/C #18: — °F; T/C #19: \_\_\_\_\_ °F; T/C #20: \_\_\_\_\_ °F;  
 T/C #21: \_\_\_\_\_ °F; T/C #22: \_\_\_\_\_ °F; T/C #23: \_\_\_\_\_ °F;  
 T/C #24: \_\_\_\_\_ °F; T/C #25: \_\_\_\_\_ °F; T/C #26: \_\_\_\_\_ °F;

Comments: \_\_\_\_\_

Thermocouple Readout: Pretest Zero/Span Check and Calibration:  
 Zero (°F): 0.4 °F Adj to: — °F Post Test Check Zero (0°F): 1.0 °F % Difference: +0.02  
 Span (2000°F): 2000.5 °F Adj to: — °F Span (2000°F): 2002.5 °F % Difference: +0.10

(Allowable % Difference = 1.5%. Use formulas on Woodstove Data Sheet #15 to calculate % Difference) In Degrees Absolute.

Thermocouple Readout Pretest Linearity Check  
 0°F = 0.5 °F; 200°F = 202.1 °F; 400°F = 399.6 °F;  
 600°F = 601.8 °F; 800°F = 802.1 °F; 1000°F = 1001.2 °F;  
 1200°F = 1198.9 °F; 1400°F = 1399.9 °F; 1600°F = 1600.4 °F;  
 1800°F = 1800.6 °F; 2000°F = 2000.5 °F

Combustion Gas (CO<sub>2</sub>, O<sub>2</sub>, CO) Train Leak Check: Pre OK JRP Post OK PDG  
 Draft (Static) Gauge Zero Check: Pre OK JRP Post OK JRP

Scale Check Pre (Wt, #'s): 769.9 - 764.9 = 5.0 lbs / 5.0 lbs = 0%  
 Post (Wt, #'s): 766.7 - 771.7 = 5.0 lbs / 5.0 lbs = 0%

Back cleaned prior to the run: Yes \_\_\_\_\_ No   
 Tunnel cleaned prior to the run: Yes \_\_\_\_\_ No

## SCALE CALIBRATION RECORD

**CUSTOMER:** Myren Consultants      **DATE:** 12-8-97

**WORK ORDER NO.:**      **PO NUMBER:**

<u>EQUIPMENT MFG</u>	<u>SERIAL NUMBER</u>	<u>SPECIFICATIONS</u>	<u>WEIGHT USED</u>	<u>INITIAL READINGS</u>	<u>FINAL READINGS</u>
1) Panther	4466459	1000 x .1 lb	Ø	Ø	
	<u>PASS.....FAIL</u>		100.0	100.0	

**NOTES:**

0.0 = 0.0  
 50.0 = 50.0  
 100.0 = 100.0  
 200.0 = 200.0  
 300.0 = 300.0  
 400.0 = 400.0  
 500.0 = 500.0

600.0 = 600.0  
 650.0 = 650.0

			500.0	500.0	
			1000.0	1000.0	
			Ø	Ø	
			XXXXXX	XXXXXX	XXXXXX

1)					
	<u>PASS.....FAIL</u>				

**NOTES:**


**ADDITIONAL COMMENTS:**

**LAST CHECKED:**      **NEXT CHECK DUE:** 6-98

**WEIGHTS CERTIFIED:** 6-96      **TECHNICIAN:** Paul F. Becherini



# QUALITY CONTROL SERVICES

LABORATORY AND METROLOGY EQUIPMENT: SALES AND SERVICE  
2340 S.E. 11th Avenue • Portland, Oregon 97214  
P.O. Box 14831 • Portland, Oregon 97293 • (503) 236-2712 • FAX: (503) 235-2535

Myren Consulting  
512 Williams Lake Road  
Colville, WA 99114

## CERTIFICATE OF SERVICE AND CALIBRATION

The measurement and test equipment initialed and dated on the QCS Report of Service and Calibration #29683 has been serviced and calibrated by Quality Control Services using test standards that are traceable to the National Institute of Standards and Technology (N.I.S.T.) through QCS master standard #1550.01. Unless otherwise noted in the comments section of the report, all measurement and test equipment meets or exceeds customer calibration tolerances.

Technician Signature: \_\_\_\_\_

Date: 11/14/08

Technician Signature: \_\_\_\_\_

Date: \_\_\_\_\_





# QUALITY CONTROL SERVICES

LABORATORY AND METROLOGY EQUIPMENT: SALES AND SERVICE

2340 S.E. 11th Avenue • Portland, Oregon 97214

P.O. Box 14831 • Portland, Oregon 97293 • (503) 236-2712 • FAX: (503) 235-2535

Date: 08/04/2004

Report Number: MYRCO 040804

Customer

Myren Consulting  
512 Williams Lake Road  
Colville, WA. 99114  
Ben Myren

## CERTIFICATE OF CALIBRATION

THE INSTRUMENTS LISTED BELOW HAVE BEEN SERVICED AND CALIBRATED BY QUALITY CONTROL SERVICES ON THE DATE INDICATED. SERVICE CONSISTS OF ACCURACY TESTS, ADJUSTING TO MANUFACTURER OR CUSTOMER SPECIFICATIONS AND COMPLETE CALIBRATION WITH STANDARDS TRACEABLE TO THE NATIONAL INSTITUTE OF STANDARDS AND TECHNOLOGY (N.I.S.T.).

Item	Make	Model	Serial Number	Location	Contact	Cal. Date	Cal. Date Due
Balance	Sartorius	QC35EDE-S	16507622	N/A	Ben Myren	07/19/2004	07/2005

### STANDARDS USED FOR THIS CALIBRATION:

Item:	Make:	Model:	Serial Number	NIST ID:	Cal. Date:	Cal. Due:
1mg-5kg	Rice Lake	1mg to 5kg	2004W	822/265349-01	08/20/2003	08/2004

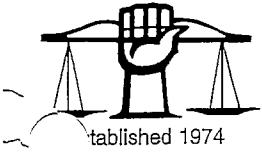
Technician:

D. Wright

Signature

D. Wright





# QUALITY CONTROL SERVICES

LABORATORY AND METROLOGY EQUIPMENT: SALES AND SERVICE  
2340 S.E. 11th Avenue • Portland, Oregon 97214  
P.O. Box 14831 • Portland, Oregon 97293 • (503) 236-2712 • FAX: (503) 235-2535

Iyren Consulting  
12 Williams Lake Road  
Solville, WA 99114

## CERTIFICATE OF CALIBRATION

Certificate Date: 4/6/08

The instruments listed below have been serviced and calibrated by Quality Control Services on the date indicated. Service consists of accuracy tests, adjusting to manufacturer or customer specifications and complete calibration with standards traceable to the National Institute of Standards(NIST).

Item	Make Model	Serial Number Customer's ID	Location	Contact	Calibration Date	Calibration Due Date
Balance	Sartorius CP224S	17050374	Lab	Ben Myren	4/1/08	10/2008

## STANDARDS

Item	Make	Model	Serial #	NIST ID	Cal Date	Cal Due
Weight Set	R.L./Troemner	1MG-25KG	A45	822/274334-07	5/7/07	8/2008

Technician: D. Deleasa

Signature: *D. Deleasa*

ID: MYRC02

## DENSITY STANDARD USED FOR TROEMNER PRECISION WEIGHTS

Troemner Inc. adjusts all new weights and all weights received for recalibration on the basis of apparent mass versus material of density 8.0g/cm<sup>3</sup> at 20°C. This action is in accordance with the recommendations of the American Society for Testing and Materials specification ANSI/ASTM E 617 and the International Organization of Legal Metrology (OIML) International Recommendation No. 20.

Previously, all weights had usually been adjusted on the basis of apparent mass versus "brass," a hypothetical material of defined density 8.4g/cm<sup>3</sup> at 0°C and 8.3909g/cm<sup>3</sup> at 20°C. This practice originated in the early 1800's and was adopted in all of the English speaking countries as well as a number of other countries. Now most mass standards and test weights are made from stainless steel (density ranges from 7.77g/cm<sup>3</sup> to 8.0g/cm<sup>3</sup>). A number of countries have adopted the recommendations of OIML and the foremost balance manufacturers are adjusting the built-in weights in their balances on the basis of apparent mass versus 8.0g/cm<sup>3</sup>. In order to smooth the transition in this country, the Reports of Calibration of the National Bureau of Standards are reporting the corrections to calibrated mass standards on both bases.

In terms of normal weighing procedures the change is very small. For a given weight, the mass value assigned on the basis of apparent mass versus density 8.0g/cm<sup>3</sup> material will be 7 parts per million higher than the value assigned on the basis of apparent mass versus "density 8.4g/cm<sup>3</sup>" material. In many cases the allowed weight adjustment tolerances are so

large that this change is immaterial although closely adjusted weights often have a smaller tolerance than the correction change. For example at the 1 kilogram level the change is 7 mg. For comparison the ANSI/ASTM E 617 Class 6 tolerance for 1 kilogram is 100 mg while the Class 3 tolerance is 2.5 mg. A detailed discussion of mass and mass values is given in Reference 3.

Precision Weights manufactured by Troemner Inc. to ASTM Class 1, 1.1, 2, 3, 4, 5, and 6 tolerances and the equivalent OIML and NBS tolerances are of the following materials:

Designation	Base Material	Density	Weight Range
Stainless Steel	18-8	7.84g/cm <sup>3</sup> at 20°C	1 g & larger
Stainless Steel	18-8	8.0g/cm <sup>3</sup> at 20°C	50 mg to 500 mg
Aluminum	1100	2.7g/cm <sup>3</sup> at 20°C	30 mg & smaller

### References:

1. ANSI/ASTM E 617  
Available from:  
Troemner Inc. 6925 Greenway Ave., Philadelphia, Pa. 19142  
American Society for Testing and Materials, 1916 Race Street, Philadelphia, Pa. 19103
2. OIML INTERNATIONAL RECOMMENDATION No. 20  
Available from:  
Organisation Internationale De Metrologie Legale  
11 Rue Trugot - 75009 Paris, France
3. NBS MONOGRAPH 133, MASS AND MASS VALUES  
Available from:  
Superintendent of Documents, U.S. Government  
Printing Office  
Washington, D.C. 20402  
Order by SD Catalog No. C13,44:1331 Stock Number  
0903-01178



**TROEMNER INC.**

Manufacturers of Precision Weights...  
Mass Standards • Balances • Laboratory Apparatus  
8825 Greenway Avenue - Philadelphia, Pa. 19142  
215724-0650

Wts. used for Scale QC Checks, P. 4-4.

M. N CONSULTING, INC.  
 512 Williams Lake Road  
 Colville, WA 99114  
 Office: 509 684 1154  
 Lab: 509 685 9458

Calibration Data Sheet # 66  
 Revision 1 8/25/08

THERMOCOUPLE CALIBRATION

DATE: 11/9/08  
 TECHNICIAN: A. Timmyren

T/C #	Location	Ice Water Bath (° F)	Boiling Water (° F)
1.	Wet Bulb	33	209
2.	Dry Bulb	33	209
3.	Stack	34	209
4.	Stove Top	33	208
5.	Left Side	33	209
6.	Back	33	208
7.	Right Side	34	209
8.	Bottom	33	209
9.	Firebox	34	209
10.	2 <sup>nd</sup> Burn/ Cat	34	209
11.	Ambient	33	209
12.	Tunnel	34	209
13.	C Gas Hot Box	34	209
14.	C Gas Impinger Exit	34	209
15.	Particulate Filter #1	33	208
16.	Condenser #1	33	209
17.	Particulate Filter #2	33	208
18.	Condenser #2	34	208
19.	Extra	33	208
20.	Extra	33	208
21.	Extra	34	208

Thermocouples checked against

Reference Thermometer #: ERTCO CAT 1005-3FC CAT 517 SN1697  
 Ice Water Bath: 32.5 °F  
 Boiling Water: 208.9 °F  
 Room Temp: 63 °F  
 BP: 28.17 " Hg

**ALTEK**

**CERTIFICATE OF CALIBRATION**

This is to Certify that your Altek Unit has been calibrated using standards whose accuracies are traceable to the National Institute of Standards and Technology (formerly NBS) within the limits of the NIST Calibration Services. Actual records pertaining to these standards are on file and are available for examination.

Certified by: Altek Industries Corp.  
Recommend Recalibration: Annually

In service date

4/11/96

Model

K2100F

Serial No.

Serial # 177533

*T. Kuech*

Calibration Technician

31 Aug. 95

Factory Calibration Date

**ALTEK INDUSTRIES CORP**

210 Commerce Drive, Rochester, NY 14623, U.S.A.  
(716) 334-3720; FAX (716) 334-6673

800-32-ALTEK

800-322-5835

Anywhere in USA

MYREN CONSULTING, INC.  
 512 Williams Lake Road  
 Colville, WA 99114  
 Office: 509 684 1154  
 Lab: 509 685 9458

Calibration Data Sheet # 65  
 Revision 1 3/3/04

THERMOCOUPLE READOUT CALIBRATION

DATE: 11/9/08  
 TECHNICIAN: A. Myren

Thermocouple Readout Manufacturer: Omega

Model #: 4108-K Serial #: 99110582 Type: K Range: 0-2000°F

Location: Dial #1 T/C Readout

Calibrated with: Altec

As found: 0° F = -0.6 Adjusted to: 0.00  
 2000° F = 1999.1 Adjusted to: 2000.0

Temp (°F)	Readout (°F)	% Dif	Temp (°F)	Readout (°F)	% Dif	Temp (°F)	Readout (°F)	% Dif
0	0.0	0.0	800	801.0	+0.08	1600	1599.3	-0.03
100	99.7	+0.05	900	899.5	-0.04	1700	1698.5	-0.07
200	201.1	+0.17	1000	1000.2	+0.01	1800	1799.2	-0.04
300	299.6	-0.05	1100	1099.5	-0.03	1900	1899.6	+0.02
400	398.6	-0.16	1200	1197.8	-0.13	2000	2000.0	0.0
500	499.7	-0.03	1300	1298.9	-0.06			
600	600.8	+0.08	1400	1398.7	-0.07			
700	699.6	-0.03	1500	1499.2	-0.04			

$$\% \text{ Dif} = \frac{(\text{Reference Temperature } ^\circ\text{F} + 460) - (\text{Readout Temperature } ^\circ\text{F} + 460)}{\text{Reference Temperature } ^\circ\text{F} + 460}$$

Or

$$\% \text{ Dif} = \frac{(\text{Reference Temperature } ^\circ\text{C} + 273) - (\text{Readout Temperature } ^\circ\text{C} + 273)}{\text{Reference Temperature } ^\circ\text{C} + 273}$$

EN CONSULTING, INC.  
 512 Williams Lake Road  
 Colville, WA 99114  
 Office: 509 684 1154  
 Lab: 509 685 9458

Calibration Data Sheet # 65  
 Revision 1 3/3/04

THERMOCOUPLE READOUT CALIBRATION

DATE: 11/19/08  
 TECHNICIAN: W. Muren

Thermocouple Readout Manufacturer: Omega

Model #: 115 KF Serial #: 4487 K7 Type: K Range: 0 - 1900 °F

Location: 456 - 0 Meter Box

Calibrated with: Altec

As found: 0° F = 000 Adjusted to: ---  
 1900° F = 1898 Adjusted to: ---

Temperature (°F)	Readout (°F)	% Dif	Temperature (°F)	Readout (°F)	% Dif
0	0	0	800	798	-0.16
100	96	-0.71	900	897	-0.22
200	202	+0.30	1000	999	-0.07
300	298	-0.26	1100	1097	-0.19
400	399	-0.12	1200	1198	-0.12
500	498	-0.21	1300	1297	-0.17
600	599	-0.09	1400	1398	-0.11
700	696	-0.34	1500	1497	-0.15
			1600	1598	-0.10
			1700	1698	-0.09
			1800	1797	-0.14
			1900	1897	-0.13
			2000	---	---

$$\% \text{ Dif} = \frac{(\text{Reference Temperature } ^\circ\text{F} + 460) - (\text{Readout Temperature } ^\circ\text{F} + 460)}{\text{Reference Temperature } ^\circ\text{F} + 460}$$

Or

$$\% \text{ Dif} = \frac{(\text{Reference Temperature } ^\circ\text{C} + 273) - (\text{Readout Temperature } ^\circ\text{C} + 273)}{\text{Reference Temperature } ^\circ\text{C} + 273}$$

THERMOMETER CALIBRATION  
 DATE: 11/9/08      TECHNICIAN: A. T. Mynum  
 MANUFACTURER: ERICO      FISHITZ      Taylor      Taylor      Premium  
 CAT #.      1005-3PC      S17      ASTM-59F      1330 N/A      1330 N/A      -  
 SERIAL NO.      1697      K85-163      A-D 11544      WB      DB      -  
 RANGE:      -100.10°C      0-200°C      0-100°F      20-120°F      20-120°F      0-220°F  
 GRADUATIONS:      0.1°C      1.0°C      1°F      1°F      1°F      2°F  
 TYPE:      Tube      Tube      Tube      Tube      Tube      Dial  
 TEMP. POINT  
 1      1.1      1.0      83      83      83      85  
 2      7.2      8.0      46      46      47      49  
 3      15.6      16.0      61      62      62      64  
 4      37      38      100      100      100      104

COMMENTS:

$^{\circ}\text{F} = (^{\circ}\text{C} \times 9/5) + 32$   
 $^{\circ}\text{C} = (5/9) (^{\circ}\text{F} - 32)$

## R E P O R T O F C A L I B R A T I O N

## LIQUID-IN-GLASS-THERMOMETER

THE THERMOMETER WAS TESTED IN A LARGE, CLOSED-TOP, ELECTRICALLY HEATED, LIQUID BATH, BEING "IMMERSED" 76MM. THE TEMPERATURE OF THE ROOM WAS ABOUT 25 DEGREES C (77 DEGREES F). IF THE THERMOMETER IS USED UNDER CONDITIONS WHICH WOULD CAUSE THE AVERAGE TEMPERATURE OF THE EMERGENT LIQUID COLUMN TO DIFFER MARKEDLY FROM THAT PREVAILING IN THE TEST, APPRECIABLE DIFFERENCES IN THE INDICATIONS OF THE THERMOMETER WOULD RESULT.

THE TABULATED CORRECTIONS APPLY PROVIDED THE ICE-POINT READING, TAKEN AFTER EXPOSURE FOR NOT LESS THAN 3 DAYS TO A TEMPERATURE OF ABOUT 20 DEGREES C (70 DEGREES F) IS 0.00 DEGREES C. IF THE ICE-POINT READING IS FOUND TO BE HIGHER (OR LOWER) THAN STATED, ALL OTHER READINGS WILL BE HIGHER (OR LOWER) TO THE SAME EXTENT. IF THE THERMOMETER IS USED AT A GIVEN TEMPERATURE SHORTLY AFTER BEING HEATED TO A HIGHER TEMPERATURE. AN ERROR OF 0.01 DEGREES OR LESS, FOR EACH 10 DEGREE DIFFERENCE BETWEEN THE TWO TEMPERATURES, MAY BE INTRODUCED. THE TABULATED CORRECTIONS APPLY IF THE THERMOMETER IS USED IN THE UPRIGHT POSITION; IF USED IN A HORIZONTAL POSITION, THE INDICATIONS MAY BE A FEW HUNDREDTHS OF A DEGREE HIGHER.

TEST NUMBER: 152439  
DATE: 07/16/96  
STANDARD SERIAL NO. 128239  
IDENTIFICATION NO. 88024



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Charles Tang-Nian  
QUALITY CONTROL MANAGER



R E P O R T O F C A L I B R A T I O N  
LIQUID-IN-GLASS-THERMOMETER

CALIBRATED BY EVER READY THERMOMETER CO.

MARKED: ERTCO CAT 1005-3FC S/N-1697  
RANGE: -1 TO +101 DEGREES C IN 0.1 DEGREE GRADUATIONS.

THERMOMETER READING	CORRECTION (ITS-90)**
0.00 C	0.00 C
10.00	0.00
20.00	0.00
30.00	0.00
37.00	0.00
40.00	0.00
50.00	0.00
56.00	0.00
60.00	0.02
70.00	0.00
80.00	0.00
90.00	0.00
100.00	0.00

\*\* ALL TEMPERATURES IN THIS REPORT ARE BASED ON THE INTERNATIONAL TEMPERATURE SCALE OF 1990 (ITS-90) PUBLISHED IN THE METROLOGIA 27, NO. 1, 3/10/90.

THIS THERMOMETER WAS CALIBRATED AGAINST A STANDARD CALIBRATED AT THE NATIONAL INSTITUTE OF STANDARDS AND TECHNOLOGY (NIST) FORMERLY THE NATIONAL BUREAU OF STANDARDS (NBS) IN ACCORDANCE WITH ASTM METHOD E 77, AND NBS MONOGRAPH 174.

FOR A DISCUSSION OF ACCURACIES ATTAINABLE WITH SUCH THERMOMETERS SEE NBS MONOGRAPH 250-23.

IF NO SIGN IS GIVEN ON THE CORRECTION, THE TRUE TEMPERATURE IS HIGHER THAN THE INDICATED TEMPERATURE; IF THE SIGN GIVEN IS NEGATIVE, THE TRUE TEMPERATURE IS LOWER THAN THE INDICATED TEMPERATURE. TO USE THE CORRECTIONS PROPERLY, REFERENCE SHOULD BE MADE TO THE NOTES GIVEN BELOW.

CONTINUED

TEST NUMBER: 152439  
DATE: 07/16/96  
STANDARD SERIAL NO. 128239  
NIST IDENTIFICATION NO. 88024

DRY GAS METER CALIBRATION DATA

Date 11/9/08 Calibration Meter # 1052202 Console Leak Check Front 0.003 CFM  
 TM 1.000  
 Back 0.000 H<sub>2</sub>O / min  
 Meter Box # 45G-P Barometric Pressure, Bp = 28.16" Hg Pitot Leak Check N/A  
 Calibrated by A.T. Myer Dry Gas Meter # 0039270 Electrical Check OK

Y = 1.9978

Orifice (dH) in. H <sub>2</sub> O	Gas Volume			Temperature				Time (t), min.
		Cal. Meter (Vc), cu.ft.	Dry Gas Meter (Vm), cu.ft.	Cal. Meter (Tc), F	Dry Gas Meter			
					Inlet (Tm1), F	Outlet (Tm2), F		
<u>.80</u>								
<u>.80</u>	init.	504,671	759,000	init.	66 65	67 71	67 71	10:01.31
<u>.80</u>	final	513,504	767,851	final	63 63	73	73	19.022
<u>.80</u>	total	8,833	9,851	avg.	63.8		70.3	
- 523.3 - 530.2								
<u>.90</u>								
<u>.90</u>	init.	514,159	768,500	init.	63 63	73 76	74 76	11:05.86
<u>.90</u>	final	520,190	774,570	final	62 62	78	78	11.098
<u>.90</u>	total	6,031	6,070	avg.	62.3		75.8	
- 522.2 - 535.8								
<u>1.00</u>								
<u>1.00</u>	init.	520,811	775,200	init.	62 63	78 80	78 80	14:34.09
<u>1.00</u>	final	528,927	783,398	final	62 62	82	82	14.568
<u>1.00</u>	total	8,116	8,198	avg.	62.2		80	
- 522.2 - 540								
<u>1.50</u>								
<u>1.50</u>	init.	530,118	784,600	init.	62 62	82	82	11:19.89
<u>1.50</u>	final	537,846	792,414	final	62 62	84	84	11.332
<u>1.50</u>	total	7,728	7,814	avg.	62		83	
- 522.2 - 543								
<u>2.00</u>								
<u>2.00</u>	init.	538,824	793,400	init.	63 62	84	84	9:19.50
<u>2.00</u>	final	546,165	800,803	final	62 62	86	86	9.325
<u>2.00</u>	total	7,341	7,403	avg.	62.25		85	

Vac  
0  
0  
0  
0  
0  
0  
0  
0  
0  
0

Y =  $\frac{V_c \cdot P_b (T_m + 460)}{V_d (P_b + dH/13.6) (T_c + 460)}$       dH =  $\frac{0.0317 \text{ dH}}{P_b (T_{m2} + 460)} [(T_c + 460) \theta / V_c]^2$

$$Y = \frac{(Y_c)(V_c)(P_b)(T_m + 460)}{(V_d)(P_b + \Delta H/13.6)(T_c + 460)} =$$

$$Y = \frac{(0.9978)(8.833)(28.16)(\overset{530.3}{703} + 460)}{(8.851)(28.16 + \overset{80}{13.6})(\overset{535.8}{638} + 460)} = \frac{131,615.188}{130,826.059} = \underline{1.00603}$$

$$Y = \frac{(0.9978)(6.081)(28.16)(\overset{523.8}{758} + 460)}{(6.070)(28.16 + \overset{90}{13.6})(\overset{522.3}{623} + 460)} = \frac{90,796.308}{89,487.169} = \underline{1.01463}$$

$$Y = \frac{(0.9978)(8.1165)(28.16)(\overset{540}{80} + 460)}{(8.198)(28.16 + \overset{1.00}{13.6})(\overset{522.2}{622} + 460)} = \frac{123,151.216}{120,867.615} = \underline{1.01889}$$

$$Y = \frac{(0.9978)(7.728)(28.16)(\overset{543}{83} + 460)}{(7.814)(28.16 + \overset{1.50}{13.6})(\overset{522}{62} + 460)} = \frac{117,907.951}{115,811.929} = \underline{1.02251}$$

$$Y = \frac{(0.9978)(7.3365)(28.16)(\overset{545}{85} + 460)}{(7.403)(28.16 + \overset{2.085}{13.6})(\overset{522.25}{62.25} + 460)} = \frac{112,847.024}{109,448.332} = \underline{1.02648}$$

Y FACTOR      VARIATION (± 0.02 ALLOWED FROM AVERAGE Y)

<u>1.00603</u>	<u>-0.01168</u> ✓
<u>1.01463</u>	<u>-0.00308</u> ✓
<u>1.01889</u>	<u>+0.00118</u> ✓
<u>1.02251</u>	<u>+0.00480</u> ✓
<u>1.02648</u>	<u>+0.00877</u> ✓

Avg Y 1.01771 ✓

$$\Delta H@ = \frac{(0.0317)(\Delta H)}{(Pb)(T_{mo} + 460)} \left[ \frac{(T_w + 460)(\Theta)}{(Y_c)(V_c)} \right]^2 =$$

$$\Delta H@ = \frac{(0.0317)(.80)}{(28.16)(70.3 + 460)} \left[ \frac{(68.8 + 460)(18.024)}{(1.9978)(8.833)} \right]^2 = 1.94818 -$$

$$\Delta H@ = \frac{(0.0317)(.90)}{(28.16)(76 + 460)} \left[ \frac{(623 + 460)(11.098)}{(1.9978)(6.031)} \right]^2 = 1.75375 -$$

$$\Delta H@ = \frac{(0.0317)(1.00)}{(28.16)(80 + 460)} \left[ \frac{(622 + 460)(11.568)}{(1.9978)(8.1165)} \right]^2 = 1.83942 -$$

$$\Delta H@ = \frac{(0.0317)(1.50)}{(28.16)(83 + 460)} \left[ \frac{(62 + 460)(11.337)}{(1.9978)(7.728)} \right]^2 = 1.83000 -$$

$$\Delta H@ = \frac{(0.0317)(2.025)}{(28.16)(85 + 460)} \left[ \frac{(6225 + 460)(9.325)}{(1.9978)(7.8365)} \right]^2 = 1.85116 -$$

<u>ΔH@</u>	<u>VARIATION (± 0.20 ALLOWED)</u>
<u>1.94818</u>	<u>+0.1037</u> ✓
<u>1.75375</u>	<u>-0.0908</u> ✓
<u>1.83942</u>	<u>-0.0081</u> ✓
<u>1.83000</u>	<u>-0.0145</u> ✓
<u>1.85116</u>	<u>+0.0067</u> ✓
<u>AVG ΔH@</u>	<u>1.84450</u> ✓

METER BOX CALIBRATION AUDIT

Test Data										
Run #	1	2	3	4	5	6	7	8	9	10
Avg. Δ H	0.9	0.9	0.9	0.9	0.9	0.9	0.9			
Max Vac	0	0	0	0	0	0	0			

Avg. Test Series Δ H: 0.9 in H<sub>2</sub>O. Test Series Max Vac: 0 in Hg

Audit Dry Gas Meter: Rockwell 1052202 Correction (Y) Factor: 0.9978

Test Dry Gas Meter: 45G-P 3039270 Correction (Y) Factor: 1.0177

Audit Data

	Audit #1	Audit #2	Audit #3	
BP:	<u>28.13</u>	<u>28.12</u>	<u>28.12</u>	"Hg
Vac:	<u>0.0</u>	<u>0.0</u>	<u>0.0</u>	"Hg
Audit Meter:				
Final Vol	<u>808.611</u>	<u>814.440</u>	<u>821.122</u>	
Initial Vol	<u>802.368</u>	<u>808.742</u>	<u>814.674</u>	
Vol (V <sub>w</sub> , ft <sup>3</sup> )	<u>6.243</u>	<u>5.698</u>	<u>6.448</u>	
Audit Meter:				
Initial	<u>64</u>	<u>62</u>	<u>62</u>	
Temp (°F)(T <sub>w</sub> )				
Mid	<u>63</u>	<u>61</u>	<u>61</u>	
Final	<u>62</u>	<u>61</u>	<u>61.5</u>	
Avg (°F/°A)	<u>63 (523)</u>	<u>61.3 (521.3)</u>	<u>61.5 (521.5)</u>	
Δ H (in H <sub>2</sub> O)				
Initial	<u>0.90</u>	<u>0.90</u>	<u>0.90</u>	
Mid	<u>0.90</u>	<u>0.90</u>	<u>0.90</u>	
Final	<u>0.90</u>	<u>0.90</u>	<u>0.90</u>	
Avg	<u>0.90</u>	<u>0.90</u>	<u>0.90</u>	
Dry Gas Meter:				
Final Vol	<u>894.764</u>	<u>900.653</u>	<u>907.445</u>	
Initial Vol	<u>888.500</u>	<u>894.900</u>	<u>900.900</u>	
Vol (V <sub>d</sub> , ft <sup>3</sup> )	<u>6.264</u>	<u>5.753</u>	<u>6.545</u>	
Dry Gas Meter				
Initial	<u>67</u>	<u>70</u>	<u>73</u>	
Temp (°F):Inlet				
Mid	<u>68.5</u>	<u>73</u>	<u>75</u>	
Final	<u>70</u>	<u>74</u>	<u>75</u>	
Avg (°F/°A)	<u>68.5 (528.5)</u>	<u>72.3 (532.3)</u>	<u>74.3 (534.3)</u>	
Dry Gas Meter				
Initial	<u>67</u>	<u>70</u>	<u>73</u>	
Temp (°F):Outlet				
Mid	<u>68.5</u>	<u>73</u>	<u>75</u>	
Final	<u>70</u>	<u>74</u>	<u>75</u>	
Avg (°F/°A)	<u>68.5 (528.5)</u>	<u>72.3 (532.3)</u>	<u>74.3 (534.3)</u>	
Avg Dry Gas				
Meter Temp (T <sub>m</sub> -°F/°A)	<u>68.5 (528.5)</u>	<u>72.3 (532.3)</u>	<u>74.3 (534.3)</u>	
Time (minutes)	<u>11:44.87</u>	<u>10:47.03</u>	<u>10:16.44</u>	

$$Y = \frac{(V_w)(MCF)(BP)(T_m)}{(V_d)(BP + \frac{\Delta H}{13.6})(T_w)}$$

$$Y \text{ Factor } \% \text{ Difference} = \frac{\text{Act} - \text{Exp}}{\text{Exp}} \times 100$$

NOTE: MCF = Meter Correction (Y) Factor for Dry Gas Meter used as a Transfer Standard

Run 1

$$Y = \frac{(6.243)(.9978)(28.13)(528.5)}{(6.264)(28.13 + \frac{0.90}{13.6})(523)} = \frac{92,608.451}{92,372.704} = 1.00255$$

$$\Delta\% = \frac{(1.00255 - 1.01463)}{1.01463} \times 100 = -1.191\%$$

Run 2

$$Y = \frac{(5.698)(.9978)(28.12)(532.3)}{(5.753)(28.12 + \frac{0.90}{13.6})(521.8)} = \frac{85,101.600}{84,521.440} = 1.00675$$

$$\Delta\% = \frac{(1.00675 - 1.01463)}{1.01463} \times 100 = -0.777\%$$

Run 3

$$Y = \frac{(6.448)(.9978)(28.12)(534.3)}{(6.545)(28.12 + \frac{0.90}{13.6})(521.5)} = \frac{96,664.947}{96,205.551} = 1.00478$$

$$\Delta\% = \frac{(1.00478 - 1.01463)}{1.01463} \times 100 = -0.971\%$$

NOTE: The Y Factor % Difference must be < +5.0% to be acceptable

Determination of Interpolated Y Factor for Average Certification Test Series Delta H from Dry Gas Meter Calibration Data:

X = -0.980

0.90 inch H<sub>2</sub>O Delta H = 1.01463 Calculated Calibration Y Factor (from Calibrations)

\_\_\_\_\_ inch H<sub>2</sub>O Delta H = \_\_\_\_\_ Calculated Calibration Y Factor (from Calibrations)

$$\frac{\text{(B)}}{\text{(A)}} - \frac{\text{(A)}}{\text{(A)}} = \frac{\text{X} \times 100}{\text{(A)}} = \text{(E)}$$

$$\frac{\text{(D)}}{\text{(C)}} - \frac{\text{(C)}}{\text{(C)}} = \frac{\text{X}}{\text{(C)}} = \text{(F)}$$

$$\frac{\text{Avg Delta H}}{\text{(A)}} - \frac{\text{(A)}}{\text{(A)}} = \frac{\text{X} \times 100}{\text{(A)}} = \text{(G)}$$

$$\left[ \frac{\text{F}}{\text{G}} \times \frac{\text{X}}{\text{G}} \right] + \frac{\text{C}}{\text{G}} = \text{Interpolated Y Factor For Avg. Test Series Delta H}$$

Volume Metering System Leak Check: \_\_\_\_\_ inch H<sub>2</sub>O in one minute

**APEX INSTRUMENTS REFERENCE METER VERIFICATION  
USING WET-TEST METER #11AE6**

**2-POINT ENGLISH UNITS**

Calibration Meter Information	
Wet Test Meter Model #	AL20
Wet Test Meter Serial #	11AE6
Wet Test Meter Gamma	0.99730

Calibration Conditions	
Date	6-Jan-08
Time	1:30
Barometric Pressure	29.50 in Hg
Calibration Tech	EW
DGM Serial Number	1052202

Factors/Conversions	
Std Temp	528 °R
Std Press	29.92 in Hg
K <sub>i</sub>	17.647 °R/in Hg

Run Time	Measuring Console				Calibration Data				Calibration Meter				Results		
	DGM Input Pressure (P <sub>in</sub> ) in H <sub>2</sub> O	Volume Initial (V <sub>1</sub> )	Volume Final (V <sub>2</sub> )	Volume Sample (V <sub>s</sub> )	Outlet Temp Initial (T <sub>1</sub> )	Outlet Temp Final (T <sub>2</sub> )	Volume Initial (V <sub>1</sub> )	Volume Final (V <sub>2</sub> )	Volume Sample (V <sub>s</sub> )	Outlet Temp Initial (T <sub>1</sub> )	Outlet Temp Final (T <sub>2</sub> )	Calibration Factor Previous (V)	Calibration Factor Current (V)	Flowrate Std & Corr (Q <sub>std&amp;corr</sub> )	Flowrate
6.00 min	-3.5	701.310	707.150	5.840	78.8	80.6	273.560	279.330	5.770	71	71	1.0067	1.0130	0.943	0.943
										Variation		0.6297		must be less than 1.5%	
10.00	-2.2	707.150	712.489	5.339	80.6	82.4	279.330	284.610	5.280	71	71	1.0084	1.0141	0.518	0.518
										Variation		0.5618		must be less than 1.5%	

I certify that the above Dry Gas Meter was calibrated in accordance with USEPA Methods, CFR 40 Part 60, App A, Method 5, Paragraph 7.1.2.2, using the Precision Wet Test Meter # 11AE6, which in turn was calibrated using the American Bell Prover # 3786, certificate # F-107, which is traceable to the National Bureau of Standards (N.I.S.T.).

Signature *[Signature]* Date 1/6/08

**APEX INSTRUMENTS REFERENCE METER CALIBRATION  
USING WET-TEST METER #11AE6  
15-POINT ENGLISH UNITS**

Calibration Meter Information		Calibration Conditions		Factors/Conversions	
Wet Test Meter Model #	AL 20	Date	3-Dec-07	Std Temp	528
Wet Test Meter Serial #	11AE6	Barometric Pressure	29.6	Std Press	29.92
Wet Test Meter Gamma	1.00190	Calibration Technician	EIW	K <sub>1</sub>	17.647
		DSM Serial Number	1052202		

Run Time	Calibration Data										Results	
	Dry Gas Meter					Calibration Meter					Dry Gas Meter	
Elapsed (t)	Meter Pressure (P <sub>1</sub> ) In H <sub>2</sub> O	Volume Initial (V <sub>1</sub> ) cubic feet	Volume Final (V <sub>2</sub> ) cubic feet	Outlet Temp Initial (t <sub>1</sub> ) °F	Outlet Temp Final (t <sub>2</sub> ) °F	Volume Initial (V <sub>1</sub> ) cubic feet	Volume Final (V <sub>2</sub> ) cubic feet	Outlet Temp Initial (t <sub>1</sub> ) °F	Outlet Temp Final (t <sub>2</sub> ) °F	Calibration Factor Value (Y)	Variation (Y <sub>max</sub> -Y <sub>min</sub> )	Flowrate Std & Corr (Q <sub>std,corr</sub> ) cfm
5.00	5.0	495.0040	502.9400	80.6	80.6	511.210	517.980	69.0	69.0	0.9852		1.337
5.00	5.0	509.9290	516.9260	80.6	80.6	517.980	524.790	69.0	69.0	0.9835		1.345
5.00	5.0	509.9290	516.9260	78.8	80.6	524.790	531.610	69.0	69.0	0.9822	0.003	1.347
										0.9837	Averages	1.343
6.00	3.0	516.9260	523.3720	80.6	80.6	531.610	537.940	69.0	69.5	0.9856		1.041
6.00	3.0	523.3720	529.8040	78.8	80.6	537.940	544.250	69.5	69.5	0.9825		1.037
6.00	3.0	529.8040	536.2360	80.6	82.4	544.250	550.550	69.5	70.0	0.9838	0.003	1.035
										0.9840	Averages	1.038
7.00	2.0	536.2360	542.2700	80.6	80.6	550.550	556.490	70.0	70.0	0.9991		0.836
7.00	2.0	542.2700	548.3125	78.8	80.6	556.490	562.440	70.0	70.0	0.9978		0.838
7.00	2.0	548.3125	554.3620	78.8	80.6	562.440	568.390	70.0	70.0	0.9966	0.003	0.838
										0.9978	Averages	0.837
10.00	1.0	554.3620	560.6520	80.6	80.6	568.390	574.600	70.0	70.0	1.0045		0.612
10.00	1.0	560.6520	566.9260	80.6	80.6	574.600	580.800	70.0	70.0	1.0055		0.611
10.00	1.0	566.9260	573.1990	80.6	80.6	580.800	586.990	70.0	70.0	1.0040	0.001	0.610
										1.0047	Averages	0.611
15.00	0.5	475.7525	482.4970	78.8	78.8	491.160	497.840	69.0	69.0	1.0075		0.440
15.00	0.5	482.4970	489.2530	78.8	80.6	497.840	504.530	69.0	69.0	1.0080		0.440
15.00	0.5	489.2530	496.0040	80.6	80.6	504.530	511.210	69.0	69.0	1.0099	0.002	0.440
										1.0088	Averages	0.440
Overall Average Y											<b>0.9978</b>	

Notes: For Calibration Factor Y, the ratio of the reading of the calibration meter to the dry gas meter, the variation between the maximum and minimum values at each flow rate must not exceed 0.030.  
Note: For the Overall Average Calibration Factor, Y, the acceptable range is between 0.95 and 1.05.

I certify that the above Dry Gas Meter was calibrated in accordance with USEPA Methods, CFR 40 Part 60, using the Precision Wet Test Meter # 11AE6, which in turn was calibrated using the American Bell Prover # 3785, certificate # F-107, which is traceable to the National Bureau of Standards (N.I.S.T.).

Signature *[Handwritten Signature]*

Date 12/3/07



## VANEOMETER CALIBRATION

Myren Consulting used a Dwyer Model 3480 Vaneometer to measure test chamber air velocity. The manufacturer's specifications for accuracy are  $\pm 5.0\%$  from 0 to 100 fpm and  $\pm 10\%$  from 100 to the top of the scale. Myren Consulting insures that the instrument is level and clean prior taking each reading. According to EPA personnel (Westlin, RTP) no further calibration is necessary.

## DRAFT GUAGE CALIBRATION

Myren Consulting used a Dwyer Model 115 AV, a  $-0.05 - 0.0 - 0.25$ " inclined red oil manometer (readability resolution  $\pm 0.001$ " H<sub>2</sub>O) to measure the static pressure in the stack. Once leveled and zeroed as per the manufacturer's written operating instructions, the Dwyer manometer is a primary standard and needs no further calibration.

The manometer is leveled and zeroed at the start of each test, checked as necessary during a run to verify that the settings have not changed and again at the end of each test run. The results of these checks are recorded on Woodstove Data Sheet #16 in each individual test.

## BAROMETER CALIBRATION

Myren Consulting used a Princo Model 453 SN W14275 Mercury barometer and a Weems and Plath aneroid barometer to measure the barometric pressure (BP). The Weems and Plath barometer was calibrated daily by comparing it to the Princo and adjusting it as necessary. The Princo when calibrated following the manufacturer's instructions is a primary standard and needs no further calibration.

## MOISTURE METER CALIBRATION

Myren Consulting used a Delmhorst RC-1E SN 1509 which was calibrated daily using the "Check" feature. Then the operation of the moisture meter was checked in the normal operating range used during testing 11-25% with a Delmhorst Moisture Content Standard Model MCS-1 at 12.0 and 22.0%. The results of these checks are recorded on Data Sheet #10.

The readings obtained with the moisture meter are then corrected as per the manufacturer's written instructions for temperature and species. If Delmhorst insulated pins are used one additional correction is required. See the following page for the correction table used to correct the readings if insulated pins were used.

7 - 7.3  
7.5 - 7.85

8 - 8.4  
8.5 - 8.95

9 - 9.50  
9.5 - 10.05

10.0 - 10.6  
10.5 - 11.2  
11.0 - 11.7  
11.5 - 12.3  
12.0 - 12.8  
12.5 - 13.3  
13.0 - 13.9  
13.5 - 14.4  
14.0 - 14.9  
14.5 - 15.4  
15.0 - 15.9  
15.5 - 16.5  
16.0 - 17.0  
16.5 - 17.5  
17.0 - 18.1  
17.5 - 18.6

24.0 - 26.0  
24.5 - 26.6  
25.0 - 27.2  
25.5 - 27.8  
26.0 - 28.4  
26.5 - 29.0

27.0 - 29.6  
27.5 - 30.2  
28 - 30.8  
28.5 - 31.4  
29.0 - 32.0  
29.5 - 32.6  
30.0 - 33.2  
30.5 - 33.8  
31.0 - 34.4  
31.5 - 35.0

26-ED ELECTRODE

OPERATING INSTRUCTIONS

The 26-E and 18-E Electrodes, fitted with Insulated pins and used with any Delmhorst Moisture Detectors for Wood, are available in detecting moisture gradient in lumber or in testing dry stock that is wet on the surface.

These Electrodes, as long as they have good insulation on their shanks, measure moisture content at the tip of the pins only, that is in a layer about 3/16" thick.

Shell and core, moisture content is easily measured by driving the pins to the proper depths.

When using the Electrode, place the pins on the wood so that the current will flow parallel to the grain and drive the pins into the wood by means of the sliding hammer. Note the pins' penetration, and read the meter.

The Moisture Meter is calibrated for use with a 4-pin Electrode. When using a 2-pin Electrode, a small correction should be applied, as noted below, where line "A" shows meter readings, and line "B" the correct readings for the 2-pin Electrode.

A=	7	8	10	12	14	16	18	20	22
B=	7.3	8.4	10.6	12.8	14.9	17.0	19.2	21.4	23.7

When the insulation on the contact pins wears off, the above correction should be disregarded, and the electrode should not be used on lumber which may have a wet surface. Always use the L-319 insulating washer especially if surface moisture on the wood is expected. If washers are not available, do not allow the retainers to touch the surface of the wood.

LEGAL RANGE

18.0 - 19.2  
18.5 - 19.8  
19.0 - 20.3  
19.5 - 20.9  
20.0 - 21.4  
20.5 - 22.0  
21.0 - 22.6  
21.5 - 23.1  
22.0 - 23.7  
22.5 - 24.3  
23.0 - 24.9  
23.5 - 25.4



WOODSTOVE DATA SHEET #26-A  
 CEM GAS TRAIN RESPONSE TIME  
 PRE-CERTIFICATION TEST SERIES CHECK

Date	Technicians	CO2 Conc.(V)	CO2 Conc.(V)	CO2 Conc.(V)	CO Conc.(V)	CO Conc.(V)	CO Conc.(V)	O2 Conc.(V)	O2 Conc.(V)	O2 Conc.(V)	O2 Conc.(V)	Conc.(V)	Conc.(V)
11/9/08	ATM												
Elapsed Time		CO2 Conc.(V)	CO2 Conc.(V)	CO2 Conc.(V)	CO Conc.(V)	CO Conc.(V)	CO Conc.(V)	O2 Conc.(V)	O2 Conc.(V)	O2 Conc.(V)	O2 Conc.(V)	Conc.(V)	Conc.(V)
0 Seconds		.349	.347	.346	.163	.166	.169						
15		.349	.346	.345	.162	.165	.167						
30		.064	.065	.063	.054	.057	.060						
45		.033	.034	.032	.042	.048	.046						
60		.016	.015	.014	.014	.015	.017						
75		.009	.009	.008	.009	.010	.010						
90		.004	.003	.003	.003	.003	.003						
105		.002	.002	.002	.002	.003	.002						
120		.001	.002	.001	.002	.002	.002						
135		.001	.001	.001	.001	.002	.001						
150		.001	.001	.001	.001	.001	.001						
165		.001	.001	.001	.001	.001	.001						
180		.001	.001	.001	.001	.001	.001						
Initial Response Time (Seconds)	~25	~25Sec	N 25	N 30	N 30	N 30	N 30	N 30	N 30	N 30	N 30	N 30	N 30
95% Response Time (Seconds)	<60	>45	>45	>45	>45	>45	>45	>45	>45	>45	>45	>45	>45
Analyzer Flow Rate	1.5CFM	1.5CFM	<60	<60	<60	<60	<60	<60	<60	<60	<60	<60	<60

Comments

Prekuma Ashwood

QA WS 1/85

CO<sub>2</sub> ANALYZER  
 MULTIFPOINT CALIBRATION REPORT FORM

Site: Colville, WA Date: 2/16/09  
 Analyzer: Make: HORIBA Model: PIR 2000 SN: 607204  
 Calibration by: A.T. Myren  
 Cal Gas Flow: 1.5 SCFH Measured by: Rotameter:  Mass Flowmeter:   
 BP: 29.17" Hg Instrument ID: Princo  
 Temp: 69 °F Instrument ID: Omega Dig  
 Analyzer last calibrated: 12/19/08 By: A.T. Myren

Cylinders:

1. # TC3AAM154 Concentration: 00.0 % CO<sub>2</sub> Cyl. Press.: 1550 psi.  
 Certified by: Oxarc Date: 11/12/07
2. # AS 90457 Concentration: 12.5 % CO<sub>2</sub> Cyl. Press.: 1480 psi.  
 Certified by: Matheson Tri Gas Date: 2/2/2009
3. # 250-1175 Concentration: 21.0 % CO<sub>2</sub> Cyl. Press.: 1490 psi.  
 Certified by: Oxarc Date: 8/22/97
4. # 250-1088 Concentration: 6.01 % CO<sub>2</sub> Cyl. Press.: 1100 psi.  
 Certified by: Oxarc Date: 1/31/01

Analyzer: Calibrated Range: 0-25.0 % Output: 0-1.0 v.  
 Flow: 1.5 SCFH Measured by: Rotameter:  Mass Flowmeter:

Calibration Results

Point #	Cyl. #	% CO <sub>2</sub>	Expected		Actual		Adj.		% Dif.	Potentiometer	
			Meter	DVM	Meter	DVM	Meter	DVM		Unadj.	Adj.
1	1	00.0	00.0	.000	00.0	.000	—	—	+0.22	6.06	—
2	2	12.5	50.0	.500	50.5	.505	50.0	.500	-0.72	4.72	4.34
3	3	21.0	84.0	.840	85.0	.850	—	—	+0.28	—	—
4	4	6.01	24.0	.240	24.0	.240	—	—	-0.41	—	—
5	1	00.0	00.0	.000	00.0	.000	—	—	+0.22	—	—

Comments:  $r = .9999688$   $b = -0.0021819$   $0.500 = 12.410466\%$   
 $m = .0404689$

0.545  
 21.071  
 5.985

Linear Regression Results:

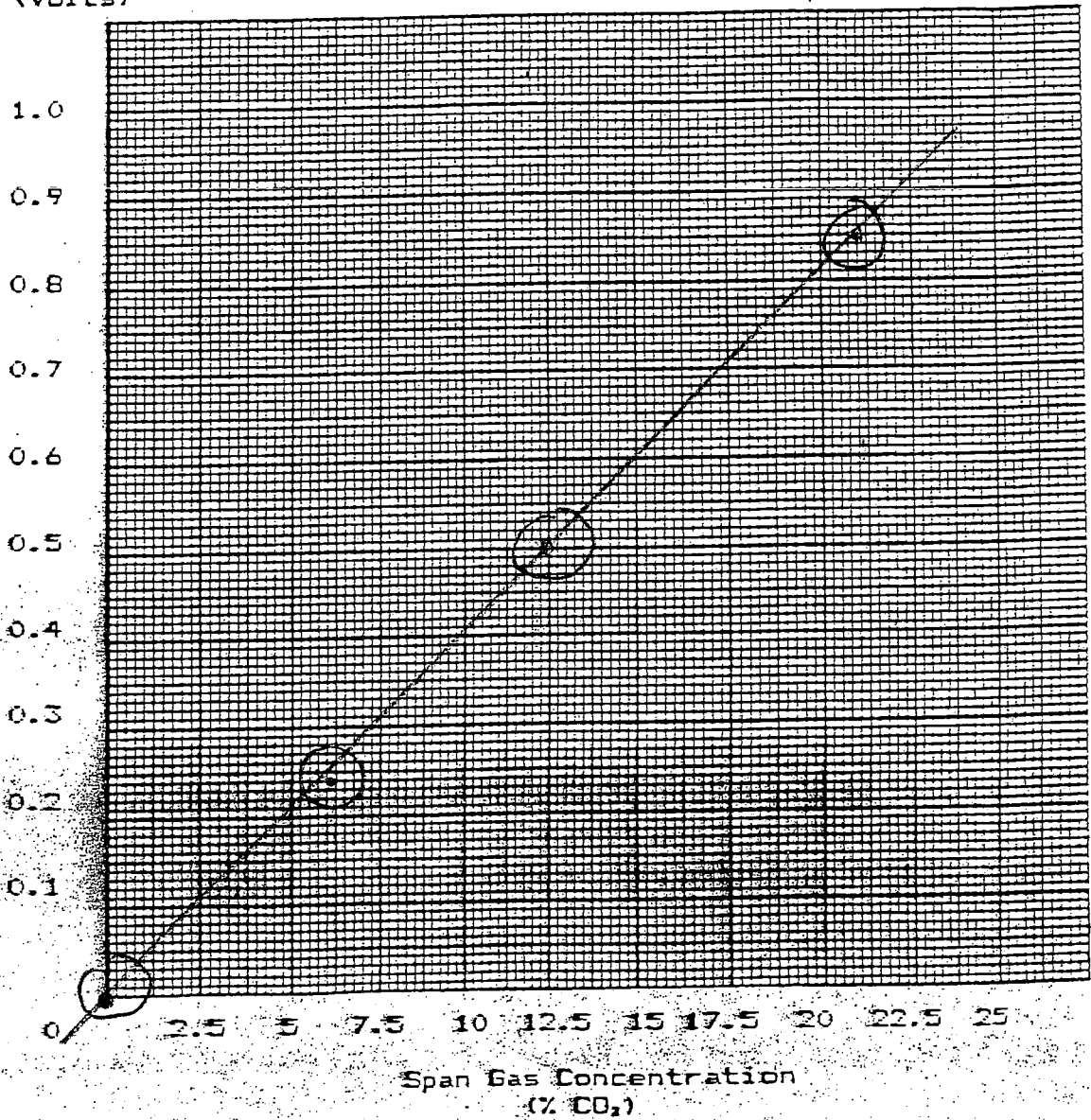
$$Y = MX + B$$

$$\text{Slope (M)} = \underline{0.0404639}$$

$$\text{Y Intercept (B)} = \underline{-0.0021819}$$

$$\text{Correlation Coefficient (r)} = \underline{0.9999688}$$

Analyzer  
Output  
(volts)



Comments

Pre kuma Ashwood

GA WS 1/85

CO ANALYZER  
MULTIPOINT CALIBRATION REPORT FORM

Site: Colville, WA Date: 2/16/09  
 Analyzer: Make: HORIBA Model: MEXA 311 GE SN: GE-30075  
 Calibration by: A.T. Myren  
 Cal Gas Flow: 1.5 SCFH Measured by: Rotameter:  Mass Flowmeter:   
 BP: 28.12 "Hg Instrument ID: Princo  
 Temp: 69°F Instrument ID: Omega Digi  
 Analyzer last calibrated: 12/19/08 By: A.T. Myren

Cylinders:

1. # TC3AAMISY Concentration: 00.0 % CO Cyl. Press.: 1550 psi.  
 Certified by: Oxarc Date: 11/12/07
2. # AS90457 Concentration: 2.00 % CO Cyl. Press.: 1480 psi.  
 Certified by: Matheson Tri Gas Date: 2/2/2009
3. # 250-1175 Concentration: 4.03 % CO Cyl. Press.: 1490 psi.  
 Certified by: Oxarc Date: 8/22/97
4. # 250-1088 Concentration: 1.26 % CO Cyl. Press.: 1100 psi.  
 Certified by: Oxarc Date: 1/31/01

Analyzer: Calibrated Range: (0-5.0%) 0-10.0 % Output: 0-1.0 v.  
 Flow: 1.5 SCFH Measured by: Rotameter:  Mass Flowmeter:

Calibration Results

Point #	Cyl. #	% CO	Expected		Actual		Adi.		% Dif.	Potentiometer	
			Meter	DVM	Meter	DVM	Meter	DVM		Unadi.	Adi.
1	1	00.0	0.00	.000	0.00	.000	—	—	-0.04	—	—
2	2	2.00	2.00	.200	2.00	.200	—	—	+0.30	—	—
3	3	4.03	4.03	.403	4.02	.401	—	—	-0.09	—	—
4	4	1.26	1.26	.126	1.26	.126	—	—	+0.17	—	—
5	1	00.0	00.0	.000	00.0	.000	—	—	-0.04	—	—

Comments: .200 = 2.0059466 %

7.0044  
2.0059  
4.0264  
1.2621

Linear Regression Results:

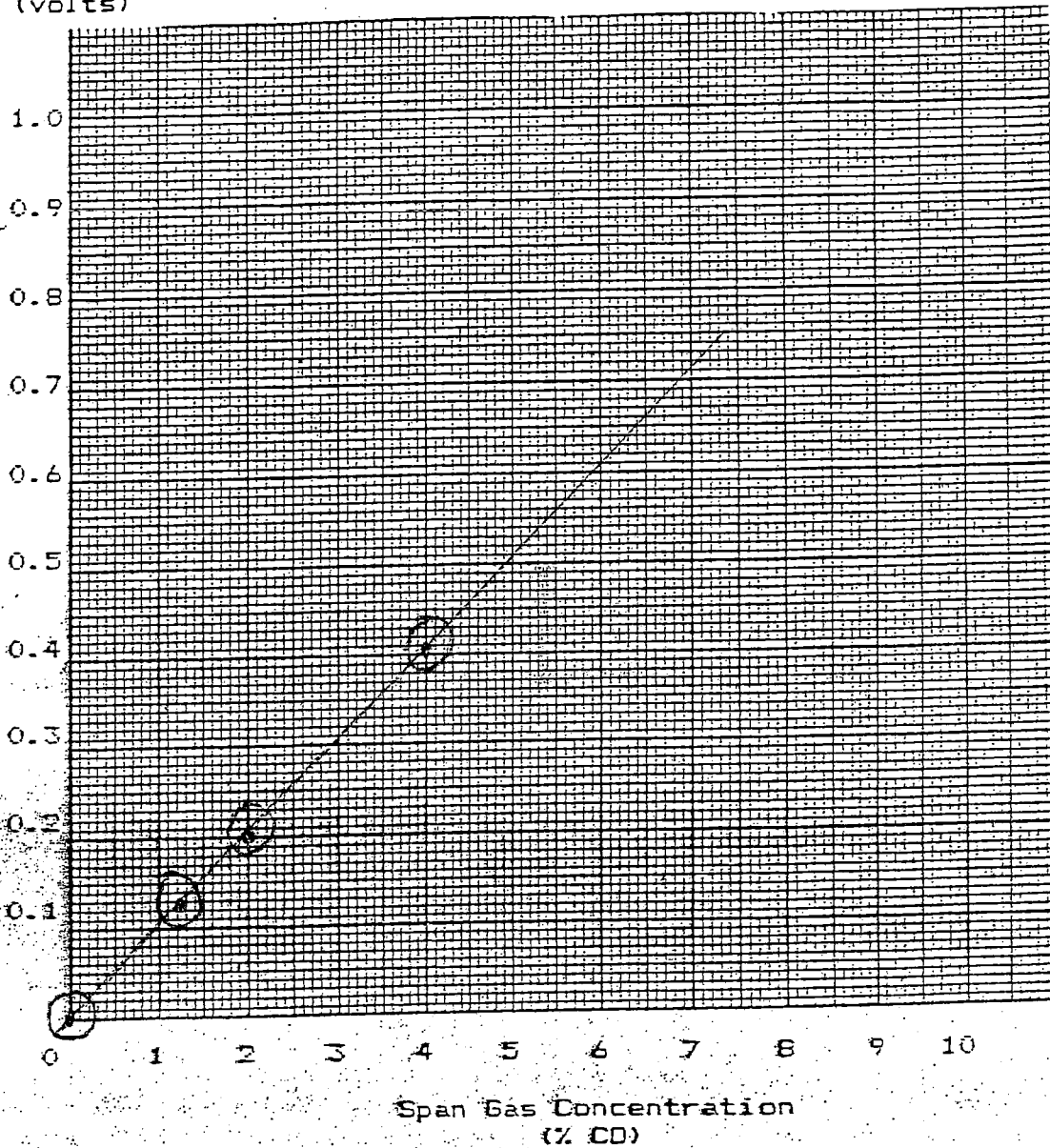
$$Y = MX + B$$

$$\text{Slope (M)} = \underline{0.0994832}$$

$$\text{Y Intercept (B)} = \underline{0.0004419}$$

$$\text{Correlation Coefficient (r)} = \underline{0.999958}$$

Analyzer  
Output  
(volts)



Comments



# MATHESON TRI-GAS

ask...The Gas Professionals™

Matheson Tri-Gas Inc.

6775 Central Avenue  
Newark, CA, 94560

Phone: 510-793-2559

Fax: 510-790-6241

*Certified Mixture Grade*

TO: Oxarc Inc  
Attn: Ted Storms  
328 West 1st  
Colville, WA 99114

TO AVOID BACKFILL, CYLINDER PRESSURE MUST BE  
GREATER THAN PROCESS PRESSURE

PHONE: 509-535-7794

FAX:

SALES ORDER NUMBER: 476173

P.O. NUMBER: CV12337

LOT NUMBER: 103-96-00348

PRODUCT: 4 COMPONENT MIXTURE

CYLINDER NUMBER: AS 90457

FILL DATE: Feb 2, 2009

SIZE: 1A

CGA/DISS OUTLET: CGA 590

CONTENT: 168.1 cu. ft.

PRESSURE: 1600 psig

COMPONENT	REQUESTED CONCENTRATION	BLEND TOLERANCE (+/-)	CERTIFIED CONCENTRATION	CERTIFICATION ACCURACY
Carbon Monoxide, TECHNICAL	2.00 %	10 %	2.00 %	+/- 2%
Carbon Dioxide, BONE DRY	12.5 %	5 %	12.5 %	+/- 2%
Oxygen, UHP	12.5 %	5 %	12.53 %	+/- 2%
Nitrogen, UHP	BAL		BAL	

TRACEABLE TO REFERENCE STANDARD SOURCE/NUMBER:

TRACEABLE TO NIST TRACEABLE WEIGHT CERTIFICATE: 822/272801-06 822/274081-06

SPECIAL INFORMATION / ADDITIONAL COMMENTS

The product listed above and furnished under the referenced purchase order has been tested and found to contain the component concentration listed above. All values in mole/mole basis gas phase unless otherwise indicated. Matheson Tri-Gas Inc. warrants that the above product(s) conform at the time of shipment to the above description. Matheson Tri-Gas Inc. liability does not exceed the value of the product purchased.

Zoran Topalovic

ANALYST

HL

SIGNATURE

Feb 9, 2009

DATE SIGNED



WELDING PRODUCTS  
 INDUSTRIAL SUPPLIES  
 INDUSTRIAL GASES  
 MEDICAL GASES



SPECIALTY GASES  
 BEVERAGE SYSTEMS  
 SAFETY PRODUCTS  
 FIRE EQUIPMENT

WWW.OXARC.COM

**MAIN OFFICE**

SPOKANE, WA 99220  
 4003 E. BROADWAY  
 P.O. BOX 2605  
 (509) 535-7794  
 FAX (509) 535-0368

BOISE, ID 83709  
 7615 W. LEMHI ST.  
 (208) 376-0377  
 FAX (208) 376-1133

EUR D'ALENE, ID 83814  
 3530 RAMSEY RD.  
 (208) 765-3311  
 FAX (208) 667-5974

COLVILLE, WA 99114  
 328 W. 1ST.  
 (509) 684-3776  
 FAX (509) 684-6742

LENSBURG, WA 98928  
 704 N. WENAS  
 (509) 925-1518  
 FAX (509) 925-1136

HERMISTON, OR 97838  
 HERMISTON-  
 McNARY HWY  
 (503) 567-7377  
 (503) 567-2265

LENNEWICK, WA 98338  
 800 W. COLUMBIA DR.  
 (509) 582-4202  
 FAX (509) 586-9859

LEWISTON, ID 83501  
 513 3RD. AVE., NORTH  
 (208) 743-8571  
 FAX (208) 746-8374

POSES LAKE, WA 98837  
 1401 WHEELER ROAD  
 (509) 785-9247  
 FAX (509) 786-9858

OKANOGAN, WA 98840  
 2256 ELMWAY  
 (509) 826-3205  
 FAX (509) 826-3905

PASCO, WA 99302  
 718 SOUTH OREGON  
 (509) 547-2494  
 FAX (509) 547-3103

TWIN FALLS, ID 83303  
 29 COMMERCIAL AVE.  
 (208) 734-9711  
 FAX (208) 734-7923

HEMLOCK, WA 98801  
 WHEMME GARDENS RD.  
 (509) 662-8417  
 (509) 662-1229

YAKIMA, WA 98903  
 1004 EAST MEAD  
 (509) 248-0827  
 FAX (509) 452-8704

**Primary Standard Certificate of Analysis**

Method of Analysis Micro GC / Gravimetric

Customer: Myren Consulting Reference # PM7234-2

P.O.# Cylinder # 250-1175

**Results of Investigation**

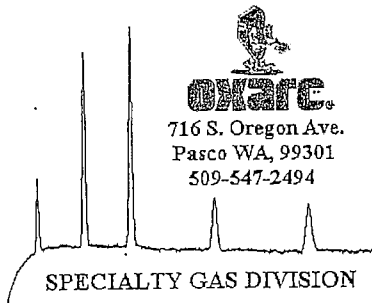
<u>Component</u>	<u>Requested</u>	<u>Concentration</u>
Air	N/A	N/A
Argon	N/A	N/A
Carbon Dioxide	21.0%	21.0%
Carbon Monoxide	4.00%	4.03%
Helium	N/A	N/A
Hydrogen	N/A	N/A
Methane	N/A	N/A
Nitrogen	Balance	Balance
Oxygen	21.0%	21.0%

Hazard Class UN 1956  
 DOT Shipping Name Compressed Gas NOS  
 Shipping Volume (scf approximate) 160 scf @ ntp  
 Cylinder Pressure 1500 psig  
 CGA Valve Connection 350

Oxarc Primary Standard mixtures are prepared with gravimetric techniques using weights traceable to NIST. Mixture blended to +/- 1% relative to minor component and certified to +/- 1% analytical accuracy.

Authorized Signature Travis Auger Date 8/25/97  
 Travis Auger

Comments:



**Primary Standard Certificate of Analysis**

Cylinder filled in Pasco WA

Method of Analysis Micro GC / Gravimetric

Customer: Myren Consulting Reference # 2010306

P.O.# Cylinder # 250-1088

**Results of Investigation**

<u>Component</u>	<u>Requested</u>	<u>Concentration</u>
Air-----	N/A -----	N/A -----
Argon-----	N/A -----	N/A -----
Carbon Dioxide-----	6.00% -----	6.01% -----
Carbon Monoxide-----	1.25% -----	1.25% -----
Helium-----	N/A -----	N/A -----
Hydrogen -----	N/A -----	N/A -----
Methane-----	N/A -----	N/A -----
Nitrogen-----	Balance -----	Balance -----
Oxygen -----	6.00% -----	6.02% -----

Hazard Class UN 1956  
 DOT Shipping Name Compressed Gas NOS  
 Shipping Volume (scf approximate) 182 scf @ NTP  
 Cylinder Pressure 1691 psig  
 CGA Valve Connection 350

Oxarc Primary Standard mixtures are prepared with gravimetric techniques using weights traceable to NIST. Mixture blended to +/- 2% relative to minor component and certified to +/- 1% analytical accuracy.

Authorized Signature *Travis Auger* Date 11/31/01  
 Travis Auger

Comments:

Bottle 4 Received #170104

1700

Blank done 12/18/07

# Certificate of Analysis

## ANALYTICAL CONTROL LABORATORY ANALYSIS ACETONE - OPTIMA

Catalog No. A929

April 29, 2004

Lot No. 041648

This is to certify that this lot was tested and found to comply with the specifications for this product. The following are the actual analytical results obtained:

### TESTS

Assay  
 Color  
 Description  
 Identification  
 Fluorescence Background (as Quinine Sulfate)  
 Pesticide Residue Analysis  
     (As Heptachlor Epoxide)  
 Substances Reducing Permanganate  
 Solubility in Water  
 Aldehyde (as HCHO)  
 Density (g/ml) @ 25 Degrees C  
 Methanol (CH<sub>3</sub>OH)  
 Isopropyl Alcohol ((CH<sub>3</sub>)<sub>2</sub>CHOH)  
 Optical Absorbance    At 400 - 350 nm  
                             At 350 nm  
                             At 340 nm  
                             At 330 nm  
 Refractive Index at 25°C  
 Residue after Evaporation  
 Titratable Acid  
 Titratable Base  
 Water (H<sub>2</sub>O)

### ACTUAL ANALYSIS

99.5%  
 5 APHA  
 Clear, Colorless Liquid  
 Pass Test  
 Not More Than 1 ppb  
 Not More Than 10 ng/L  
  
 Pass Test  
 Pass Test  
 0.0005%  
 0.7854  
 0.03%  
 0.01%  
 0.002  
 0.003  
 0.05  
 0.65  
 1.3556  
 0.6 ppm  
 0.0002 Meq/g  
 <0.0001 Meq/g  
 0.5%

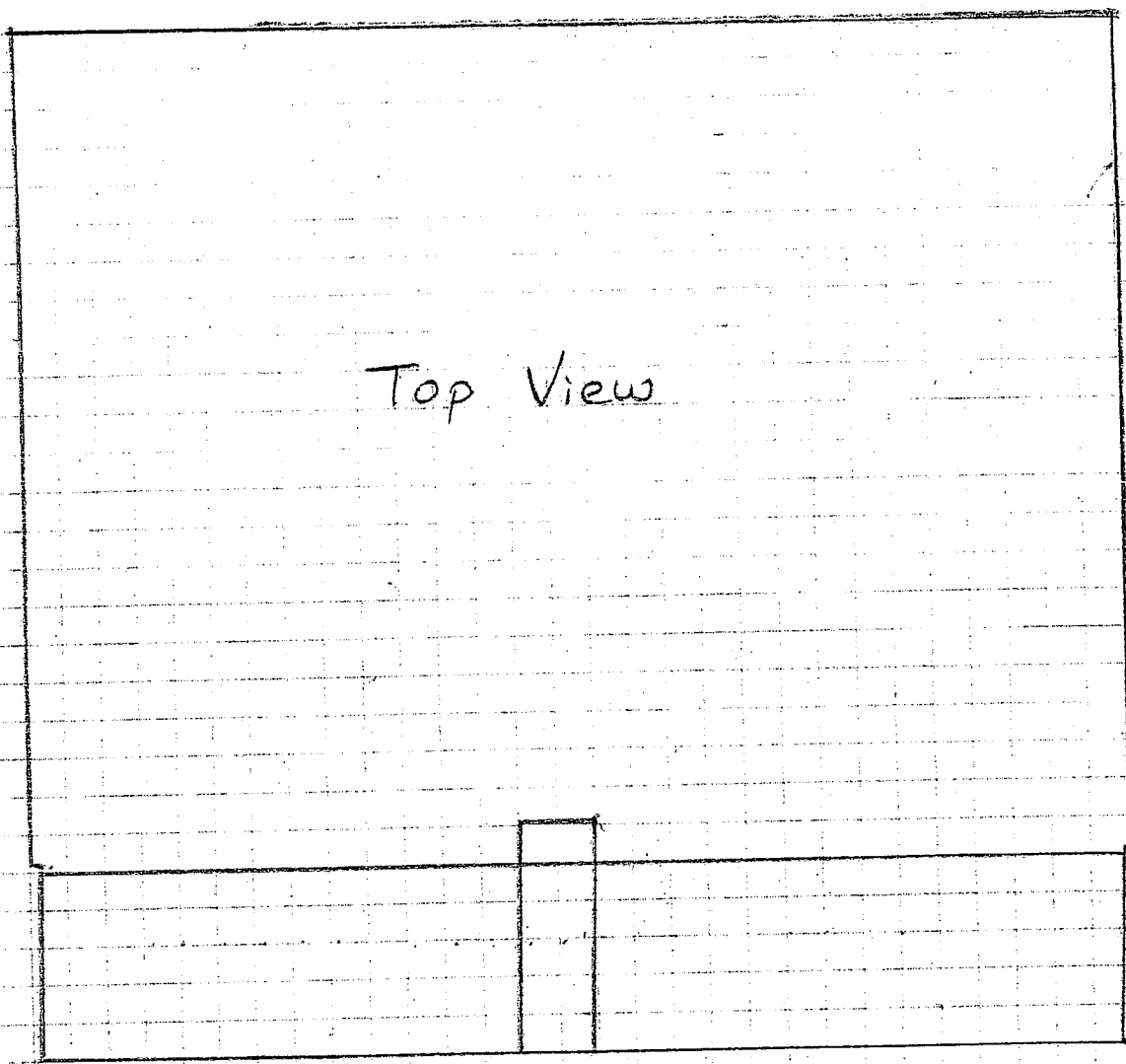
*Edgar E. Hess*

Approved By: \_\_\_\_\_

Edgar E. Hess  
Q.C. Laboratory Manager



Chemical Division  
1 Reagent Lane  
Fair Lawn, N.J. 07410  
201-796-7100



Top View

- 18.75"

- 3.4375"

- 2.750"

- 0.0"

2.0"

19.625"

19.75"

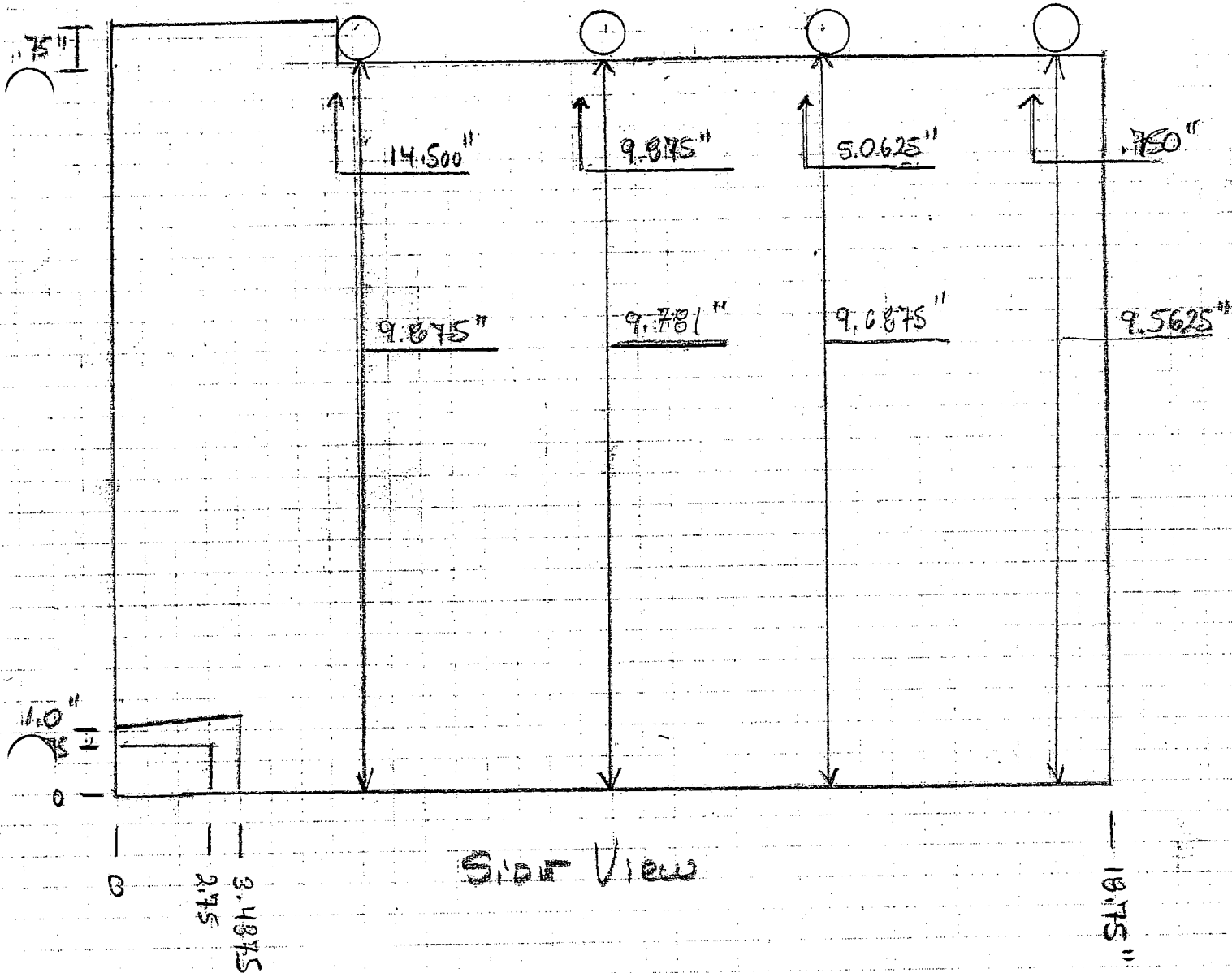
Kumar Ashward

Not to Scale

3/5/09

A.T. Myren

Page 1 of 4



KUMA Ashwood  
 Not to Scale  
 3/5/09  
 A.J. Myren  
 Page 2 of 4

# KUMA ASHWOOD - USEABLE FIREBOX VOLUME CALCULATIONS

$$\begin{aligned}
 A: & 19.750'' \times .750'' \times 9.5625'' = 141.645 \text{ in}^3 \\
 B: & 19.750'' \times \frac{9.5625 + 9.875}{2} \times (18.75 - (4.25 + 1.75)) = 2639.248 \\
 C: & 19.75'' \times 9.875 \times (4.25 - 2.75) = 292.547 \\
 D: & 19.625'' \times 9.875 \times 2.75 = 532.941 \\
 E: & 19.625'' \times 4.25 \times .75 = 62.555 \\
 & \text{---} \\
 & 3668.936 \text{ in}^3
 \end{aligned}$$

Less:

Btm Duct

$$2.75 \times 0.75 \times 19.625'' = 40.477 \text{ in}^3$$

LPAO

$$.75 \times .75 \times 2 = 1.125$$

$$\frac{1 + 15}{2} \times 2 \times 3.4375 = \frac{8.594}{50.196 \text{ in}^3}$$

$$3668.936 \text{ in}^3 - 50.196 \text{ in}^3 = 3618.740 \text{ in}^3$$

$$3618.740 \text{ in}^3 \div 1728 \text{ in}^3/\text{ft}^3 = \underline{2.094 \text{ ft}^3} \text{ USEABLE FIREBOX Vol.}$$

Fuel Load Weight Calculations:

$$2.094 \text{ ft}^3 \times 7 \text{ lbs}/\text{ft}^3 = 14.659 \text{ lbs} - \text{Ideal Fuel Load Weight}$$

$$\begin{aligned}
 14.659 \pm (0.10 \times 14.659) &= 16.125 = 16.1 \text{ lbs.} \\
 &= 13.193 = 13.2 \text{ lbs.}
 \end{aligned}
 \left. \begin{array}{l} \\ \\ \end{array} \right\} \text{Fuel Load Weight Range.}$$

Fuel Piece Length (Maximum)

$$19.750'' \times 0.8333 = 16.458'' = 16.4375'' (16 \frac{7}{16}'')$$

Page 3 of 4

A.J. Myren

## STOVE QC

The Kuma Ashwood noncatalytic wood stove is a medium sized stove with a useable firebox volume of 2.1 cubic feet. It has several distinguishing features. They are as follows:

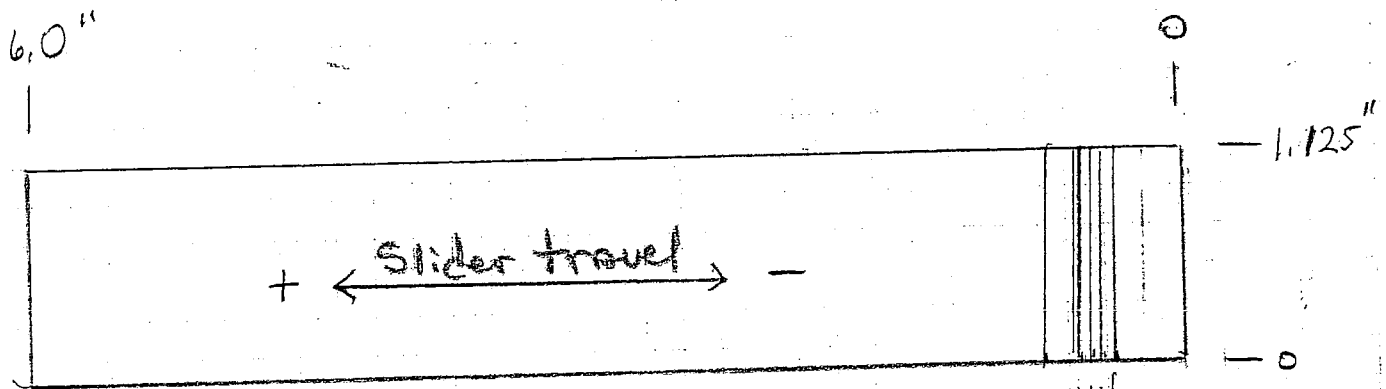
1. The unit is specifically designed with a 2.75" combustion air inlet that can be hooked up to a duct delivering outside air to the unit. There are 2 inlet locations, one on the bottom of the unit that will be used when the unit is installed as a freestanding unit on legs or a pedestal and one on the back of the unit that will be used when the unit is installed as a fireplace insert. The cover plate for the inlet hole not being used is moved from one location to the other and attaches with 2 screws.
2. The unit was tested with an ash pan.
3. The unit is designed so that it can be installed as either a freestanding unit or as a fireplace insert.

The critical dimensions in this stove are as follows:

1. Vertical Throat Dimension: 2.375"
2. Horizontal Throat Dimension: 1.25"  
Note: The vertical and horizontal throat dimensions are measured at the front edge of the baffle.
3. Air Wash Gap: 0.3125"
4. Minimum Primary Air Setting: 0.3655". See drawing on page 4 of 4 in this Section.
5. Lower Primary Air Orifice - Inlet Orifice: 1-0.4375" hole
6. Lower Primary Air Orifice - Outlet Orifices: 1-0.25" and 2-0.1875" holes
7. Secondary Air Tubes  
Front: 40-5/32" holes on 1/2" centers  
Middle Front: 52-3/32" holes on 3/8" centers  
Middle Rear: 52-3/32" holes on 3/8" centers  
Rear: 20-3/32" holes on 1" centers
8. Combustion Air Inlet Orifice (Outside Air Hookup): 2.75" diameter hole.
9. Secondary Air Inlet Orifice: 1.75" X 0.75"
10. (Adjustable) Primary Air Inlet Orifice: 1.125" X 6", of which 0.3655" is always open.

Kuma Ashwood

# Primary Air Inlet Orifice Settings



Run 1 Wide Open

Run 2 M.H.  
0.728" open

Run 4 Low  
0.3655" open

Run 5 M.Low  
0.428" open

Run 7 M.Low  
0.467" open

Run 6 M.Low  
0.5235" open

Run 3 M.Low  
FCT .553" open

The primary air adjustable inlet orifice is 6.0" x 1.125". To increase the amount of air pull the slide to the left, to decrease the amount of push the slider to the right. NOTE: The slider rod exits the unit on the L side of the stove.

Kuma Ashwood

N to Scale

4/9/09 A.T. Myren

P. 4 of 4

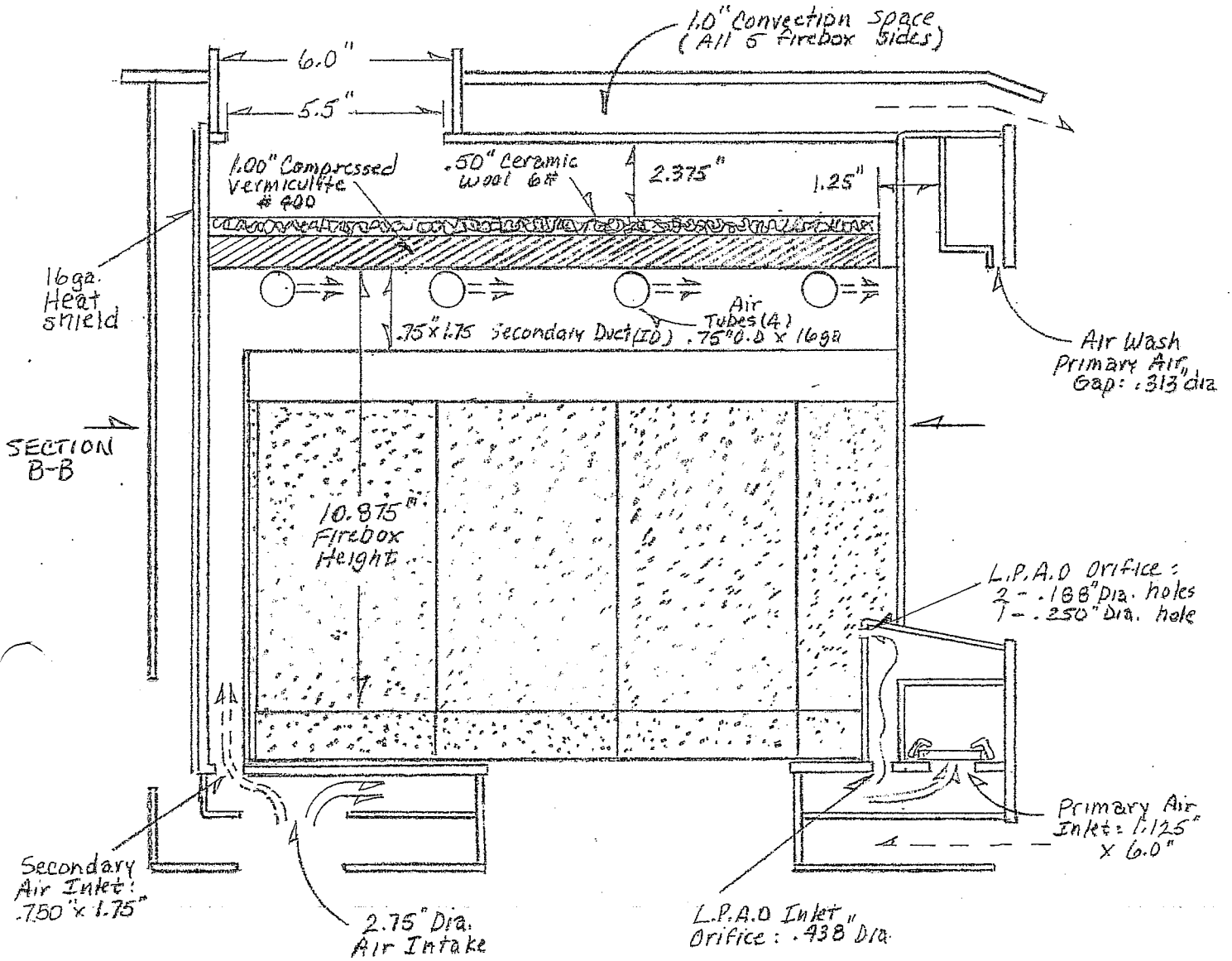


# Ashwood Part Specifications

Part #	Description	Dimensions (inches)	Quantity	Composition
1	Firebox assembly	18.75x20x16.25	1	3/16" Low carbon steel
2	Firebox top	18.5x22.5	1	1/4" Low carbon steel
3	Flue collar	2.0 height 6.0 diameter	1	3/16" Low carbon steel
4	Primary draft channel (cross sectional area)	Sides-1.25x2.5	2	10ga. Low carbon steel
		Bottom- 2.0x2.5	1	10ga. Low carbon steel
		Top - 1.5x3.0	1	10ga. Low carbon steel
5	Primary draft control	1.5x6.5	1	1/4" Low carbon steel
6	Secondary draft ducts	Sides 2.0x16.25	2	10ga. Low carbon steel
		Rear- 2.0x20.50	1	10ga. Low carbon steel
		Riser- 2.0x10.50	1	10ga. Low carbon steel
7	Convection shell	22.0x25.0x19.5	1	12ga. Low carbon steel
8	Heat Shield	16.0x22.5	1	16ga. Low carbon steel
9	L.P.A.O. Tower	2.0x3.5x3.5	1	12ga. Low carbon steel
10	Primary fee duct	1.0x12.0x20.0	1	12ga. Low carbon steel
11	Secondary burn tubes	21.0x.75 diameter	4	16ga. Low carbon steel
12	Gaskets	Door seal- 57.6x.625 diameter	1	Woven fiberglass
		Glass seal- 50.4x.750	1	96.5% Fibrous glass 3.5% surface sizing
13	Firebrick	4.5x9.0	10	81% Fireclay 19% Silica alumina
		2.5x9.0	2	
		4.5x7.5	6	
		2.5x7.5	2	
		4.5x5.75	1	
		1.25x4.5	1	
14	Baffle	1.0x16.75x20.5	1	#400 compressed vermiculite
15	Baffle wool blanket	.50x16.75x22.50	1	Ceramic wool fiber 6#/sq.ft. density
16	Blower motor	20.0x3.0 diameter	1	EBM Pabst C-Frame motor dual tangential variable speed controlled
17	Door	14.0x19.0	1	Cast Iron
18	Glass	10.75x15.50	1	5mm Neo-Ceramic
19	Ash Drop Plenum	4.0x8.0x2.25	1	.25" rectangular steel tubing

Note: - all dimensions given are O.D. For actual area regarding air flow etc. see drawings.

- Components listed above are actual stove body parts that involve combustion and operation of the unit. List does not include pedestal, legs etc.



- Primary Air
- Secondary Air
- L.P.A.O. Air
- Convection Air

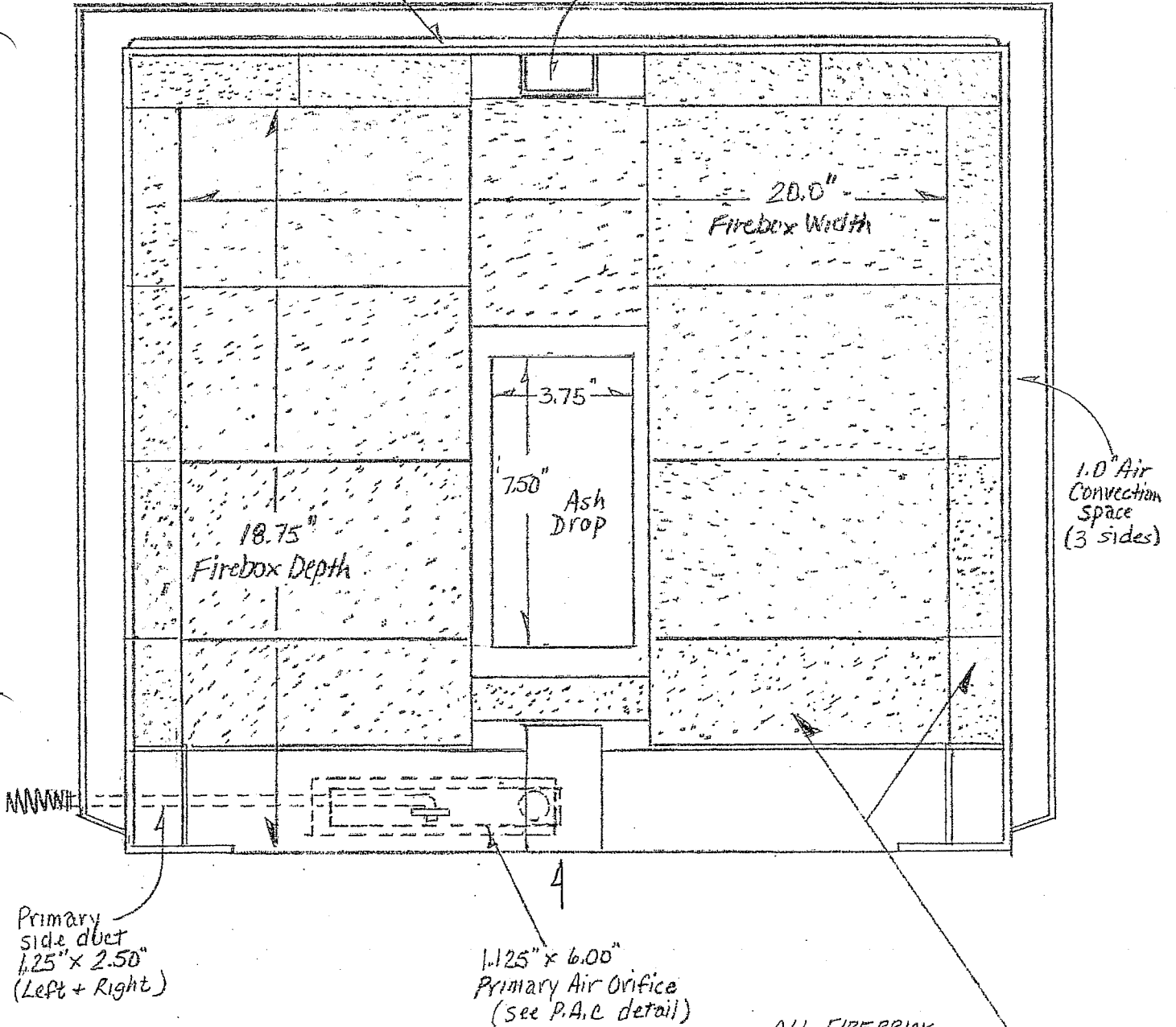
NOTE: ALL DRAWINGS ARE STOVE BODY ONLY AND DO NOT INCLUDE LEGS OR PEDESTAL.

TITLE: KUMA MODEL: ASHWOOD	DR # 1	DR BY M.F.
VIEW CROSS-SECTION A-A	DATE 3/09	SCALE 1/4" = 1"

SECTION A-A

.063" Heat shield  
 .250" Air space

Secondary Air Orifice Riser  
 I.D. = .750" x 1.75"



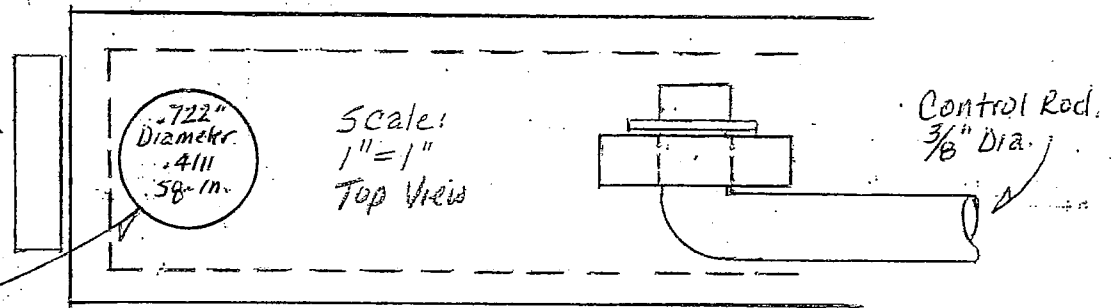
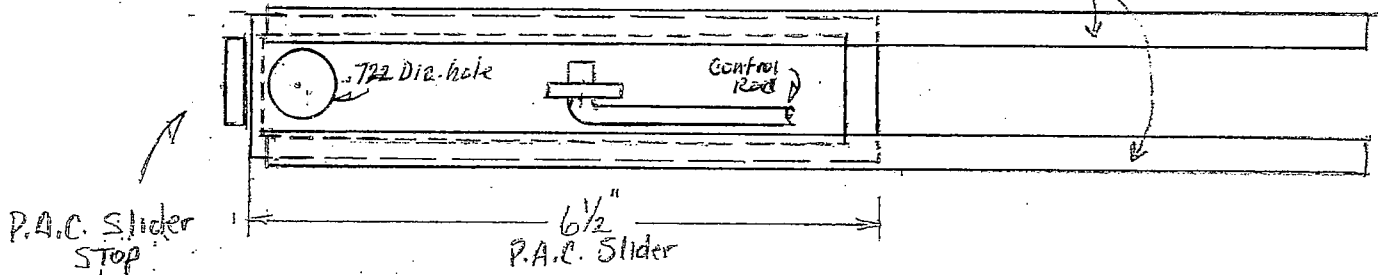
ALL FIREBRICK  
 SHOWN TO SCALE :  
 9.5 - BOTTOM BRICKS  
 4 - LEFT SIDE  
 4 - RIGHT SIDE  
 4 - REAR WALL  
 COMPOSITION: LOW-DUTY  
 FIREBRICK MFG. BY MUTUAL  
 MATERIALS INC.  
 81.0 % FIRECLAY  
 19.0 % ALUMINA SILICA

TITLE: KUMA MODEL: ASHWOOD	DR # 2	DR. BY M.F.
VIEW: CROSS-SECTION B-B	DATE 3/09	SCALE 1/4" = 1"

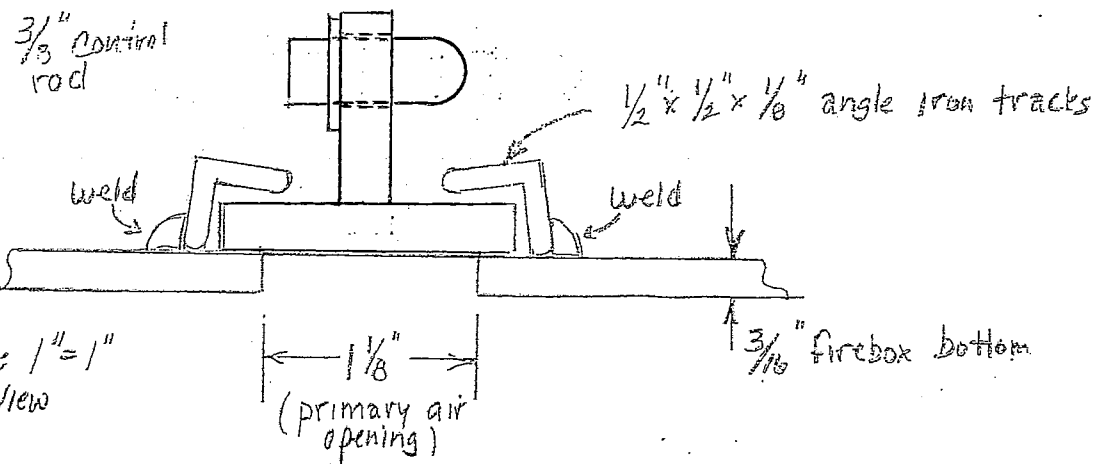
----- =  $1\frac{1}{8}$ " x  $6$ " primary air opening  
 ----- =  $\frac{1}{4}$ " x  $1\frac{1}{2}$ " P.A.C. Slider

Scale:  $\frac{1}{2}$ " = 1", Top View

$\frac{1}{2}$ " x  $\frac{1}{2}$ " 7 iron tracks



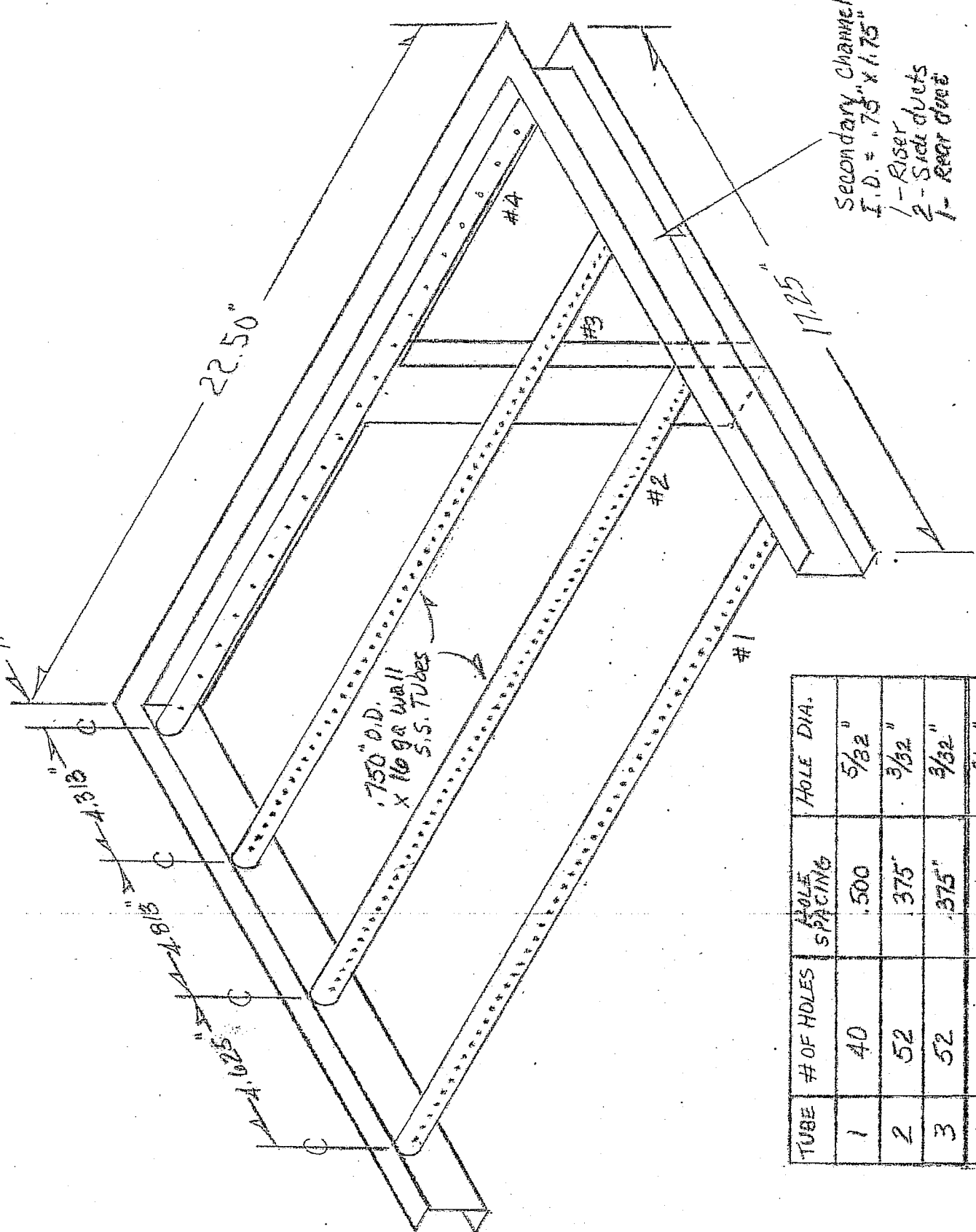
Minimum P.A.C. Setting: .411 SG-in. =  $\frac{1}{2}$  in P.A.C. slider is .122" Dia. equivalent to test model min. open area of  $1.125$ " x  $.3655$ "



TITLE: KUMA MODEL: ASHWOOD	DR. NO. 3	DR. BY: M.F.
VIEW: PRIMARY AIR CONTROL DETAIL	DATE: 3/09	SCALE: AS NOTED

Top of Stove

1.625"

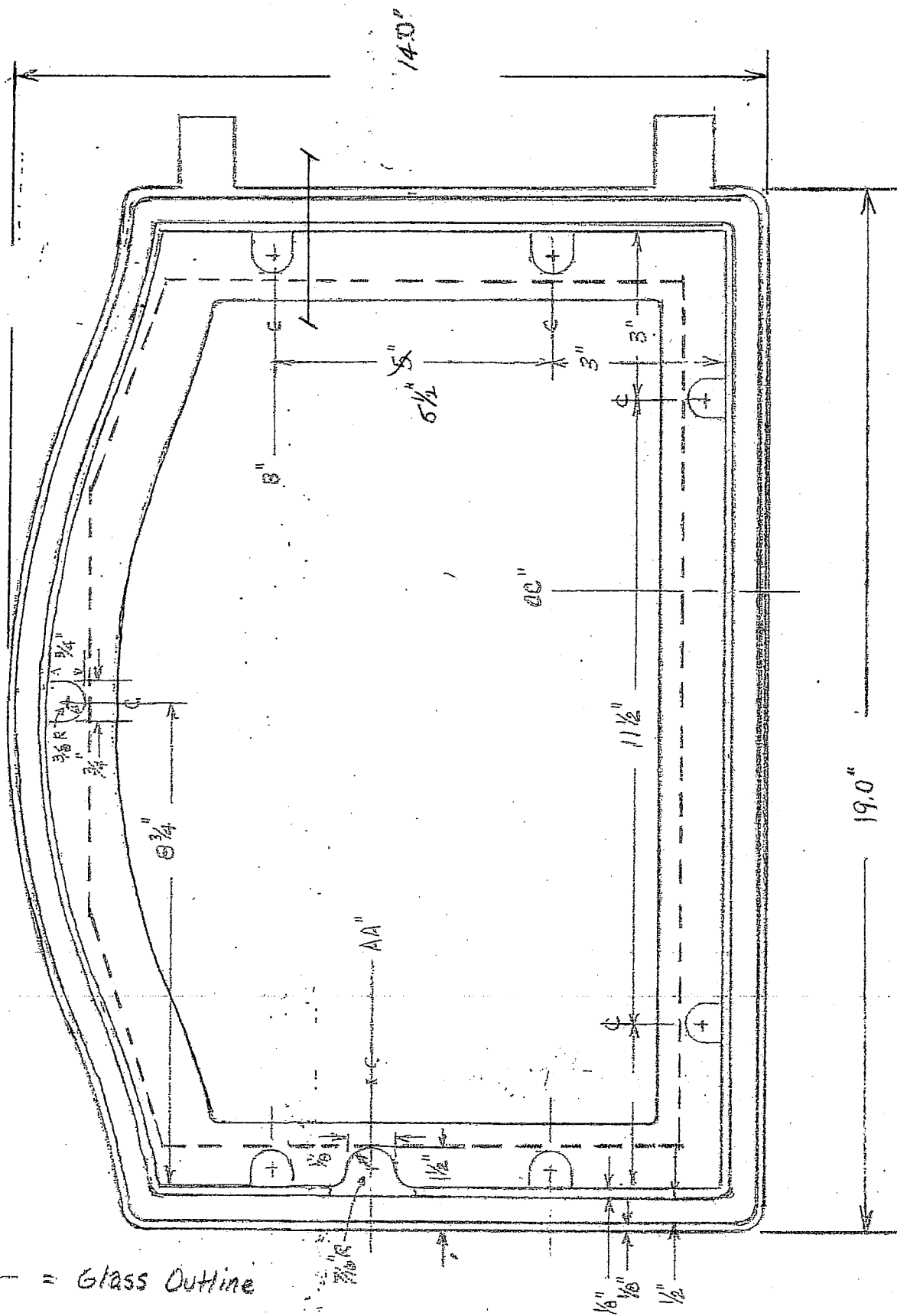


Secondary Channel  
I.D. = .75" x 1.75"  
1 - Riser  
2 - Side ducts  
1 - Rear duct

.750" O.D.  
x 16 ga wall  
S.S. Tubes

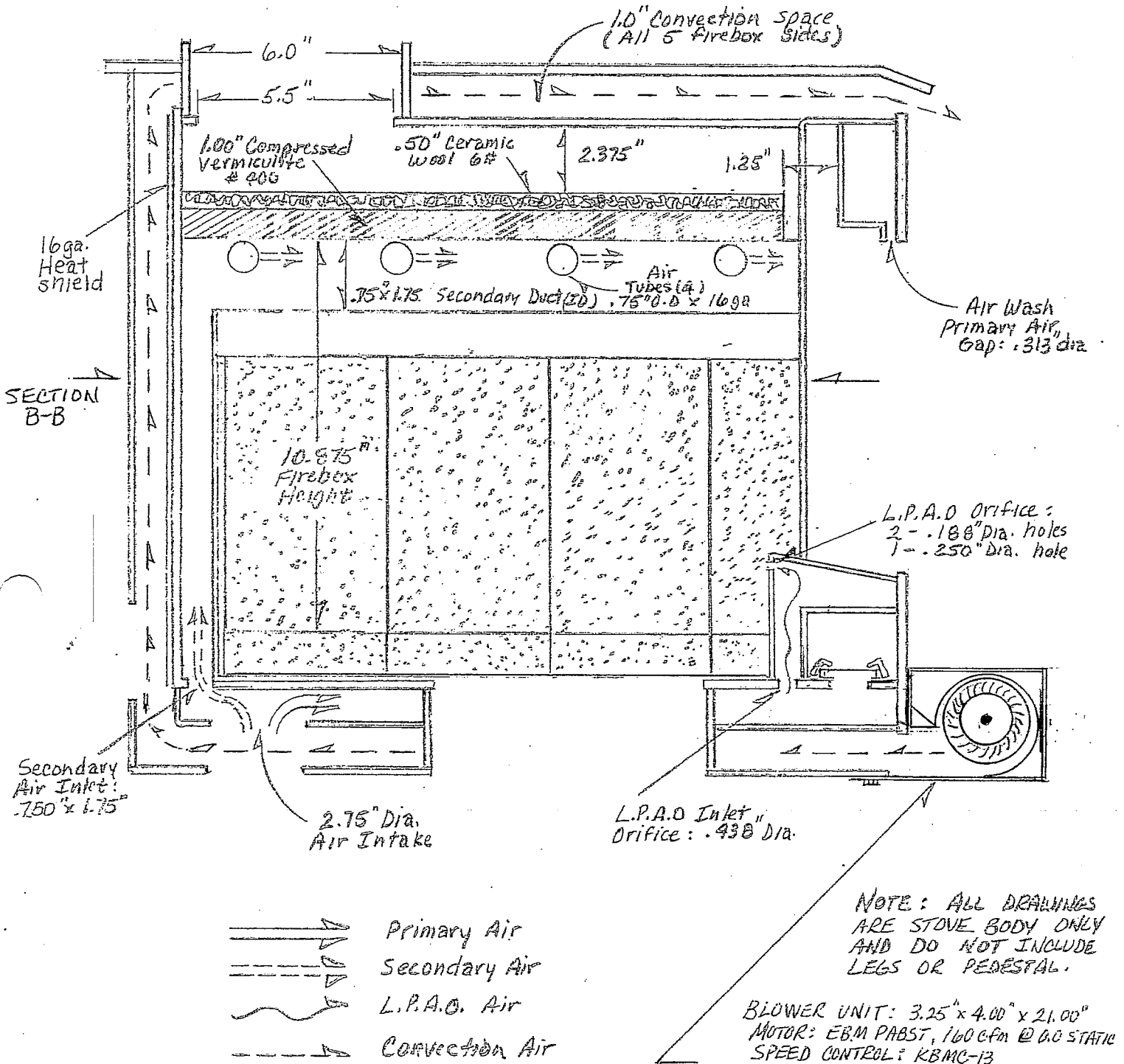
TUBE	# OF HOLES	HOLE SPACING	HOLE DIA.
1	40	.500	5/32"
2	52	.375"	3/32"
3	52	.375"	3/32"
4	20	1.0"	3/32"

TITLE: KUMA MODEL: ASHWOOD	DR # 4	DR BY M.F.
VIEW: SECONDARY PERSPECTIVE	DATE 3/09	SCALE 1/4" = 1"



- - - Glass Outline

TITLE: KUMA MODEL: ASHWOOD	DR # 5	DR BY: M.F.
VIEW: DOOR, BACK	DATE: 3/09	SCALE: 3/8" = 1"



TITLE: KUMA MODEL: ASHWOOD	DR # 6	DR BY M.F.
VIEW BLOWER AIR FLOW	DATE 3/09	SCALE 1/4" = 1"



**KUMA STOVES, INC.**

Operating instructions

**Primary Air Control:** Set primary air control so that the end of the rod attached to the slider is set at:

	Th. Rod	Amt. Orifice is open.
Low	2.309"	0.3655"
M. Low	2.309"-2.5935"	0.3655"-0.650"
M. High	2.5835"-2.8935"	0.550"-0.950"
High	Wide Open	6.00"
FCT	2.309"-2.5935"	0.3655"-0.650"

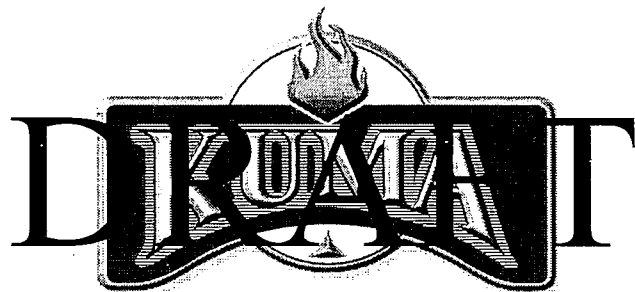
**Door:** Close the door as soon as the fuel is loaded. If the fuel load is slow to ignite, crack the door open 1/8". Adjust the door opening to maximize impact of air flow from door opening in the coal bed. Close the door as soon as the fuel load ignites.

**Fan:** Operate fan as follows. Note that the low setting is when the knob on the speed control is turned clockwise as far as possible.

Low	On low at 30 minutes.
M. Low	On low at 30 minutes.
M. High	On low at 30 minutes.
High	On High at 5 minutes.

**LPAO:** Clear coals away from in front of the LPAO for all runs.





# **KUMA STOVES**

Hayden ID, USA

MODEL# Ashwood

Testing being performed by Omni Test Laboratories

This manual covers the following Kuma stove model:

K-ASH

## **INSTALLATION AND OPERATING INSTRUCTIONS**

**SAVE THESE INSTRUCTIONS**

Revised 4-2-09

Welcome to the Kuma family.

Kuma is a modified version of the Greek word Kauma which means "a great heat".

We would like to take the time to say thank you for purchasing a Kuma stove. If this is your first Kuma stove, you have joined a long list of family members, some since 1981. We are a family business that still desires to maintain a good relationship with each and every one of our customers. Our mission is to provide you with a quality product that will last a lifetime. If you ever have a problem with your stove, we will do what is needed to get it resolved and keep you warm.

You may have noticed a portion of the Bible enclosed in your owner's packet. It is a small gift for you. Our faith in Jesus Christ is very important to us and we have that faith because there is hope in heaven. That hope comes from the message of truth that is found in this new testament.

Thank you for allowing us the opportunity to warm your house. May God bless you and we anticipate that you will enjoy the use of your new Kuma wood stove.

Sincerely,

The Freeman Family

Under specific test conditions, this heater has been shown to meet the U.S. Environmental Protection Agency and Washington State emission limits for residential wood stoves.

*Please read the safety precautions and the entire installation and operation instructions carefully. Failure to properly install and maintain your wood stove can result in an unsafe condition.*

Contents

Section 1.....Safety Precautions

Section 2.....Mobile Home Installation Instructions

Section 3.....Residential Installation Instructions

Section 4.....Wood Burning Operation Instructions

Section 5.....Maintenance

Section 6.....Installation Clearances and Diagrams

Section 7.....Troubleshooting

Section 8.....Replacement Parts List

Section 9.....Warranty

Section 10.....EPA Information

## Section 1 – Safety Precautions

Install and use in accordance with the manufacturers installation and operation instructions contained in this manual only.

1. If this stove is not properly installed, a house fire can occur. For your protection, follow the installation instructions provided. We recommend contacting local building or fire officials regarding restrictions and installation inspection requirements in your area. We also recommend that your Kuma stove be installed by a properly trained and licensed installer, preferably an NFI (National Fireplace Institute) expert.
2. **DO NOT CONNECT THIS UNIT TO A CHIMNEY FLUE SERVICING ANOTHER APPLIANCE.**
3. Do not use gasoline, gasoline-type lantern fuel, kerosene, charcoal lighter fluid, or similar liquids to start or “freshen up” a fire in this heater. Keep all such liquids well away from the heater while it is in use.
4. Do not burn garbage.
5. **DO NOT OVERFIRE.** If any part of the stove or chimney glows, the stove is in an overfire condition. If this happens, shut the air control off immediately.
6. **WARNING: DO NOT INSTALL IN A SLEEPING ROOM**
7. **CAUTION:** The structural integrity of the floor, wall and ceiling/roof must be maintained.
8. **DO NOT USE SINGLE WALL PIPE FOR ANY CHIMNEY APPLICATION, EXTERIOR OR THROUGH THE WALL OR CEILING.** Single wall pipe may only be used as a connection between the stove and an approved masonry or stainless steel chimney. **Single wall pipe may not be used as a connector in mobile homes.**
9. When installing into an existing masonry or metal chimney, examine the chimney system carefully. If you have any questions, seek professional advice. We recommend having existing chimneys cleaned and inspected by a qualified professional prior to the installation of your new stove.
10. **NOTE ALL MINIMUM CLEARANCE REQUIREMENTS TO COMBUSTIBLES.** Installation must comply with minimum clearances as listed in this manual. (see section 6)
11. Do not operate this stove with the door in an open position.
12. **Do not operate this stove with the ash pan open.**
13. This stove must be connected to a minimum 6” diameter listed chimney that complies with U.L. type 103HT factory built chimney or a code approved masonry chimney. If the masonry chimney does not meet code, a U.L. 1777 approved liner must be installed.
14. When connecting single wall or double wall connector pipe to the stove and chimney, use 3 screws per pipe joint including 3 screws securing the pipe to the stove. Depending on the type of double wall pipe you are using, it may also be necessary to fasten it at the chimney. Simpson Duravent’s DVL double wall uses a snap lock connector and does not need screws.
15. When connecting this stove to a masonry chimney, make sure you observe all applicable clearances including walls, ceilings and other combustible material. A masonry chimney must be minimum 6” diameter and constructed with a liner according to NFPA code 211. If you have any questions about the condition or the code compliance of your masonry chimney, please speak with a qualified professional. **WHEN PENETRATING A COMBUSTIBLE WALL TO CONNECT TO AN OUTSIDE MASONRY CHIMNEY YOU MUST BE CERTAIN THAT THE WALL PASS THROUGH IS A SAFE AND LISTED METHOD.** Please refer to NFPA code 211 for details about listed wall pass through methods. To obtain a copy of the NFPA code 211, you may visit their website at [www.nfpa.org](http://www.nfpa.org) or call them toll free at 1(800)344-3555. Your local building department may also have information regarding NFPA code 211.

## Section 2 – Mobile home installation (Leg or Pedestal)

INSTALL AND USE IN ACCORDANCE WITH THE MANUFACTURER'S INSTALLATION AND OPERATING INSTRUCTIONS ONLY. WHILE MOST ANYONE WITH BASIC CARPENTRY SKILLS CAN SUCCESSFULLY AND SAFELY INSTALL THEIR KUMA WOOD STOVE, IT IS HIGHLY RECOMMENDED THAT IT IS INSTALLED BY A QUALIFIED PROFESSIONAL WHO IS PROPERLY TRAINED AND LICENSED—PREFERABLY AN NFI CERTIFIED (NATIONAL FIREPLACE INSTITUTE) EXPERT.

**CAUTION:** The structural integrity of the mobile home floor, walls and ceiling/roof must be maintained. Use additional bracing if required. Never cut a load bearing wall or engineered truss. Use elbows if necessary to offset the pipe.

**CAUTION:** NEVER INSTALL A STOVE IN A SLEEPING ROOM.

*STEP 1: Make sure you have the proper tools, materials, and stove components.*

### Tools:

1. Reciprocating Saw
2. Assorted Screwdrivers
3. Measuring Tape
4. Pencil
5. Plumb Line
6. Electric or Cordless Drill with assorted drill and driver bits
7. Tin Shears
8. Utility Knife
9. Pliers
10. Hammer
11. Assorted Wrenches

### Materials:

1. Caulking to seal roof flashing and storm collar. High temperature silicone is recommended.
2. Assorted heavy duty nails and screws.
3. Short pieces of 2x4 or 2x6. Two pieces minimum 24" long.
4. Copper wire (8 gauge) for grounding. Grounding "clamp" "terminal" or "lug" for attaching ground wire at stove and mobile home frame.

Stove Components: (each component has installation instructions included see sec. 8 for a complete list of accessories)

1. Stove body (K-ASH)
2. Pedestal or leg kit (KA-ASHPED, KA-WLEGSTEEL, etc.)
3. Door Kit (DOOR2CASTC, DOOR2GOLDC, etc.)
4. Outside air kit (KA-OUTSIDEAIR)
5. Optional Blower (KA-BLOWER2)

### Determining the stove location:

When choosing a stove location there are a few things that should be considered.

1. Try to choose a location that is centrally located in the house.
2. Try to choose a location that will be easy to access from your wood storage area.

3. Survey the roof area above and around the location of the chimney exit. Be sure there are no dormers, roof valleys or any other roof irregularities that could cause difficulty when trying to set and seal the roof flashing.
4. If possible, survey the attic area above and around the location of the chimney. Be sure there are no major obstructions such as plumbing, heating ducts, electrical wires, phone cables, etc. Also check the crawl space below and around the stove location for the same obstructions.

*STEP 2: Installing the chimney.*

*Use only 6" Class A solid fuel chimney that has been U.L. Safety tested for wood stoves.*

**IMPORTANT:** These instructions are a very basic guideline for the steps to installing your chimney. For complete instructions, refer to the installation manual that came with your chimney. Chimney installation instructions are usually located in the box with the chimney cap or chimney support components. If you have any questions about the installation of your chimney, please contact the dealer where you purchased your stove.

**CAUTION:** Inspect all chimney components for damage. Do not use any damaged chimney components.

1. Familiarize yourself with the clearances of the stove, for the configuration in which you have chosen to install, i.e. corner installation or straight wall installation (see section 6). Notice the clearances listed for the chimney, this will help you determine the location of the hole in the ceiling.
2. Once you've determined the hole location for the chimney, use a drywall saw or reciprocating saw to cut the ceiling to the desired hole size. **BE SURE TO CHECK FOR OBSTRUCTIONS BEFORE CUTTING THE HOLE, REFER TO PIPE INSTALLATION INSTRUCTIONS FOR HOLE SIZE.**
3. Use a plumb to transfer the ceiling hole center to the underside of the roof sheeting in the attic. Once you've marked the hole center on the roof sheeting, drill a hole from the inside or poke a screw or nail through the sheeting so you can find that location once you're on the roof.
4. **Always be careful when using a ladder and working on a roof. Have someone hold the ladder for you while you are climbing up and down. Use a positioning belt or harness and safety rope to secure yourself on the roof.** Locate the hole or screw/nail on the roof that you poked through from the attic. Lay the roof flashing down and center over the hole, screw or nail. Using a pencil, trace the inside of the flashing cone onto the roof. Remove the flashing and use a reciprocating saw to cut out the hole. **Cut the hole out about 1" larger than the mark all the way around.**
5. Use the two pieces of 2x4 or 2x6 to brace across the trusses in the attic. Position the bracing in a way that you will be able to attach the chimney support with the proper clearance to the bracing (see chimney installation instructions for proper clearances). Attach the chimney support to the bracing using screws or nails.
6. Using a flat pry bar, gently lift the shingles off the roof from the middle of the hole up. Slide the flashing up under the shingles on the top half of the hole and let the flashing sit on top of the shingles on the bottom half of the hole. Use silicone or roof tar to seal underneath the flashing and use screws or nails to fasten the flashing to the roof. Be sure to apply a small amount of sealer to each screw head.
7. Slide the first section of chimney through the flashing and into the chimney support. Chimney supports vary from one brand of pipe to another. Be sure that the first section of pipe is well secured into the chimney support, again, paying close attention to the chimney manufacturers installation instructions.
8. Continue to fasten chimney sections above the first one until the correct height is reached (see pipe installation instructions).
9. Install the chimney cap.
10. Install the storm collar above the flashing and use high temp silicone to seal.

1. If necessary, install a roof brace or guy wires to steady the chimney. Bracing is usually required if the chimney extends more than five feet above the roof.

#### *STEP 3: Installing the hearth and outside air vent*

1. The hearth must be a minimum 3/8" thick non-combustible material and must extend beyond the base of the stove 6" to the sides and back and 16" to the front (see section 6)
2. **When building a hearth pad on site, be sure to leave an area open for the installation of the outside air vent.** Once the hearth is positioned according to the minimum clearances, locate and mark out the hole for the 4" outside air vent. On a pedestal model stove, this hole may be anywhere under the stove base. On a leg model stove, try and locate the hole to line up with the hole in the bottom of the stove. On a pre-manufactured hearth, use a hole saw or circular saw to cut through just the backing board then use a hammer and firmly hit the tile or stone on the top side. If the backing board was cut to the correct depth, the tile or stone will break out very clean. Also using a hole saw or circular saw cut the hole through the home floor into the crawl space. Be sure to line this hole up with the one in the hearth.
3. If you are installing your outside air vent through the wall, use a 4" hole saw or reciprocating saw to cut the hole through the wall. **BE SURE TO CHECK FOR OBSTRUCTIONS IN THE WALL.**

#### *STEP 4: Setting the stove and connecting to the chimney*

1. Assemble the stove (legs, pedestal, ash pan, blower). **Follow the installation instructions that are included in each accessory box.** Once the stove is assembled set the stove gently on the hearth using cardboard to protect the hearth.
2. Position the stove on the hearth according to the clearances shown on the diagrams in section 6. Be sure that the stove is at least minimum clearance from all combustible walls and materials. If possible it is advisable to set the stove 1-2 inches further away from the combustibles than required.
3. USING DOUBLE WALL PIPE ONLY, (single wall is not approved for a mobile home) connect the stove to the chimney. If necessary, use elbows to offset the pipe so that the stove can remain at the correct clearance and still connect to the chimney. Secure each pipe joint with three screws, using the screws provided with the pipe.
4. Drill a small hole through the hearth and route the 8 gauge copper wire into the crawl space. Use a grounding "connector" or "lug" to attach the ground wire to the stove and to the frame of the mobile home.
5. When required by local code, you will need to fasten the stove to the floor of the mobile home. To fasten a leg model, simply mark the location of the hole in the bottom of the legs, drill holes and bolt into the bottom of the leg from the crawl space. To fasten a pedestal model, holes will need to be drilled in the pedestal base. Once the holes are drilled in the base, mark the location on the floor and use bolts and nuts or lag screws to fasten.

Your stove is now ready for use. If your stove installation required a permit and requires inspection by the local building department please do not forget to call for an inspection. It is important that your permit and inspection be finalized, as some insurance companies will require the stove to be inspected. It is also a great idea to give your insurance a call and let them know that you have installed a wood stove.

PLEASE REFER TO SECTION 4-*Wood Burning Operation Instructions* before lighting your first fire.

### Section 3 – Residential installation

INSTALL AND USE IN ACCORDANCE WITH THE MANUFACTURER'S INSTALLATION AND OPERATING INSTRUCTIONS ONLY. WHILE MOST ANYONE WITH BASIC CARPENTRY SKILLS CAN SUCCESSFULLY AND SAFELY INSTALL THEIR KUMA WOOD STOVE, IT IS HIGHLY RECOMMENDED THAT IT IS INSTALLED BY A QUALIFIED PROFESSIONAL WHO IS PROPERLY TRAINED AND LICENSED—PREFERABLY AN NFI CERTIFIED (NATIONAL FIREPLACE INSTITUTE) EXPERT.

**CAUTION:** The Structural integrity of the floor, walls and ceiling/roof must be maintained. Use additional bracing if required. Never cut a load bearing wall or engineered truss. Use elbows if necessary to offset the pipe.

**CAUTION:** NEVER INSTALL A STOVE IN A SLEEPING ROOM.

*STEP 1: Make sure you have the proper tools, materials, and stove components.*

#### **Tools:**

1. Reciprocating Saw
2. Assorted Screwdrivers
3. Measuring Tape
4. Pencil
5. Plumb Line
6. Electric or Cordless Drill with assorted drill and driver bits
7. Tin Shears
8. Utility Knife
9. Pliers
10. Hammer
11. Assorted Wrenches

#### **Materials:**

1. Caulking to seal roof flashing and storm collar. High temperature silicone is recommended.
2. Assorted heavy duty nails and screws.
3. Short pieces of 2x4 or 2x6. Two pieces minimum 24" long.

**Stove Components:** Each component has installation instructions included. (See section 8 for a complete list of accessories.)

1. Stove body (K-ASH)
2. Pedestal or leg kit (KA-ASHPED, KA-WLEGSTEEL, etc.)
3. Door Kit (DOOR2CASTC, DOOR2GOLDC, etc.)
4. Outside air kit (KA-OUTSIDEAIR) Outside air is only required for manufactured homes. Check your local building codes

#### **Determining the stove location:**

When choosing a stove location there are a few things that should be considered.

1. Try to choose a location that is centrally located in the house.
2. Try to choose a location that will be easy to access from your wood storage area.
3. Survey the roof area above and around the location of the chimney exit. Be sure there are no dormers, roof valleys or any other roof irregularities that could cause difficulty when trying to set and seal the roof flashing.



4. If possible, survey the attic area above and around the location of the chimney. Be sure there are no major obstructions such as plumbing, heating ducts, electrical wires, phone cables, etc. Also check the crawl space below and around the stove location for the same obstructions.

*STEP 2: Installing the chimney.*

*Use only 6" Class A solid fuel chimney that has been U.L. Safety tested for wood stoves.*

**IMPORTANT:** These instructions are a very basic guideline for the steps to install your chimney. For complete instructions, refer to the installation manual that came with your chimney. Chimney installation instructions are usually located in the box with the chimney cap or chimney support components. **DO NOT** mix different brands of chimney components. If you have any questions about the installation of your chimney, please contact the dealer where you purchased your stove.

**CAUTION:** Inspect all chimney components for damage. Do not use any damaged chimney components.

*Installing the chimney – Continued*

1. Familiarize yourself with the clearances of the stove for the configuration in which you have chosen to install i.e. corner installation or straight wall installation (see section 6). Notice the clearances listed for the chimney, this will help you determine the location of the hole in the ceiling.
2. Once you've determined the hole location for the chimney, use a drywall saw or reciprocating saw to cut the ceiling to the desired hole size. **BE SURE TO CHECK FOR OBSTRUCTIONS BEFORE CUTTING THE HOLE, REFER TO PIPE INSTALLATION INSTRUCTIONS FOR HOLE SIZE.**
3. Use a plumb to transfer the ceiling hole center to the underside of the roof sheeting in the attic. Once you've marked the hole center on the roof sheeting, drill a hole from the inside or poke a screw or nail through the sheeting so you can find that location once you're on the roof.
4. **Always be careful when using a ladder and working on a roof. Have someone hold the ladder for you while you are climbing up and down. Use a positioning belt or harness and safety rope to secure yourself on the roof.** Locate the hole or screw/nail on the roof that you poked through from the attic. Lay the roof flashing down and center over the hole, screw or nail. Using a pencil, trace the inside of the flashing cone onto the roof. Remove the flashing and use a reciprocating saw to cut out the hole. **Cut the hole out about 1" larger than the mark all the way around.**
5. Use the two pieces of 2x4 or 2x6 to brace across the trusses in the attic. Position the bracing in a way that you will be able to attach the chimney support with the proper clearance to the bracing (see chimney installation instructions for proper clearances). Attach the chimney support to the bracing using screws or nails.
6. Using a flat pry bar, gently lift the shingles off the roof from the middle of the hole up. Slide the flashing up under the shingles on the top half of the hole and let the flashing sit on top of the shingles on the bottom half of the hole. Use silicone or roof tar to seal underneath the flashing and use screws or nails to fasten the flashing to the roof. Be sure to apply a small amount of sealer to each screw head.
7. Slide the first section of chimney through the flashing and into the chimney support. Chimney supports vary from one brand of pipe to another, be sure that the first section of pipe is well secured into the chimney support, again, paying close attention to the chimney manufacturers installation instructions.
8. Continue to fasten chimney sections above the first one until the correct height is reached (see pipe installation instructions)
9. Install the chimney cap
10. Install the storm collar above the flashing and use high temp silicone to seal.
11. If necessary, install a roof brace or guy wires to steady the chimney. Bracing is usually required if the chimney extends more than five feet above the roof.

*STEP 3: Installing the hearth and outside air vent*

OUTSIDE AIR IS REQUIRED FOR MOBILE HOMES ONLY but may be used if desired.

1. The hearth must be a minimum 3/8" thick non-combustible material and must extend beyond the base of the stove 6" to the sides and back and 16" to the front (section 6)
2. When building a hearth pad on site, be sure to leave an area open for the installation of the outside air vent. Once the hearth is positioned according to the minimum clearances, locate and mark out for the 4" outside air vent. On a pedestal model stove, this hole may be anywhere under the stove base. On a leg model stove, try and locate the hole to line up with the hole in the bottom of the stove. On a pre-manufactured hearth, use a hole saw or circular saw to cut through just the backing board then use a hammer and firmly hit the tile or stone on the top side. If the backing board was cut to the correct depth, the tile or stone will break out very clean. Also using a hole saw or circular saw cut the hole through the home floor into the crawl space. Be sure to line this hole up with the one in the hearth.
3. If you are installing your outside air vent through the wall, use a 4" hole saw or reciprocating saw to cut the hole through the wall. **BE SURE TO CHECK FOR OBSTRUCTIONS IN THE WALL.**

*STEP 4: Setting the stove and connecting to the chimney*

6. Attach the legs or pedestal to the stove following the instructions provided in the box with them. Once the legs or pedestal is attached, set the stove gently on the hearth using cardboard to protect the hearth. (If using cast or plated legs you must use leg spacer part# KA-WCLSK)
1. Position the stove on the hearth according to the clearances shown on the diagrams in section 6. Be sure that the stove is at least minimum clearance from all combustible walls and materials. If possible it is advisable to set the stove 1-2 inches further away from the combustibles than required.
2. Using double wall or single wall stove pipe, connect the stove to the chimney. We recommend using double wall pipe regardless of pipe clearance; however, single wall pipe is approved for use. If necessary, use elbows to offset the pipe so that the stove can remain at the correct clearance and still connect to the chimney. Secure each pipe joint with three screws, using the screws provided with the pipe. Be sure to follow the clearance diagrams in section 6 pertaining to the correct pipe, single or double wall. Single wall pipe has a minimum clearance of 18" and double wall a minimum clearance of 8"

Your stove is now ready for use. If your stove installation required a permit and requires inspection by the local building department please do not forget to call for inspection. It is important that your permit and inspection be finalized, as some insurance companies will require the stove to be inspected. It is also a great idea to give your insurance a call and let them know that you have installed a wood stove.

PLEASE REFER TO SECTION 4-*Wood Burning Operation Instructions* before lighting your first fire.

## Section 4 – Wood burning operation instructions

### IMPORTANT:

Your new KUMA wood stove is shipped with a baffle packing to eliminate damage in shipping. Once the stove is set in place and ready to use you will need to remove the baffle restraints. To remove the baffle restraints, cut the ties in front of the nylon buckle and pull forward on the bottom cable until it pulls out. Remove the two cardboard pieces from on top of the baffle and discard. Be careful not to dislodge or damage the ceramic wool blanket on top of the bricks. Your stove is now ready for operation.

### CAUTION:

When building the first couple of fires, be careful to build the fire small and increase the heat slowly over a 4-5 hour period. The paint on the stove “cures” with heat and needs to be done slowly. As the paint “cures” it gives off a smell and even sometimes a visible “smoky” haze into the room. Make sure the area is well ventilated during the curing operation. The smell will disappear after a few hours of operation.

### A word about draft.

The principle of draft is that warm air rises. Your chimney provides draft which sucks the smoke up the chimney. The stove does not “push” out the smoke. Your Wood Classic stove has been designed and approved for use under normal conditions. Unacceptable smoking usually indicates poor draft in your chimney system.

### Recommendations on building and maintaining a fire.

Start by opening the air control on the stove to fully open. Fully open, depending on the model, will be pulled all the way out to the left, pulled all the way forward, or in the case of the largest stove, the two vents near the bottom will be pushed towards the center.

### NEVER USE FLAMIBLE LIQUIDS TO START OR FRESHEN UP A FIRE.

Using a good firestarter can make lighting a fire much easier. There are several different types of firestarter available in “chips” “nuggets” and gels. Newspaper also makes a good fire starter if it is torn into strips. When building a fire, use plenty of fire starter on the bottom and use small kindling directly on top of that. Use progressively larger pieces as you stack wood all the way to the top of the firebox. When starting a fire you should never use unsplit pieces of wood unless they are small such as twigs and branches.

Once the wood is stacked in the firebox, you may light the fire starter and leave the door slightly cracked open for a few minutes to aid in the start up of your stove. Once the fire is well lit, shut the door, but leave the air control in the open position for about 20-30 minutes. After burning for about a half an hour in the open position, you can start to regulate the heat output and burn rate by shutting the air control down.

Remember to let your stove burn open for 20-30 minutes each time you reload it with wood. Shutting the air control prematurely can cause excessive creosote in the chimney: Use the following as a general guideline for desired burn rates.

Low burn	Draft handle pushed all the way in
Med-Low burn	Draft handle pulled out approximately 1/8” – 1/4”
Medium burn	Draft handle pulled out approximately 1/4” – 1/2”
Med-High burn	Draft handle pulled out approximately 1/2” – 1”
High burn	Draft handle pulled out all the way

### Additional instructions and information.

1. Build your fires directly on the firebrick. Using a grate will allow too much air to the coal bed and will result in incomplete combustion of the wood. Using a grate can also leave charred pieces of wood after the fire has gone out.
2. Use only the best grade of dry wood available. Wood should be seasoned for 1 full year prior to being used. Split wood will season much faster and better than wood left in the rounds. Burning green or wet wood greatly increases the chance of creosote build up and produces significantly less heat. The number 1 cause for creosote build up is moisture in the wood. Store your wood

in a dry location. Any wood stored near the stove needs to maintain proper clearance from the stove.

3. Small hot fires produce less creosote than long, low smoldering fires. When you start your stove or are re-kindling (reloading) your wood stove with a full or sizeable load of wood, open the draft fully and burn the stove at full burn for 20-30 minutes to heat up the chimney and secondary burn system. This ensures that when the draft control is pushed in for a lower, longer burn, the stove will burn cleaner. You should notice more upper firebox flame activity. This is smoke from the wood mixing with pre-heated air and burning. This is called secondary burn and results in higher stove temperature at lower burn rates and less soot and creosote build-up. Just after starting the fire, some smoke may occur until the chimney warms up to produce some draft. During normal operation, adjust the draft to the position required. If properly set, it will assure longest burn times and the most even heat cycle. Larger loads of wood will create the longest burn times.

#### **Optional blower operation instructions**

To install the blower, follow the instructions packaged with the blower. Plug the blower into the nearest 115V grounded circuit. Turn the variable speed knob to 'click' onto high speed. As the knob is turned clock-wise, the blower speed decreases to your desired speed. The blower speed should match the desired burn rate on your stove: i.e. low-burn rate...low blower speed; high-burn rate... high blower speed and so forth.

### **Ash Pan Operating Instructions:**

#### **Safety Precautions**

1. Do not operate your wood stove with the ash pan open or removed.
2. Empty the ash pan when the fire is at its lowest point or out.
3. NEVER empty ashes into a combustible container (paper bag, plastic bucket, etc.)
4. NEVER leave ashes in the house or garage. Ashes that seem to be cool may not be.
5. Check gasket on ash pan periodically to ensure a good seal.

#### **Operation**

1. Wait until the fire is at its lowest point or out.
2. Remove the ash pan by turning the handle and pulling out.
3. Take the ash pan outside and dump the ashes into a metal or other non-combustible container.
4. Before replacing the ash pan, check to see if any ashes need to be removed from the ash pan plenum. If any significant amount of ashes remain in the ash plenum, it will prevent the ash pan from sliding all the way in and it may not seal, resulting in air entering the ash grate which will produce a runaway fire.
5. Replace the ash pan by inserting it back into the stove, pushing in on the handle while in the horizontal position, and turning to the straight up and down position (spring pointed down).

## Section 5 – Maintenance

Use the table below as a general maintenance schedule for your stove. See below the table for detailed information on performing the maintenance.

Ash disposal	Every 1-2 weeks
Chimney inspection and cleaning	Every 2-3 months
Gasket replacement	Every year or as needed
Glass cleaning and replacement	As needed
Brick replacement	Replace broken bricks as needed
Clean and inspect stove	Every year
Replace ceramic insulation	Every year or as needed

### Ash disposal – Every 1-2 weeks

1. Empty the ash pan when the fire is out. Never try to empty the ash pan when the stove has an active or full fire, doing so will over heat the stove.
2. Using gloves, remove the ash pan by turning the handle to one side or the other and pulling straight out.
3. Dump the ashes into a non-combustible container away from the house. **NEVER EMPTY ASHES INTO A COMBUSTIBLE CONTAINER SUCH AS A PLASTIC BUCKET OR PAPER BAG. NEVER LEAVE ASHES IN THE HOUSE OR GARAGE.**
4. Before replacing the ash pan, check to see if any ashes need to be removed from the ash pan plenum. If any ashes remain in the ash plenum it will prevent the ash pan from sliding all the way in and it may not seal, resulting in air entering the ash grate which will produce a runaway fire.
5. Replace the ash pan by inserting it back into the stove, pushing in on the handle while in a horizontal position, and turning the handle vertically (spring towards the bottom).

### Chimney inspection and cleaning – Every 2-3 months

1. Refer to the chimney manufacturers installation instructions for additional information on cleaning the chimney. We recommend having the chimney cleaned by a licensed professional chimney sweep.
2. When wood is burned, it releases tar and other organic vapors. When these vapors combine with moisture, creosote is formed and enters the chimney. When the stove is burning on a low setting, the exhaust can be moving slow and the chimney can be relatively cool. This combination of slow exhaust and a cool chimney causes creosote to stick to the walls of the chimney. When creosote accumulates, it causes the draft to slow and the problem of creosote accumulation will compound. If the creosote is not removed on a regular basis, a chimney fire can occur which can damage the chimney and/or stove. Therefore, the importance of regular chimney maintenance cannot be emphasized enough.

### Gasket Replacement – Every year or as needed

1. Gaskets need to be checked at least once a year. The gaskets on your stove are designed to keep unwanted air out of the firebox. Neglecting these gaskets can cause a decrease in burn times, more wood consumption and possible over heating of the stove. When checking the gaskets, look for wear areas that show fraying or cutting. Check the gasket for softness by pressing them with your finger and give a slight tug on one area to see if the glue is still holding. Gaskets that are cut or fraying can cause small air leaks in that spot. Gaskets that are hard will not conform to the stove and may leak air. Gaskets that are not held in with glue could come out at an inconvenient time. The gaskets that need to be checked are: Door gasket, ash pan gasket, and glass gasket. Refer to section 8 for part numbers for the correct gasket for your stove and check with your dealer for parts availability.

### Glass cleaning and replacement – as needed

1. Never clean the glass when it is hot.

2. Clean the glass with an approved stove glass cleaner, never use an abrasive material like sandpaper or steel wool
3. Your stove is equipped with an airwash system that will self-clean the glass. If the glass is black or covered with soot from slow burning, simply load the stove with good, dry, split wood and burn at high burn for about 20- 30 minutes and the glass should burn clean.
4. Never build a fire against the glass.
5. When closing the door be sure that no pieces of wood are protruding from the door opening that could touch the glass. Excessive stress like closing the door on a piece of wood will break the glass. If the glass ever breaks in your stove, don't panic, simply shut the air off and let the fire burn out. Do not continue to operate a stove with broken glass. Do not leave the stove unattended with broken glass.
6. To replace the glass it may be helpful to remove the door from the stove and place on a clean soft work area. Remove the retaining ring screws and retaining ring, remove the glass and dispose of properly, CAUTION: BROKEN GLASS WILL BE SHARP. Clean the door thoroughly where the new piece of glass will install. Set the new piece of glass into the door and replace the retaining ring and screws. Be careful to tighten the screws evenly, uneven pressure can break the glass. Tighten the screws just enough to hold the glass firmly, overtightening can cause uneven pressure and can break the glass.

#### **Brick replacement – As needed**

1. Bricks should be inspected and replaced if necessary at least once a year. Cracked bricks are fine as long as they remain in place. Some of the bricks inside your stove are interchangeable, so shuffling bricks around can be done, for example, a baffle brick that is broken and will not stay in place can be swapped with a brick on the firebox bottom.

#### **Clean and inspect stove – Every year**

1. Your stove should be fully cleaned and inspected once a year. This is a great time to inspect the bricks, gaskets, ceramic blanket and the rest of the stove for signs of abnormal wear. Start by shoveling all the ashes out of the stove and emptying the ash pan. Use a shop vac to clean the hard to reach places. Look at the inside of the stove for signs of wear, paying close attention to the stainless steel baffle brick holders and burn tubes. Discoloration of the stainless steel is normal as is slight sagging. If either of the brick holders is failing to keep the bricks in place then it should be replaced.

#### **Replace ceramic insulation – Every year or as needed**

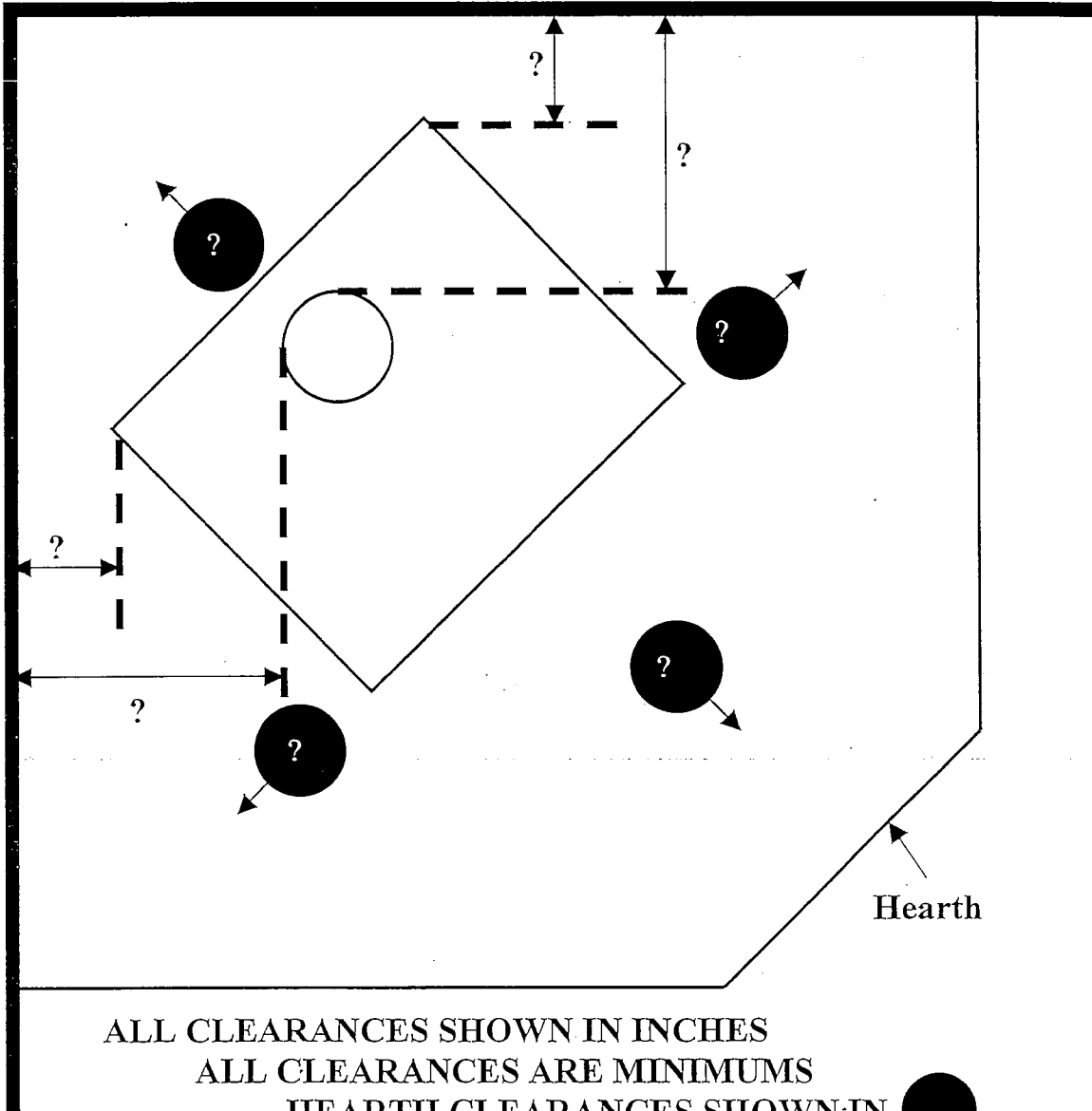
1. At least once a year, check the ceramic insulation on top of the baffle in your stove. The ceramic insulation is designed to keep heat in the stove and increase efficiency. As long as the insulation is in place it can be left alone. If the insulation becomes torn during cleaning, simply lay it back together tightly in that area. If the insulation tears to multiple pieces, it should be replaced, smaller pieces can become caught in the draft and cause a restriction.

**Section 6** – Clearances and diagrams

**Figure #1 Double Wall Pipe**

Use this diagram for the following installations:

1. Mobile Home installation with the stove in a corner using double wall pipe.
2. Residential installation with the stove in a corner using double wall pipe. For single wall pipe, refer to figure 2.



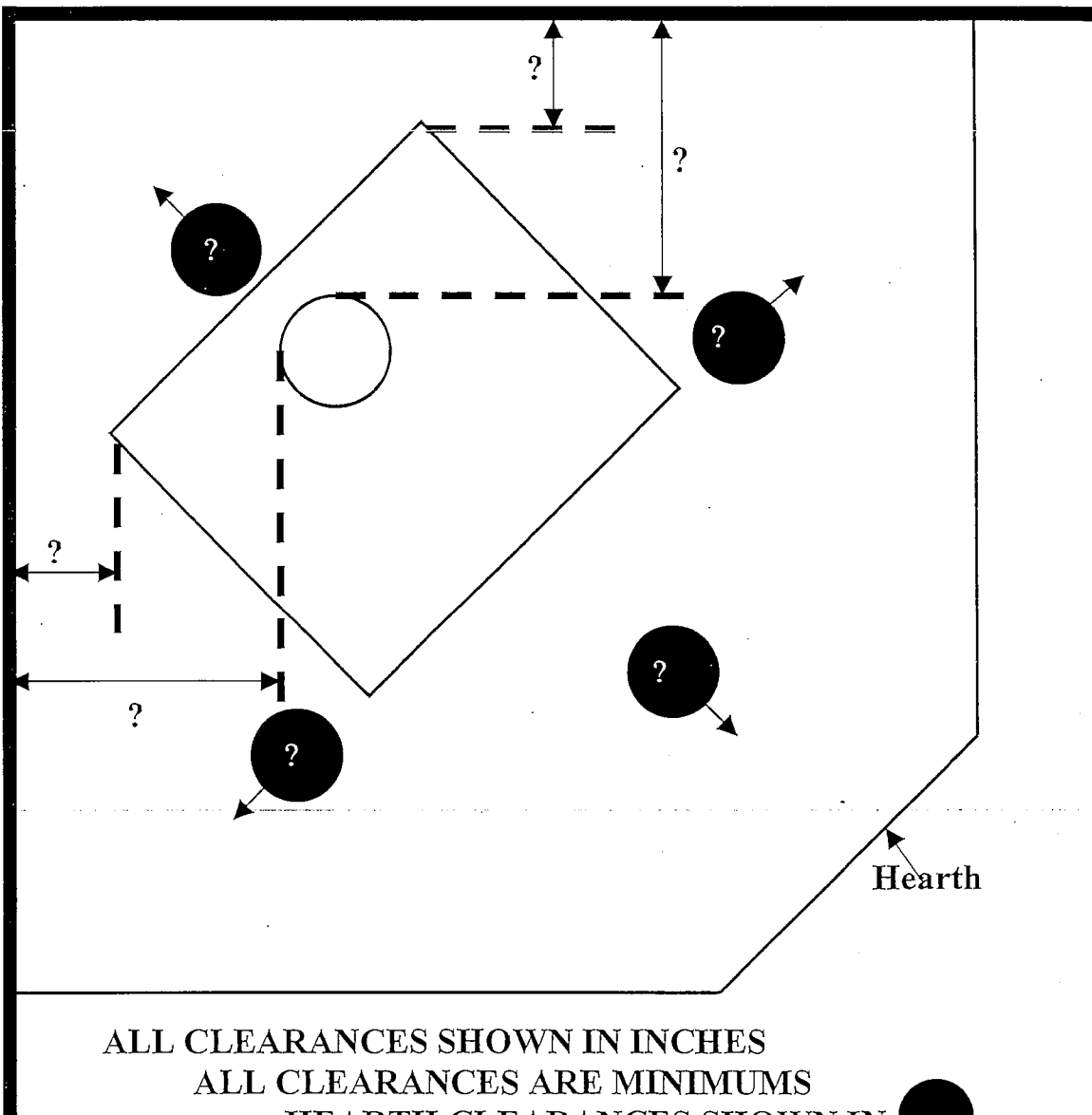
**ALL CLEARANCES SHOWN IN INCHES  
ALL CLEARANCES ARE MINIMUMS  
HEARTH CLEARANCES SHOWN IN**



**Figure #2 Single Wall Pipe**

Use this diagram for the following installation:

1. Residential installation with the stove in a corner using single wall pipe. For double wall pipe, refer to figure 1. For mobile home installation in a corner, refer to figure 1

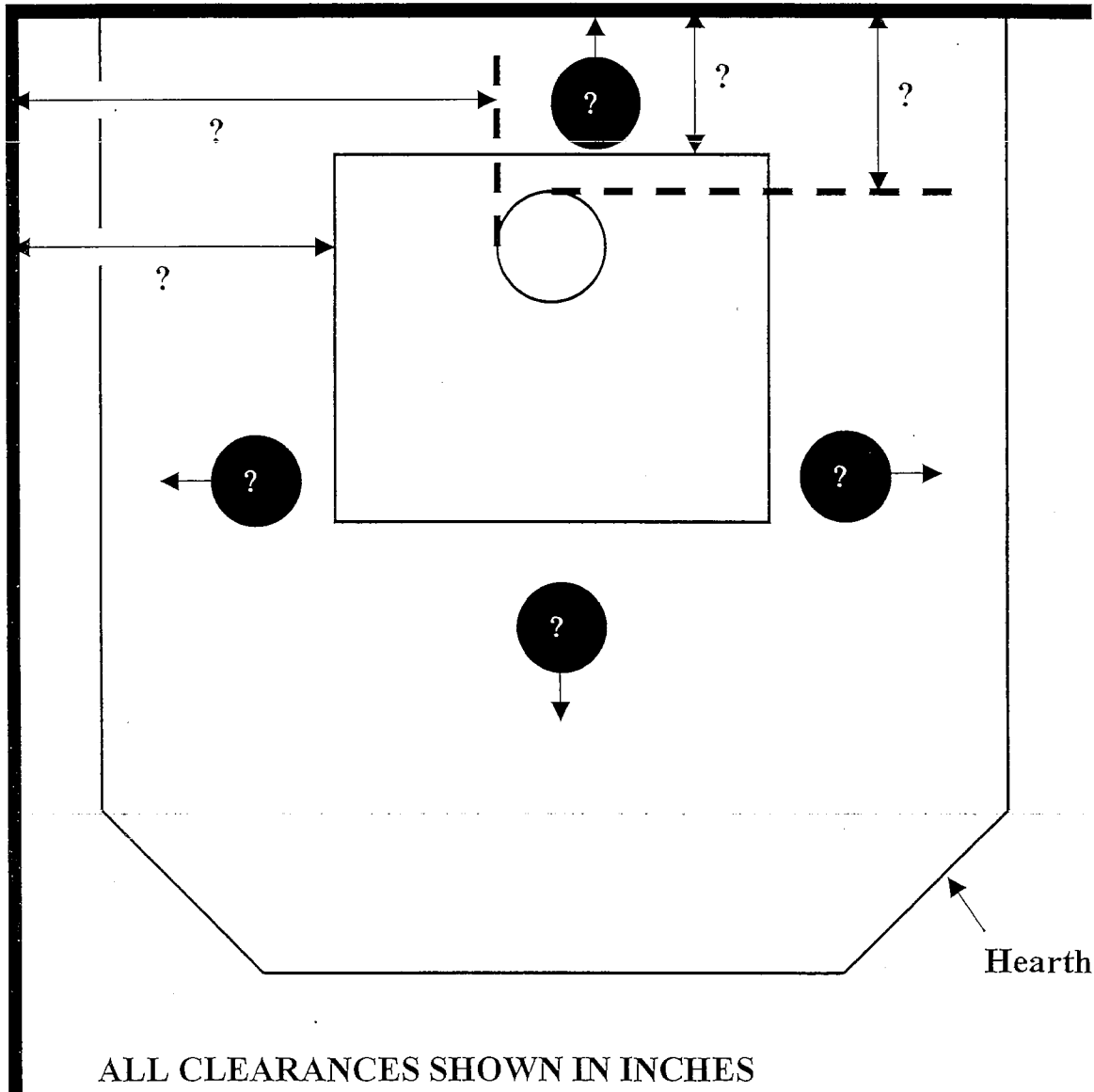




**Figure #3 Double Wall Pipe**

Use this diagram for the following installations:

1. Mobile home installation with the stove on a straight wall using double wall pipe.
2. Residential installation with the stove on a straight wall using double wall pipe. For single wall pipe, refer to figure 4.

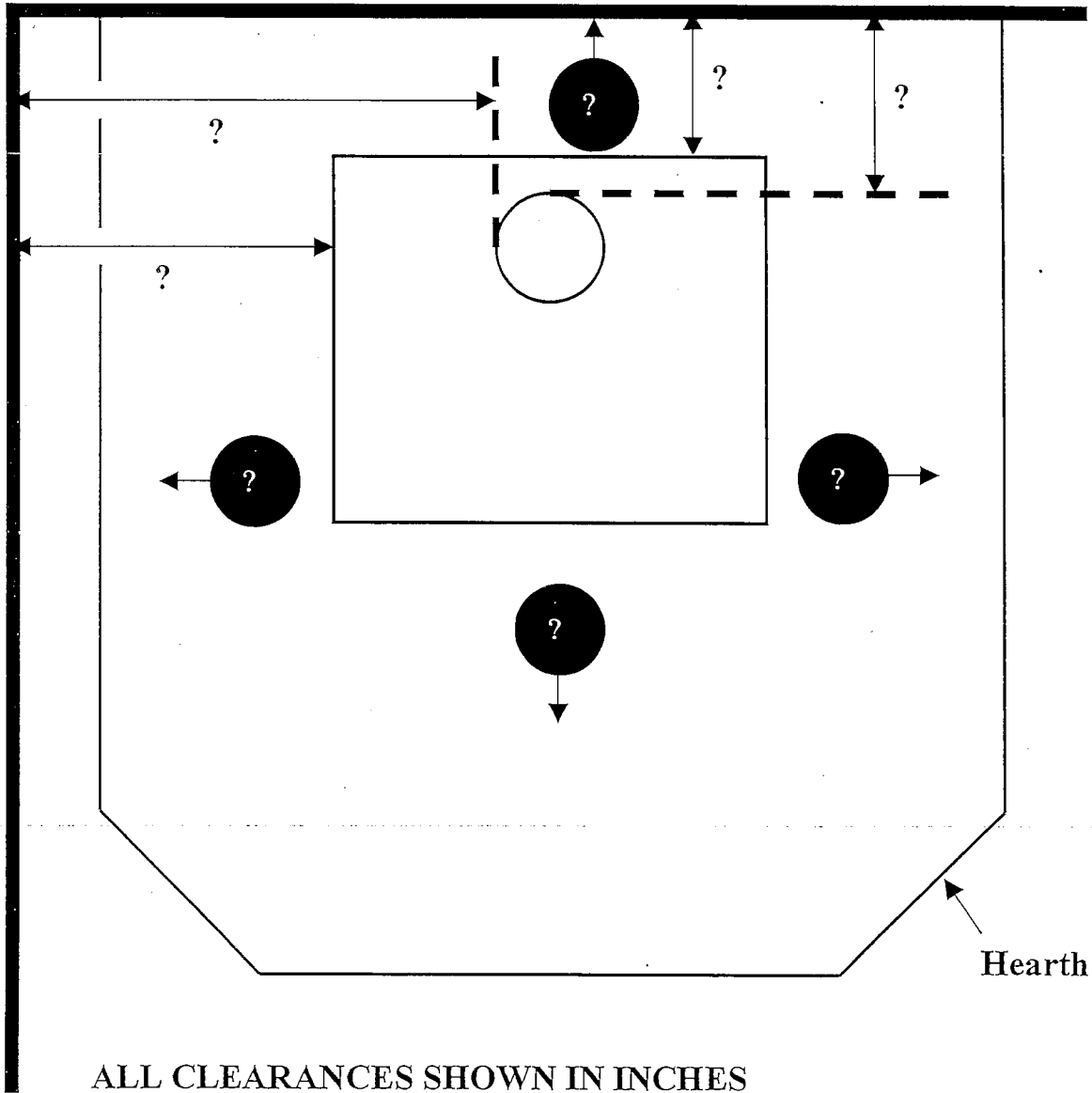


**ALL CLEARANCES SHOWN IN INCHES  
ALL CLEARANCES ARE MINIMUMS .  
HEARTH CLEARANCES SHOWN IN** ●

**Figure #4 Single Wall Pipe**

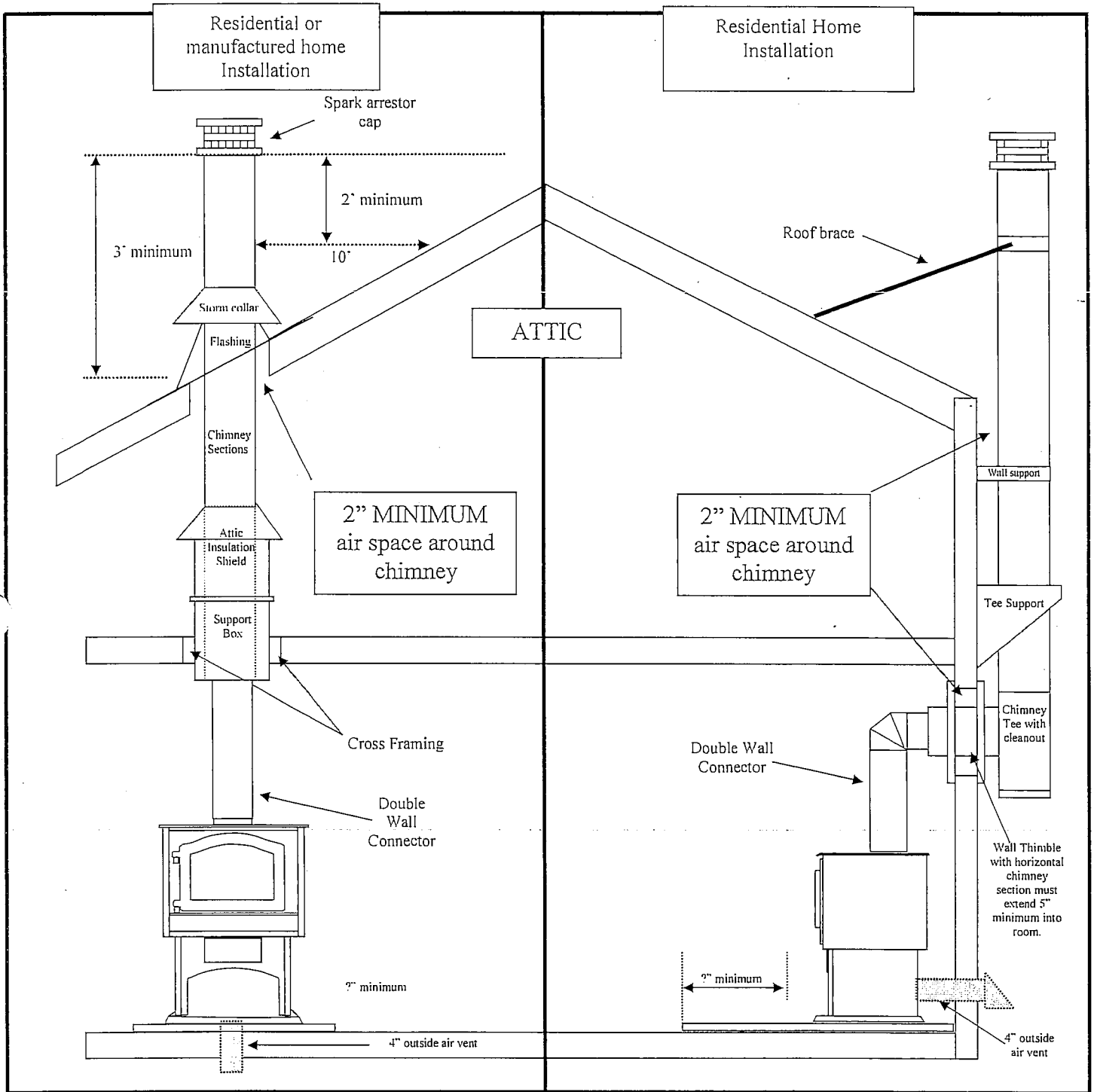
Use this diagram for the following installations:

1. Residential installation with the stove on a straight wall using single wall pipe. For double wall pipe, refer to figure 3. For mobile home installation on a straight wall refer, to figure 3.



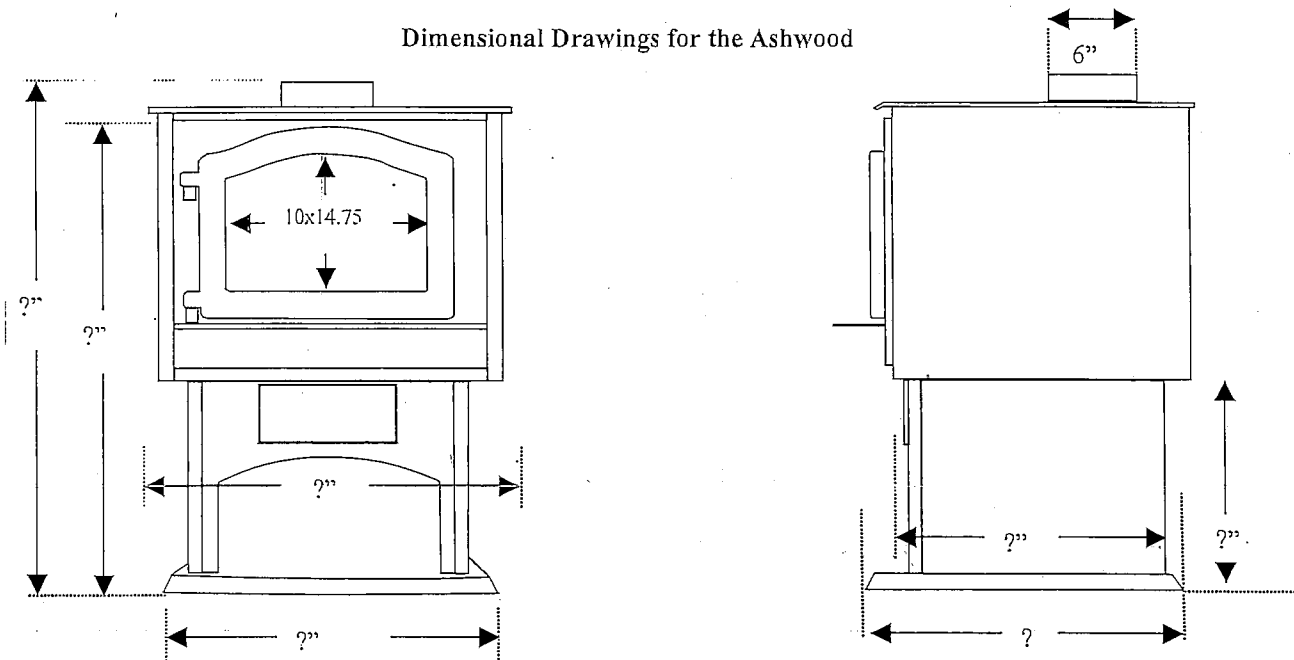
**ALL CLEARANCES SHOWN IN INCHES  
ALL CLEARANCES ARE MINIMUMS  
HEARTH CLEARANCES SHOWN IN ●**

Ashwood Installation diagram for manufactured chimneys  
**NEVER INSTALL A WOOD STOVE IN A SLEEPING ROOM**

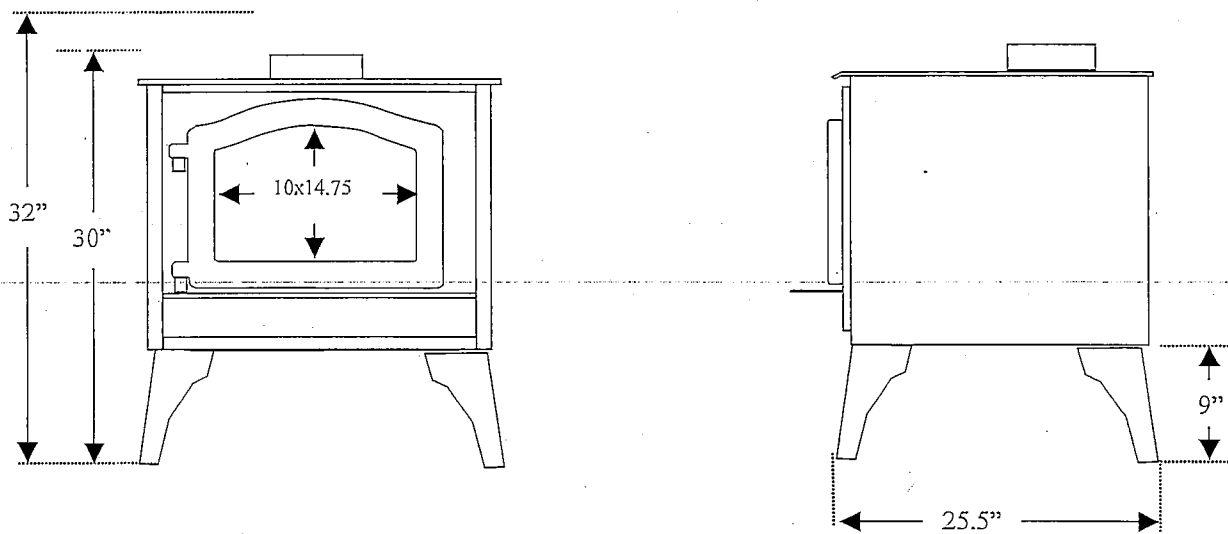


These diagrams are for manufactured chimneys. For Brick Chimneys a safety listed thimble must be used when a connection is made through a combustible wall to a lined masonry chimney. This stove may be connected to a lined masonry chimney or a listed factory built chimney designed for use with solid fuels and conforming to, Canadian ULC629 or USA UL-103HT . Clearances to combustibles must be maintained per manufacturer's instructions on chimney pipe , and stove pipe connectors. Use only double-wall connector in mobile homes

Dimensional Drawings for the Ashwood



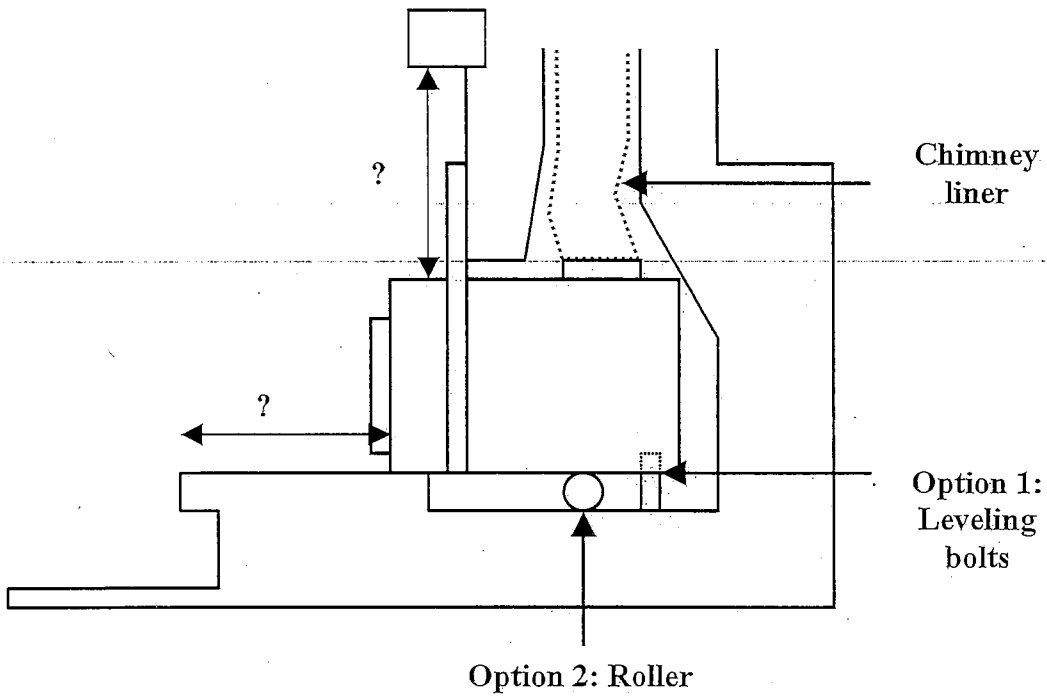
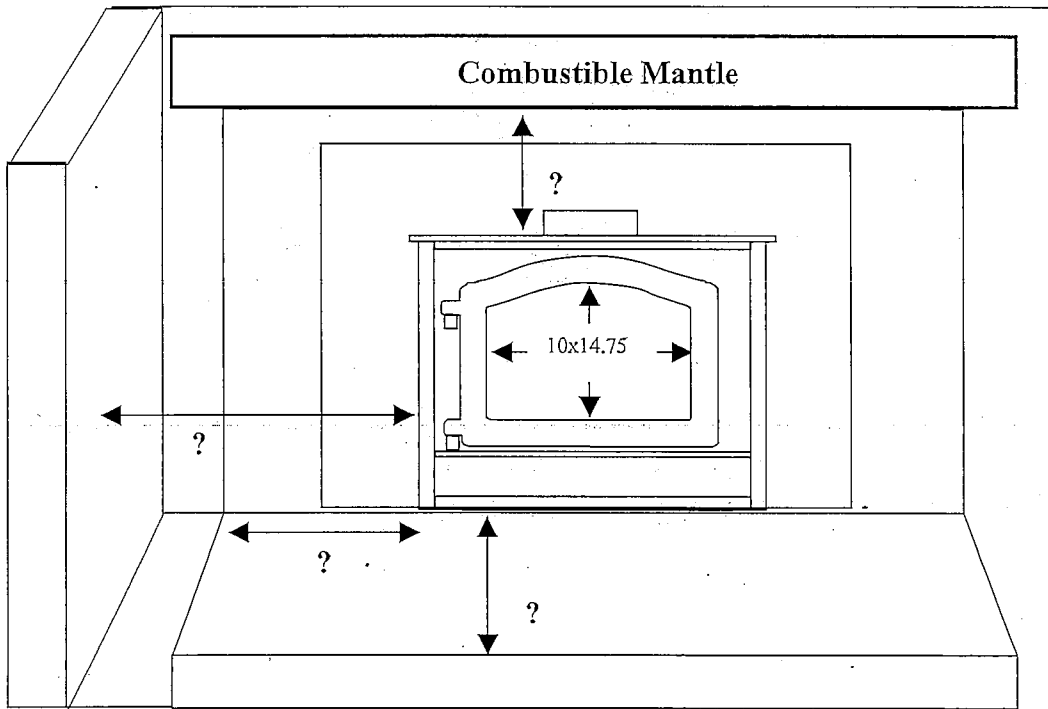
Ashwood Pedestal (K-ASH + KA-ASHPED)



Wood Classic Leg (K-WC + KA-WLEGSTEEL)

Figure #5 Insert

Use this diagram for the following installations: 1. Installation into a masonry fireplace



## Section **7** – Trouble Shooting

1. Stove burns lazy at start up.
2. Stove back-puffs or smokes into the room at start up.
3. Stove smokes out the door when it is open.
4. Stove won't shut down.
5. Stove won't burn hot enough. Lazy burn.
6. Burn time too short.

### Stove burns lazy at start up. return to top

1. The chimney is still cool, allow more time to warm up.
2. Wood is not seasoned (still green). Wood should sit for about 1 year, split and loosely stacked if it was cut green.
3. Wood is well seasoned but has a lot of surface moisture. Your wood supply must be covered. Check your tarps or other covering to see that no rain or snow is getting to your wood. Wood should be covered on top, but open on the sides to allow air movement to aid in drying.
4. Check the air supply to the stove. If you have installed outside air, check the ducts for blockage. If you are not using outside air, be sure you have removed the cover plate on the back of the pedestal. (pedestal models only)

### Stove back-puffs or smokes into the room at start up. return to top

1. Chimney is cold. Cold chimneys can produce a “reverse draft” where cold air is rushing down the chimney into the stove. Open a door or a window for about 5 minutes to equalize pressure in the house then try restarting with small strips of newspaper. Using small strips of newspaper or an approved fast burning firestarter and small pieces of kindling will create heat faster to help reverse the cold air.
2. Chimney and/or the chimney cap needs to be cleaned. Your chimney should be checked and cleaned if necessary every few months. Even a small amount of build up can cause a draft restriction, for example: ¼ inch of build up on the side wall of a 6” chimney reduces the effective area of the chimney by about 20%. Pay close attention to the chimney cap, especially if it has a screen. Screened chimney caps can become blocked enough to restrict flow in just a few weeks.

### Stove smokes out the door when it is open. return to top

1. The door was opened too quickly. Crack the door open just a small amount and let the stove “breathe” a few seconds before opening all the way.
2. Chimney and/or the chimney cap needs to be cleaned. Your chimney should be checked and cleaned if necessary every few months. Even a small amount of build up can cause a draft restriction, for example: ¼ inch of build up on the side wall of a 6” chimney reduces the effective area of the chimney by about 20%. Pay close attention to the chimney cap, especially if it has a screen. Screened chimney caps can become blocked enough to restrict flow in just a few weeks.

### Stove won't shut down. return to top

1. The ash pan may not be sealing correctly (pedestal model). Check the ash pan gasket for tearing or fraying. See the ash pan instructions in section 5. Even a small amount of undesired air can keep the stove from shutting down.
2. Check the main door gasket and glass gasket for proper seal. See section 5 for instructions on checking your gaskets.

### Stove won't burn hot enough. Lazy burn. return to top

1. Wood is not seasoned (still green). Wood should sit for about 1 year, split and loosely stacked if it was cut green.

2. Wood is well seasoned but has a lot of surface moisture. Your wood supply must be covered. Check your tarps or other covering to see that no rain or snow is getting to your wood. Wood should be covered on top, but open on the sides to allow air movement to aid in drying.
3. Chimney and/or the chimney cap needs to be cleaned. Your chimney should be checked and cleaned if necessary every few months. Even a small amount of build up can cause a draft restriction, for example: ¼ inch of build up on the side wall of a 6" chimney reduces the effective area of the chimney by about 20%. Pay close attention to the chimney cap, especially if it has a screen. Screened chimney caps can become blocked enough to restrict flow in just a few weeks.
4. Check the air supply to the stove. If you have installed outside air, check the ducts for blockage. If you are not using outside air, be sure you have removed the cover plate on the back of the pedestal. (pedestal models only)
5. Atmospheric conditions. Occasionally, barometric episodes occur that affect draft, thereby affecting stove performance. If your stove has been working fine and performance drops suddenly, this is most likely the cause, and will usually go away within a few days.
6. Your fuel load may be too small or the wood size too large for the coal bed. A small bed of coals requires re-kindling to build up the heat, only put large chunks of wood on a very hot and active bed of coals.

**Burn time too short.** return to top

1. Your fuel load may be too small or the wood size too large for the coal bed. A small bed of coals requires re-kindling to build up the heat, only put large chunks of wood on a very hot and active bed of coals. If there are large chunks of charred wood left after the fire has gone out, the coal bed was not hot enough.
2. Fuel quality. Harder, denser woods produce longer burn times. Likewise, softer woods produce shorter burn times.
3. The ash pan may not be sealing correctly. Check the ash pan gasket for tearing or fraying. See the ash pan instructions in section 5. Even a small amount of undesired air can keep the stove from shutting down.
4. Check the main door gasket and glass gasket for proper seal. See section 5 for instructions on checking your gaskets.

## **Section 8 – Accessories and Parts**

### *Accessories*

1. KA-BLOWER2- Stove blower.
2. KA-OUTSIDEAIR- Outside air kit.
3. KA-WLEGSTEEL- Black steel leg set.
4. KA-WLEGCAST- Black cast iron leg set.
5. KA-WLEGGOLD- Gold plated leg set.
6. KA-WLEGPEWTER- Pewter plated leg set.
7. KA-WCPED- Pedestal kit (includes ash pan)
8. KA-SUNBURST1BLK- Decorative window sunburst, painted black.
9. KA-DOOR2CASTC- Complete black door. Includes: Glass, glass holder, gaskets, door handle and door pins.
10. KA-DOOR2GOLDC- Complete gold door. Includes: Glass, glass holder, gaskets, door handle and door pins.
11. KA-DOOR2PEWTERC- Complete pewter door. Includes: Glass, glass holder, gaskets, door handle and door pins.

### *Parts*

1. KR-ASHGRATE- Replacement ash grate

2. KR-ASHPANGASK- Replacement ash pan gasket, includes glue.
3. KR-BRICK- Replacement firebrick.
4. KR-DOORGASKET- Replacement door gasket, includes glue.
5. KR-GLASS2- Replacement glass, includes gasket.
6. KR-GLASSGASKET- Replacement glass gasket
7. KR-ASHBURNTUBE1- Front baffle burn tube.
8. KR-ASHBURNTUBE2- Middle-front baffle burn tube.
9. KR-ASHBURNTUBE3- Middle-rear baffle burn tube.
10. KR-ASHBURNTUBE4- Rear baffle burn tube.
11. KR-ASHINSULATION- Ceramic baffle insulation.
12. KR-ASHBAFFLE- Ceramic baffle board

## **Section 9 – Warranty and warranty registration**

For all warranties, please contact the dealer where you purchased your stove. Kuma Stoves will not warranty defective products directly to the consumer.

### ***THE WARRANTY ON YOUR NEW KUMA STOVE IS AS FOLLOWS:***

#### **Lifetime warranty:**

All welded steel components including but not limited to: Firebox, top plate, convection shell, stove base, ash drawer, firebrick holders, air plenums and ash plenum.

#### **5 year warranty:**

All stainless steel baffle components including: Front and rear baffle brick holders and secondary burn tubes. All cast iron components including: Door casting (does not include gold or pewter plating) and ash grate.

#### **1 year warranty:**

Stove blower (if equipped).

#### **30 day warranty:**

Gold or pewter plating including the plating on the stove door or sunburst. Gold and pewter is warranted against chipping/flaking only, NOT tarnishing or scratching. Glass is warranted for 30 days against single line cracking, NOT multiple line or "spider web" cracking. Paint is warranted against flaking/bubbling only, NOT scratching or discoloration.

#### **NOT WARRANTED:**

Including but not limited to: Firebrick, ceramic insulation, door gasket, glass gasket and ash pan gasket.

This warranty does not apply in cases of abuse, mishandling, unauthorized repair, alterations, misuse, accident, misapplication, improper installation, improper maintenance and/or service. Kuma Stoves reserves the right, under this warranty, to replace, repair or authorize repair of the defective product at its sole discretion. No other warranty, expressed or implied accompanies this written warranty.



Section **10** – EPA Information

If you are a dealer and you will be displaying this stove, please cut this tag out and affix it to the stove.

Manufactured by KUMA STOVES INC. Model: ASHWOOD

US ENVIRONMENTAL PROTECTION AGENCY

MEETS EPA PARTICULATE MATTER (SMOKE)  
REQUIREMENTS FOR NON-CATALYTIC WOOD HEATERS  
MANUFACTURED ON OR AFTER JULY 1, 1990

**SAMPLE:**

SMOKE  
THIS MODEL

TBD

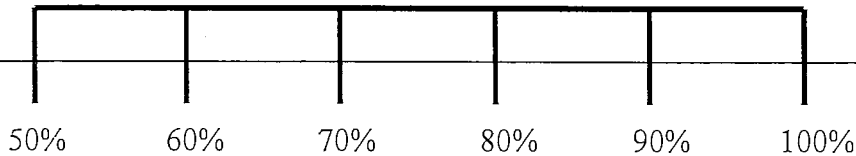
**ACTUAL #’S**  
(GRAMS PER HOUR)

0

7.5

EFFICIENCY\*

**TBD**



Wood heaters with higher efficiencies cost less to operate.

**\*NOT TESTED FOR EFFICIENCY. THE VALUE INDICATED IS FOR  
SIMILAR NON-CATALYST EQUIPPED WOOD HEATERS.**

**HEAT OUTPUT**

**??,??? TO ??,??? BTU/HR**

Use this to choose the right size appliance for your needs. Ask dealer for help.

This wood heater will achieve low smoke output and high efficiency only if properly maintained. See owners manual.

## STOVE STORAGE

The KUMA Ashwood Noncatalytic Woodstove tested by

Myren Consulting, Inc. is being held in custody by

Kuma Stoves, Inc. and is being stored at:

Kuma Stoves, Inc.

Contact person(s):

2150 W. Hayden Ave.

Mark Freeman

Hayden, ID 83835

Phone:

208 762 8002

**A. Temporary storage at Myren Consulting until certification is granted:**

A single strap of steel banding is placed around the stove so that the banding crosses the door horizontally, making it impossible to open the door on the unit. If it is necessary to break the banding to check an internal dimension or component, the banding is immediately replaced after the work on the unit is completed. The unit is identified with its name written on a stove storage label that is taped to the window of the unit. (See next page for an example copy of a stove storage label.)

**B. Permanent storage after certification has been granted:**

The following measures have been taken to permanently seal the unit and prevent tampering. Several lengths of steel banding are placed around the stove in a manner that prevents the door from being opened. At least two of these lengths cross at 90° angles. At each 90° crossing point on the top of the stove and perhaps elsewhere, a Myren Consulting address label is placed over the crossing point. The lab manager then initials the label and it is then taped in place with 2" clear packing tape. The stove is then loaded onto a pallet and strapped to the pallet with several lengths of steel banding. A box - either cardboard, chipboard or plywood - is placed over the stove and attached to the pallet.

**C. The sealed unit is identified as follows:**

The name of the unit is written on a Myren Consulting address label which is affixed to the outside of the box. The top and sides of the box also have several stove storage labels affixed to it which clearly identify the unit as a test stove being stored pursuant to 40 CFR Part 60. These labels have the name of the stove clearly written on them. (A sample stove storage label follows on the next page.)

**D. The unit was returned to the manufacturer via:** Commercial  
Carrier (USF Reddaway) or by pickup truck.

W A R N I N G

SEALED EPA TEST STOVE

DO NOT OPEN OR TAMPER WITH THE SEALS AND PACKAGING ON THIS STOVE.

TO DO SO WILL VOID THE CERTIFICATION ON THIS STOVE.

Kuma Ashwood

W A R N I N G

SEALED EPA TEST STOVE

DO NOT OPEN OR TAMPER WITH THE SEALS AND PACKAGING ON THIS STOVE.

TO DO SO WILL VOID THE CERTIFICATION ON THIS STOVE.

